# PROCESSED DATA FROM THE STRONG-MOTION RECORDS OF THE IMPERIAL VALLEY EARTHQUAKE

OF 15 OCTOBER 1979

— FINAL RESULTS — 1983

## CALIFORNIA DEPARTMENT OF CONSERVATION DIVISION OF MINES AND GEOLOGY

SPECIAL PUBLICATION 65







STATE OF CALIFORNIA GEORGE DEUKMEJIAN GOVERNOR

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OF THE IMPERIAL VALLEY EARTHQUAKE
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Ву

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### CONTENTS

	Page
INTRODUCTION	1
EARTHQUAKE CHARACTERISTICS	1
STATION DESCRIPTIONS	1
Meloland Overpass Bridge	
Imperial County Services Building	
Freefield Station Near the Imperial County Services	,
Building	7
Westmorland and Niland Freefield Stations	
RECORDS, DIGITIZATION AND PROCESSING	8
1. Uncorrected Accelerograms	9
2. Corrected Accelerations, Velocities, Displacements	11
3. Response Spectra	12
4. Fourier Spectra by FFT	12
5. Duration Spectra	
6. Spectra of Amplitude Sustained for any Given	
Number of Cycles	12
REFERENCES	19
APPENDIX. Computer plots of processing	23
El Centro - Rt. 8/Meloland overcrossing	
El Centro - Imperial County Services Building	
El Centro - Imperial County Center - Ground	
Westmorland	
Niland	
Westmorland (Aftershock)	295

#### **ILLUSTRATIONS**

Figure	1	Location map of CDMG stations and October 15, 1979 earthquake epicenter in Imperial Valley	2
Figure	e 2	El Centro - Route 8/Meloland overpass Instrumentation scheme	4
Figure	e 3	El Centro - Imperial County Services Blvd.	6
		TABLES	
Table	1.	Epicentral, focal, and fault distances (km)	3
Table	2.	Digitized measurements from the Rt. 8/Meloland overcrossing record	14
Table	3.	Digitized measurements from the Imperial County Services Bldg. record	15
Table	4.	Record data and instrumental constants	16
Table	5.	Variable sensitivities	17
Table	6	Peak values of processed data	18

#### INTRODUCTION

This report contains summaries and plots of the results of completed processing performed on the six most significant strong-motion records obtained at five California Division of Mines and Geology (CDMG) accelerograph stations during the Imperial Valley earthquake of 15 October 1979.

Information on all the CDMG strong-motion records recovered from this earthquake as well as on the CDMG accelerograph stations from which these records were obtained was published by CDMG in 1980 in its Preliminary Report 26. Copies of Preliminary Report 26 as well as additional copies of this report are available from California Division of Mines and Geology, Office of Strong Motion Studies, 2811 "O" Street, Sacramento, California 95816.

Digital data of the processed records corresponding to the plots of the Volume 1, 2, and 3 (uncorrected data, corrected data, and Fourier and response spectra, respectively) may be obtained on magnetic tape from CDMG at the above address.

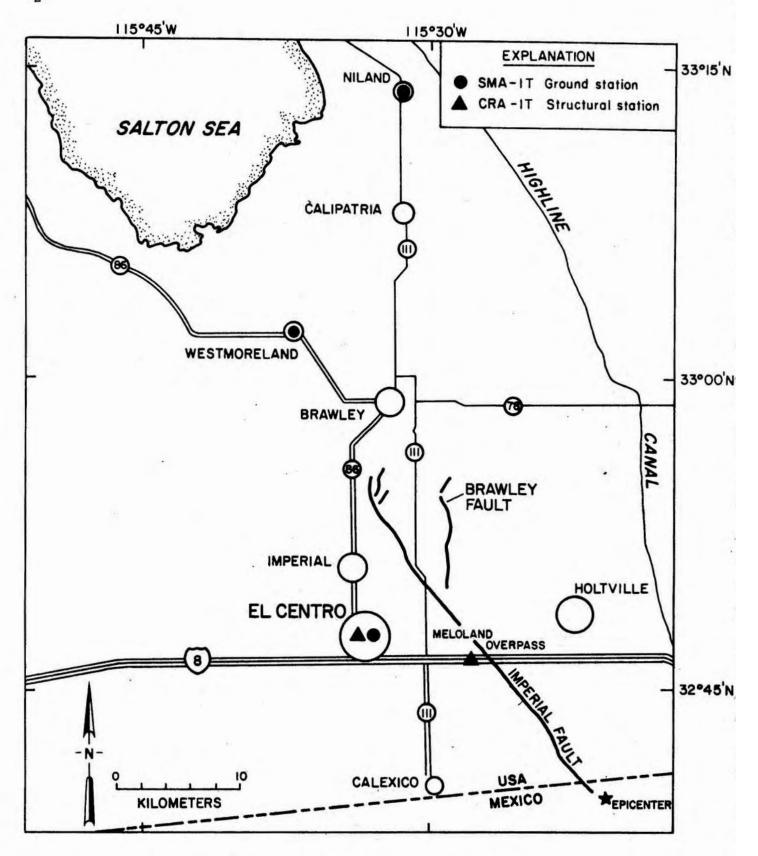
Processed data of additional records of this earthquake may be found in U.S. Geological Survey Open-File Report 80-703 (Brady and others, 1980).

#### EARTHQUAKE CHARACTERISTICS

A moderate-magnitude earthquake ( $M_L$  = 6.6, California Institute of Technology, Seismology Laboratory) occurred at 16:17 (PDT) on 15 October 1979, approximately 15.5 km east-southeast of Calexico, California (Figure 1). The main shock, a 12 km focal depth event centered in Baja, California, was located at 32.63°N latitude and 115.33°W longitude (Brady and others, 1980). The earthquake was generated by right-lateral slip on the northwest trending Imperial fault, and produced approximately 30 km of surface rupture that extends northward from the international border into the United States.

#### STATION DESCRIPTIONS

As stated above, strong-motion records for the Imperial Valley earthquake were obtained at five CDMG accelerograph stations. These five stations were: (1) the Meloland overpass bridge; (2) the Imperial County Services Building; (3) a freefield station near the County Services Building; and (4 and 5) the Westmorland and Niland freefield stations. Table 1 presents the distances from each of these stations to the epicenter of the Imperial Valley earthquake, to its focal point, and to the nearest point on the fault trace associated with the earthquake.



 Location map for 15 October 1979 Imperial County Earthquake. The CDMG stations as well as the epicenter are indicated.

TABLE 1: EPICENTRAL, FOCAL, AND FAULT DISTANCES (km)

Station	Epicentral distance	Focal <sup>1</sup> distance	Fault <sup>2</sup> distance
El Centro - Rt. 8/Meloland overcrossing	19	23	0.5
El Centro - Imperial County Services Bldg	28	31	7.3
El Centro - Imperial County Center Ground	28	31	7.2
Westmorland	53	54	13
Niland	70	71	34

<sup>1</sup> focal depth = 12 km (Brady and others, 1980)

Distance to the nearest point on the fault trace associated with the 1979 Imperial Valley earthquake, from the CDMG Alquist-Priolo special studies maps for the El Centro and Brawley quadrangles.

#### El Centro ROUTE 8/MELOLAND OVERPASS Strong Motion Instrumentation Scheme

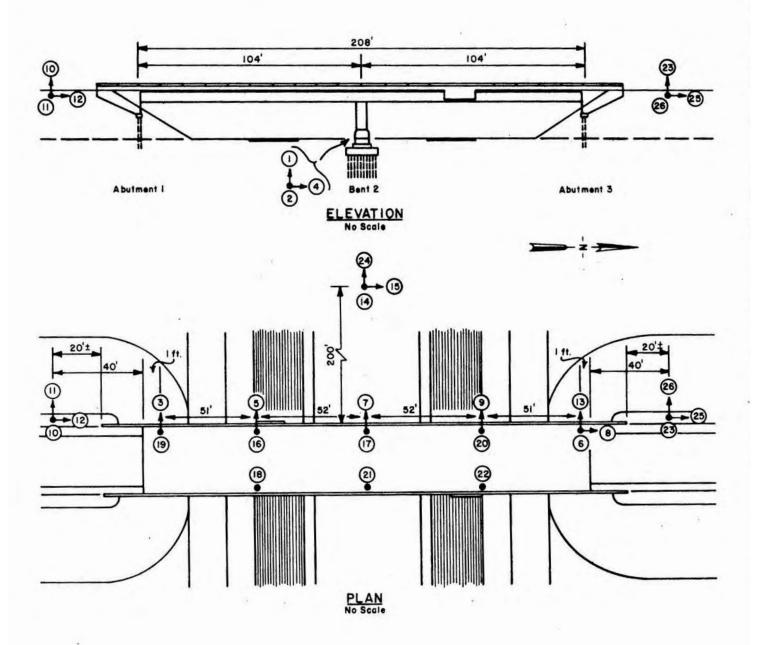


Figure 2

 Location and orientation of recording channels at El Centro Route 8/ Meloland overpass bridge.

#### Meloland Overpass Bridge

The Meloland overpass bridge on Route 8 (CDMG Station No. 01336) is made up of two spans of continuous, reinforced concrete, three-cell box girder that are supported by open-ended diaphragm abutments and a single 5-foot diameter reinforced concrete column, all on reinforced concrete piles. The two spans are about 104 feet each and there is no skew (Figure 2). The bridge was designed in 1968-69 by the California Department of Transportation, using the 1968 California Division of Highways criteria. It was built in 1971. The bridge is located approximately 0.5 km southwest of the trace of the Imperial fault and 21.4 km northwest of the epicenter.

In November 1978 the bridge and three adjacent ground sites were instrumented with two 13-channel accelerograph systems. The two systems were installed in accordance with the bridge strong-motion instrumentation guidelines and data analysis procedures developed at the U.S. Geological Survey (Raggett and Rojahn, 1978). The instrumentation is maintained by the CDMG's Office of Strong Motion Studies.

Although both systems operated during the earthquake, only one of the systems (channels 14 through 26) provided a record that was considered complete and of a quality sufficiently high to warrant digitization and processing. The record from the other system (channels 1 through 13) was flawed by several short (fraction of a second) instrument stalls.

Although the bridge sustained no significant structural damage during the earthquake, the strong-motion records from the bridge constitute an important data set. This is the first occasion on which strong-motion data have been obtained from an extensively instrumented structure located less than 1 km from the surface rupture zone of a damaging earthquake. Because of these unusual features several analyses of the recovered records were performed or were underway at the time this report was being prepared for publication (Cramer Lisiecki, 1982; Werner, 1983).

#### Imperial County Services Building

The County services building (CDMG Station No. 01260) was a six-story, reinforced-concrete, frame-and-shear-wall structure supported on concrete piles. It was designed according to the requirements of the 1967 edition of the Uniform Building Code (UBC). The building was completed in 1971.

The building was 125 feet long (five 25-foot-long bays) in the east-west direction, 75 feet wide (three 25-foot-long bays) in the north-south direction, and about 82 two feet high (see Figure 3). Shear walls in the north-south direction and a movement-resisting frame in the east-west direction provided lateral-force resistance. The vertical loads were resisted by reinforced concrete slabs, pan joists, girders and columns.

## IMPERIAL VALLEY EARTHQUAKE 15 OCTOBER 1979 EL CENTRO COUNTY SERVICES BUILDING STRONG-MOTION INSTRUMENTATION SCHEME

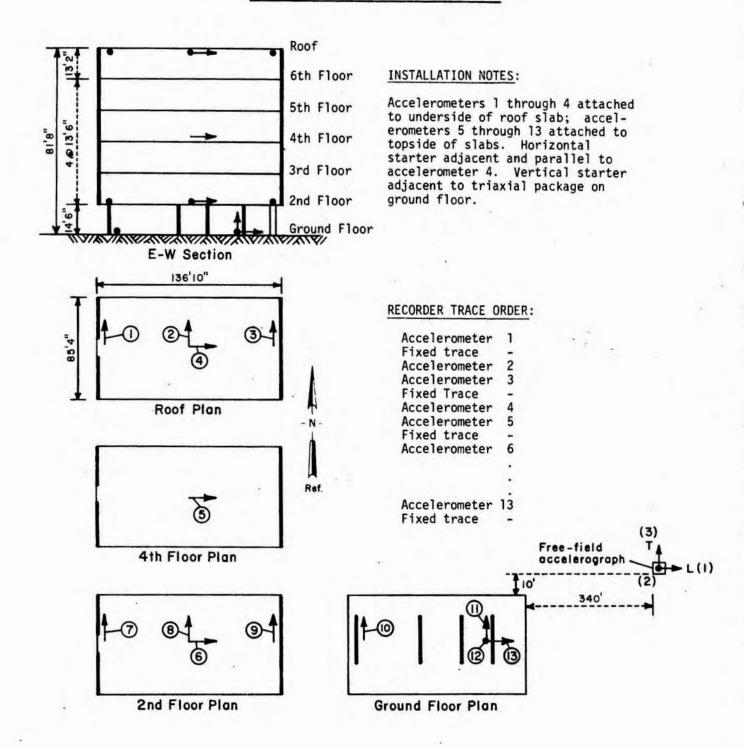


Figure 3

 Location and orientation of recording channels at El Centro Imperial County Services Bldg. Thirteen accelerometers tied into a central recorder were placed as shown on Figure 3. The recorder was equipped with radio-time-signal synchronization.

During the earthquake the building suffered severe structural damage. Its repair was deemed infeasible and the structure was demolished. The strong-motion records recovered from the building after the earthquake represent the first set of records obtained from an extensively instrumented building that sustained major structural damage during an earthquake. For this reason, the records are of considerable interest to scientists and engineers, and numerous studies of building response have been performed (Allawh, 1979; Altman, 1982; Etemadieh, 1982; Hall, 1983; Krieger and Sozen, 1983; and Pauschke and others, 1981).

#### Freefield Station Near the Imperial County Services Building

A triaxial freefield accelerograph mounted on a 1.2 m x 1.2 m concrete pad was located 100 m east of the Imperial County Services Building (CDMG Station No. 01335). During the earthquake this station recorded ground motion. The recorder is equipped with radio-time-signal synchronization.

#### Westmorland and Niland Freefield Stations

Both the Westmorland station (CDMG Station No. 11369) and the Niland station (CDMG Station No. 11023) consist of a SMA-1 recorder mounted on a concrete slab on grade ("free field") inside a one-story fire station building. Both recorders are equipped with radio-time-signal synchronization.

#### RECORDS, DIGITIZATION AND PROCESSING

The six records analyzed in this report were recovered from the instruments within a few days of the event and developed at the CDMG Office of Strong Motion Studies. Copies were made for initial studies and for digitizing. Table 2 lists the data for the stations and instruments. Table 6 includes maximum accelerations scaled from the original records. Components are designated as to the direction (azimuthal if horizontal) of positive instrument case acceleration (that is, ground acceleration if the instrument is measuring ground motion). Positive accelerations, together with positive velocity and displacement in later analyses, are located above the time axis on the original recording and in all plots. Positive directions of horizontal components are indicated in Figures 2 and 3.

Five of the records are 57-58 seconds long because the accelerographs are designed to operate for one minute after trigger. One record is 90 seconds long due apparently to the resetting of the timing circuit by aftershocks. As a consequence of the lengths of the records and their unusual signal content, the standardized programs developed and installed by the U.S. Geological Survey at the computer center of the Lawrence Berkeley Laboratory were modified in three specific ways:

- The maximum processable record length was extended to 60 seconds.
- Angular sensitivities were used to give a more accurate treatment of the behavior of the central recording instruments.
- 3. The corrected data density was doubled from 50 to 100 pts/sec.

The records were digitized from contact prints of the originals by IOM-TOWILL of Santa Clara, California, on a trace-following laser scanner. The digitizer's least count is one micrometer  $(10^{-6}\text{m})$  and its RMS error in digitizing a straight line of the photographic quality of the traces on these records is approximately 10 micrometers (Fletcher and others, 1979). For comparative purposes, the largest peak-to-peak excursions on the original records are approximately 40 mm. Each record was digitized in several sections, or frames, of 10 cm length, and subsequently reassembled to recover a total record duration of approximately 57 seconds (Porter and others, 1979).

Because the width of the CRA records (17.5 cm) recovered at the Meloland overpass and at the Imperial County Services Building exceeded the width of the digitizer work table (6 cm), special handling during digitizing and reassembly of these records was required. The method used is an extension of the one developed for the handling of the 1979 Coyote Lake earthquake records (Porter and others, 1983):

- The record was divided into four panels with three overlap zones. One reference trace was located in each overlap zone and was thus common to each pair of adjacent panels.
- 2. Butting lines were drawn perpendicular to the traces at 9.5 cm intervals from the trace onsets, so that each panel was divided into frames of 10 cm length. Six frames per panel were used in the case of the Meloland overpass record, while nine frames per panel were required to cover the record from the Imperial County Services Building.
- 3. The composite record was synchronized by shifting the panels to match the time coordinates of the first butting line--which incidentally coincided with the time of maximum signal activity. The time shifts (values in square brackets, Tables 2 and 3) varied between 61 and 283 micrometers.

The internal consistency of the method is shown by the relatively small differences (values in parentheses, Table 2 and 3) in the separations between the butting lines as measured in the doubly-digitized overlap zones. In the case of the first and fifth butting lines, the differences ranged between 7 to 91 micrometers. The total separation in this instance is 38 cm; the differences correspond to a maximum of one part in 4200.

Much of the analysis in the first four of the following sections is similar to that of the Caltech data reports (Hudson, 1976) and the data reports of the U.S. Geological Survey since 1971. A brief description is included here of analysis steps or of notations that are not covered in the above.

#### Uncorrected Accelerograms

The digitized reference traces are subtracted from the data traces, and the digitized time marks are used to determine the time scale. The instrument sensitivities scale the ordinates to accelerations. The components are specified by the direction of positive acceleration of the instrument case (that is, ground acceleration, for a ground-level instrument) and this positive acceleration is plotted herein above the time axis. This convention, using azimuthal bearings for horizontal components, has been in effect with the USGS since 1978. Table 6 contains the maximum accelerations for each component from this digitized data.

A special procedure was used where desirable, particularly for the records from the 13-channel central recorders, to remove nonlinearities induced by the recording sytem. This modification takes into account two effects:

The oblique recording of the galvinometers on the film. The
presence of the effect is denoted by the slight deviations from
the perpendicular of the galvinometer light beams for zero
signal. The deviations can be as large as 7-8°, and the
relative correction due to this effect can be as great as 3
percent.

 The differences in sensitivities for positive and negative tilt tests. The differences can range as high as five percent.

This method of calibration was used for the record from the Imperial County Services Building (Table 5).

The theory behind this approach is based on the following assumptions:

a. The angular deflection B of the galvinometer light beam is proportional to the acceleration a,

where B is measured with respect to  $A_0$ , the calibration angle for zero signal.  $A_0$  is measured with respect to the normal to the film.

 The factor of proportionality k contains an additional small dependence on the acceleration,

$$k = k_0 + k_1 a,$$

where  $k_0$  and  $k_1$  are the zero- and first-order perturbation constants.

c. The film and galvinometer coordinate systems are linked by the relation that the angle for the average amplitude over the entire length of the record is the same as A<sub>O</sub>, the calibration angle for zero signal.

The solutions for the constants in terms of the calibration angles are:

$$k_0 = (B_0^+ + B_0^-)/2g$$

and

$$k_1 = (B_0^+ - B_0^-)2g^2$$
,

where  $B_0^+$  and  $B_0^-$  are the angular deflections for a = +g and a = -g. The formula

$$a = (B/k_0)/[1 + (1 + 4k_1B/k_0^2)^{1/2}]$$

gives the acceleration a for the angular deflection B, while the relation

$$B = arc tan [(D/L) + tan A0] - A0$$

converts the film deflection D into B. L is the distance between the galvinometer and the film. In the case of central recording instruments L = 17.788 cm. For the central recorder in the Imperial County Services Building, separate calculations have shown that the combination of the two effects can produce a resultant correction that can reach 4.2 percent in the case of certain traces.

Discrepancies between values for the peak acceleration when scaled from the original record or from the digitized version are due to two reasons, namely the different interpretation given to the peak's shape by the staff and the laser digitizer (or its operator), and the different placement of the zero acceleration axis by the staff and the computer program removing the mean acceleration value. A discrepancy of 0.02 g corresponds to 0.36 mm on the original film.

#### 2. Corrected Accelerations, Velocities, Displacements

The corrections performed include the following:

- a. High frequency Ormsby filtering (low pass) on data at 200 pts/sec with a ramp falling linearly from 23 to 25 Hz.
- b. Instrument correction using the national period and damping, performed on both 50 and 100 pts/sec data.
- c. The baseline correction using a low frequency Ormsby filter (high-pass) with a ramp rising linearly from 0.03 to 0.17 Hz.
- d. Corrected velocity and displacement, including initial values, are derived during the baseline correction.

The selection of the filter parameters, namely the cutoff frequency  $f_c$  and the roll-off termination frequency  $f_T$ , used in the low-frequency filtering during c. above was based on the following discussion (Basili and Brady, 1978):

a. Low-frequency cut-off f<sub>c</sub>. For the stations closest to the epicenter it was noted that the onset and termination times for the main seismic pulse are 5 sec and 11 sec, respectively. The difference, or duration of the large-amplitude signal, is 6 sec and thus the low-frequency cut-off is

$$f_c = 1/6 \text{ sec} = 0.17 \text{ Hz}.$$

b. Low-frequency termination f<sub>T</sub>. The duration of the active signal portion of the near-epicentral records generally does not exceed 30 sec. Since the processed records are nearly 60 sec long, the usual criterion of not allowing the longest period retained to exceed one-third of the record duration, or 20 sec, can be extended without conflict to include all of the active signal. The low-frequency termination is thus

$$f_T = 1/30 \text{ sec} = 0.03 \text{ hz}.$$

The same filter settings were used throughout the data set to allow the retention of the complete range of frequencies for the stations closest to the epicenter. For the stations furthest removed (Niland and Westmorland, 70 and 53 km epicentral distance, respectively) the corrected displacements exhibit moderate amplitude signals over the entire record length. This persistence is legitimate and not an artifact of the processing technique (Brady and others, 1982).

The corrected accelerations, velocities, and displacements in the plotted data are positive when in the direction of the listed components. The peak values are listed in Table 6.

#### Response Spectra

The linear plots and the tripartite log-log plots of response spectra have been calculated from data at 100 pts/sec, for the slight advantage to be gained in the accuracy of the high frequency components. The Fourier amplitude spectrum appears in the linear plots, calculated at the same period values as the response spectra. The long period content is removed with a ramp starting at 5.9 sec and finishing at 33.3 sec. The data tape contains response spectra calculations at 100 pts/sec.

#### 4. Fourier Spectra by FFT

These spectra are plotted on both linear and log-log axes to accent the particular characteristics at each end of the spectrum. The location of both the low and high frequency ramps are indicated by the positions of  $f_{\rm C}$  and  $f_{\rm T}$  in each case.

#### Duration Spectra

The contour plot of the velocity response envelope spectrum indicates at which times the envelope of the velocity response of a 5 percent-damped oscillator passes through various levels of velocity. The periods of the oscillators chosen are in the range 0.05 to 4 sec and their response for the entire duration of the record is used in preparing the plots. The discrete velocity levels, as defined by the contour intervals, are suitable fractions of the peak velocity response.

The duration spectrum is obtained from this velocity response envelope spectrum by adding the total time for which the velocity envelope is greater than each velocity level. A series of radial straight lines is drawn on this spectrum to indicate the number of cycles of oscillation for any oscillator, so that the duration can be quoted in cycles. Although not labelled specifically, these lines represent 1, 2, 4, 8 ... cycles, as can be readily be seen from the axes. Corrected data at 50 pts/sec were used in these calculations.

#### 6. Spectra of Amplitudes Sustained for Any Given Number of Cycles

From the duration spectra discussed in section 5 it is possible to plot for a duration equal to a particular number of cycles, both the relative displacement response amplitude (or, more specifically, the envelope amplitude) sustained or exceeded and the fraction of the maximum amplitude that this relative displacement amplitude represents.

The required amplitudes are selected from the envelope plot by drawing a horizontal line on the plot with a cumulative length, below the envelope, equal to the number of cycles desired (Perez, 1979). A tripartite description of displacement, velocity, and acceleration amplitudes could also be plotted in the same way the response spectrum is portrayed, assuming only that the response is approximately sinusoidal.

In the plots reproduced here, the topmost curve is the maximum response in the response spectra (explained in section 3) but with 5 percent damping, while under this curve are drawn the curves for the amplitudes sustained for one complete cycle and for 2, 4, 8, 16 and 32 cycles. These additional six spectral curves give a fairly comprehensive coverage for most of the amplitudes that occur during the history of the response. Corrected data at 50 pts/sec were used in calculating these plots.

TABLE 2

EL CENTRO ROUTE 8 / MELOLAND OVERCROSSING RECORD IMPERIAL VALLEY EARTHQUAKE OF 15 OCTOBER 1979 DIGITIZED MEASUREMENTS FROM THE

			-167 (-75)			113 (40)				-36 (-91)				35 (22)		
	Butting Line 5	474312	-167	474479	474489	113	474376	474394	474411	-36	474436	474401	474369	35	474334	474465
	Difference	95964	(-24)	96105	95975	(18)	95953		95899	(-5)	95974		69896	(-71)	92176	
ers)	Butting Line 4	378348	-116 (-24)	378464	378514	91	378423	378468	378512	20 (-2)	378462	378482	378500	-58	378558	378589
Butting Line Intersections and Differences (micrometers	Difference	95190	(-73)	95141	92136	(9-) 89	95173		95185	31 (-24)	92166		95181	(-45)	95207	
)ifferenc	Butting Line 3	283158	-165 (-73)	283323	283318	89	283250	283288	283327	31	283296	283308	283319	-32 (-45)	283351	283439
ections and	Difference	95111	(-4)	95180	95126	(-2)	95133		95172	(-5)	95194		95244	(-25)	95264	
ne Inters	Butting Line 2	188047	96-	188143	188192	75 (-2)	188117	188136	188155	53 (-5)	188102	188088	188075	-12 (-25)	188087	188170
Butting Li	Difference	94639		94643	94657		94655		94694		94696		94595		94620	
	Butting Line 1	93408	s -92	93500	93535	s 73	93462	93462	93461	s . 55	93406	93444	93480	s 13	93467	93474
ence	Time shift	[95]	Difference between panels	0		Difference between panels	[73]			Difference between panels	[128]			Difference between panels	[140]	
Panel Reference Trace		1 1	Difference b	2 1	2	Difference b	3 2	8	4	Difference b	4 4	5	9	Difference b	5 6	7

values in parentheses show the differences in the time coordinate between adjacent panels after the panels are shifted to remove the differences at the first butting line.

Values in square brackets give the shift in the time coordinate needed to synchronize the panels at the

first butting line.

TABLE 3

DIGITIZED MEASUREMENTS FROM THE
EL CENTRO IMPERIAL COUNTY SERVICES BUILDING RECORD
IMPERIAL VALLEY EARTHQUAKE OF 15 OCTOBER 1979

Butting Difference	Butting Line Butting Difference Bu	Butting Line Difference Bu	Butting Line Difference Bu	_	ections and Difference Difference	Difference Butting		es (micromet Difference	ers) Butting	Difference	Butting	
Line 2	Line 1 Line 2	Line 2	Line 2			Line			Line 4		Line 5	
1 [0] 93605 189024 284118	93605 189024	189024			284	284	118		379025		474475	
2 93619 95440 189059 95138 284197	95440 189059 95138	95440 189059 95138	189059 95138	95138		284	197	94903	379100	95440	474540	
Difference between panels 61 50 (-9)	61	61	(6-) 09	(6-) 09	(6-)		52	52 (-8)	45	45 (-16)	54	54 (-1)
2 [61] 93558 95451 189009 95136 28 <sup>4</sup>	93558 95451 189009 95136	95451 189009 95136	189009 95136	95136		787	284145	94910	379055	95431	474486	
3 93579 189041 28	189041	189041			28	28	284210		379126		474555	
4 93601 95474 189075 95202 28	95474 189075 95202	95474 189075 95202	189075 95202	95202		28	284277	94923	379200	95427	474627	
Difference between panels 147 (0)	147	147	147 (0)	147 (0)	(0)		135	135 (-12)	138	138 (-9)	110	110 (-37)
4 [208] 93454 95474 188928 95214 28	93454 95474 188928 95214	95474 188928 95214	188928 95214	95214		28	284142	94920	379062	95455	474517	
5 93470 188952 28	188952	188952	10	10	28	58	284207		379137		474580	
6 93489 95489 188978 95297 28	95489 188978 95297	95489 188978 95297	188978 95297	95297		28	284275	94941	379216	95430	474646	
Difference between panels 74 82 (8)	74 82	74 82	82 (8)	82 (8)	(8)		99	(8-) 99	63	63 (-11)	62	62 (-12)
6 [283] 93415 95481 188896 95313 28	93415 95481 188896 95313	95481 188896 95313	188896 95313	95313		28	284209	94944	379153	95431	474584	
7 93441 188927 28	188927	188927			. 32	- 82	284228		379200		474625	

values in parentheses show the differences in the time coordinate between adjacent panels after the panels are shifted to remove the differences at the first butting line.

values in square brackets give the shift in the time coordinate needed to synchronize the panels at the first butting line.

TABLE 4: STATION DATA AND INSTRUMENT CONSTANTS

S T A	T 1	0 N		ponent	Sensit.	Nat.	Damping	Digitize
NAME	CDMG number	Coordinates	No.	Azim. (degree)	(mm/g)	Freq. (Hz)	fraction	length (sec)
El Centro - Rt 8/Meloland	01336	32.773 N	14	UP	18.1	50.6	.61	58
overcrossing		115.448 W	15	360	17.6	52.3	.66	
overcrossing			16 17	UP UP	17.7	51.7	.63	
			18	UP	17.4 18.0	50.9 52.5	.61	
			19	UP	17.6	52.4	.63	
			20	UP I	17.4	53.3	.62	
			21	UP	18.1	50.7	.64	
			22	UP	18.0*	50.7	.61	
			23	UP	17:5	51.9	.66	
			24	270	17.4	52.8	.64	
			25	360	17.3	50.7	.64	
			26	270	17.1	51.0	.64	
El Centro -	01260	32.793 N	1	360	18.2	52.8	.66	57
Imperial County		115.563 W	2	360	18.4	53.6	.65	
Services Bldg			3	360	17.4	53.2	.63	
	1		4	90	18.4	52.9	.64	
		1	5	90	17.1	50.8	.63	
1		1	6	90	18.2	52.1	.61	
		1	7	360	18.6	54.8	.65	
	1	- 1	8	360	18.2	54.2	.64	
	1		9	360	17.2	51.8	.64	
	1	1	10	360 360	17.4	53.0	.64	
			12	UP	18.4	54.5	.67	
			13	90	18.5	51.5 54.0	.66	
El Centro -	01335	32.793 N	1	92	17.7	26.6	.579	57
Imperial County		115.562 W	. 2	UP	18.4	26.2	.581	
Center - Ground			3	2	17.9	26.6	.627	
Westmorland	11369	33.037 N	1	180	18.4	25.5	.572	57
		115.623 W	2	UP	17.0	25.5	.591	
			3	90	17.2	25.5	.600	
Niland	11023	33.239 N	1	90	17.5	26.7	.559	57
		115.512 W	2	UP	17.6	26.4	.565	
			3	360	18.9	25.8	.575	

<sup>\*</sup> estimated

TABLE 5

Imperial County Services Building

Imperial Valley Earthquake of 15 October 1979

Variable Sensitivities

Trace No.	FBA Sensitivities (mm)	_A°	B+°	B-°
	+18.80			
1	-17.90	7.513	5.854	5.725
	+18.40			
2	-18.50	5.212	5.806	5.947
	+17.50			
3	-17.60	2.859	5.580	5.667
	+18.90			
4	-19.10	5.053	5.965	6.142
	+15.75			
5	-15.80	2.795	5.028	5.088
	+18.00			- 10
6	-18.00	0.403	5.776	5.785
	+18.40		- 0-0	04
7	-18.60	4.021	5.838	5.986
	+18.30			
8	-18.30	1.585	5.855	5.889
	+16.80			4.25
9	-17.20	-0.957	5.405	5.515
	+17.70			
10	-17.80	0.032	5.685	5.653
	+18.70			
11	-18.60	-2.361	6.020	5.936
	L(+)-18.90,T(+)-17.70		1 411 4	
12	L(-)-18.60,T(-)-19.50	-4.525	5.980*	5.980
	+18.10	2 502	Carrolle.	- 01-
13	-18.80	-7.260	5.794	5.863

<sup>\*</sup> assumed value, because the tilt test for this component could not be performed (vertical orientation).

TABLE 6: PEAK VALUES OF PROCESSED DATA

STATION	COM	PONENT	MAX	. ACCELERAT	ION	MAX. VELOCITY	MAX. D.	
	Number	Orientation	scaled (g)	digitized (g)	corrected (cm/sec <sup>2</sup> )	(cm/sec)	(cm)	
El Centro -	14	UP	.231	.256	225.1	29.34	8.93	
Rt 8/Meloland	15	360°	.318	.318	305.0	71.65	21.53	
overcrossing	16	UP	.503	.485	472.0	37.19	8.31	
	17	UP	.225	.231	223.9	30.32	8.47	
	18	UP	.443	.448	428.6	35.24	8.63	
	19	UP	.212	.210	200.4	28.46	8.25	
	20	UP	.447	.449	450.9	36.70	8.67	
	21	UP	.229	.273	261.8	34.61	9.92	
	22	UP	.408	.400	392.4	30.43	7.68	
	23	UP	.251	.241	227.1	28.77	8.09	
	24	270°	.296	.297	292.7	90.94	32.57	
	25	360°	. 350	.348	332.9	79.58	22.32	
	26	270°	.385	. 384	375.8	96.53	37.55	
El Centro -	1	360°	.557	.546	531.3	62.80	17.36	
Imperial County	2	360°	.565	.566	551.6	63.55	17.58	
Services Bldg	3	360°	.588	.584	569.4	72.54	18.92	
	4	90°	.481	.460	443.9	98.14	33.46	
1	5	90°	.260	.274	258.2	83.32	29.57	
	6	90°	.291	. 285	268.5	74.88	28.48	
	7	360°	.358	.363	355.8	44.72	16.98	
	8	360°	.319	. 316	307.4	45.67	17.06	
	9	360°	.767	.645	641.9	51.53	14.50	
	10	360°	. 347	.337	330.6	43.26	14.52	
N A	11	360°	.291	.290	284.0	42.42	16.04	
	12	UP	. 186	. 184	174.3	16.19	7.01	
	13	90°	. 319	.327	325.0	64.59	27.41	
El Centro -	1	92°	.237	.237	231.4	64.38	28.24	
Imperial County	2	UP	.266	.251	230.9	17.40	7.98	
Center - Ground	3	2°	.243	.213	209.0	36.20	16.43	
Westmorland	1	180°	. 106	. 112	107.4	21.13	7.44	
	2 3	UP	.085	.086	84.4	7.09	2.59	
	_ 3	90°	.081	.076	73.0	19.79	12.35	
2000	1	180°	. 161	. 156	141.8	10.14	12.35 2.62	
aftershock*	2	UP	. 120	.117	94.5	2.79	0.92	
.  _	_ 3	90°	.088	.114	110.0	11.44	6.14	
Ni land	1	90°	. 100	.111	106.1	12.16	5.30	
	2	UP	.028	.035	33.2	3.95	1.93	
	3	360°	.074	.070	66.3	8.04	4.01	

<sup>\*</sup> Time of Aftershock recorded by Westmorland station is unknown.

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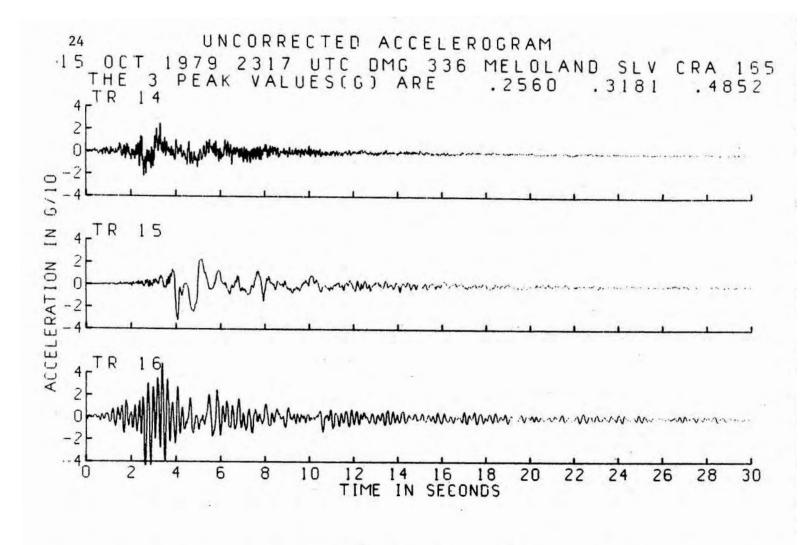
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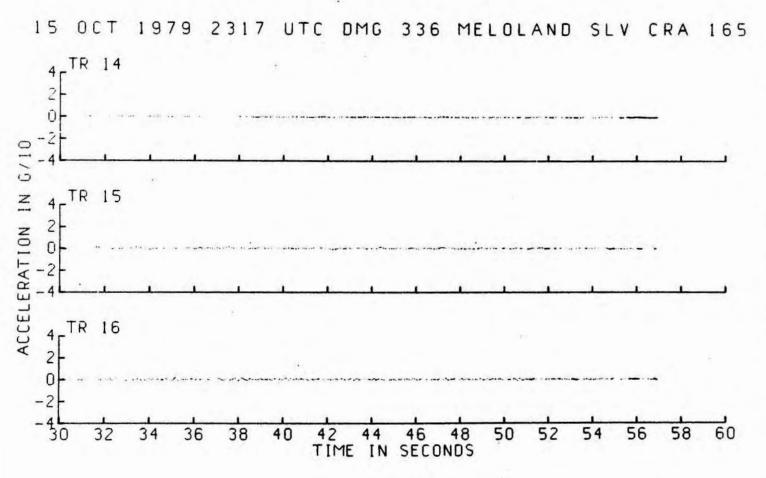
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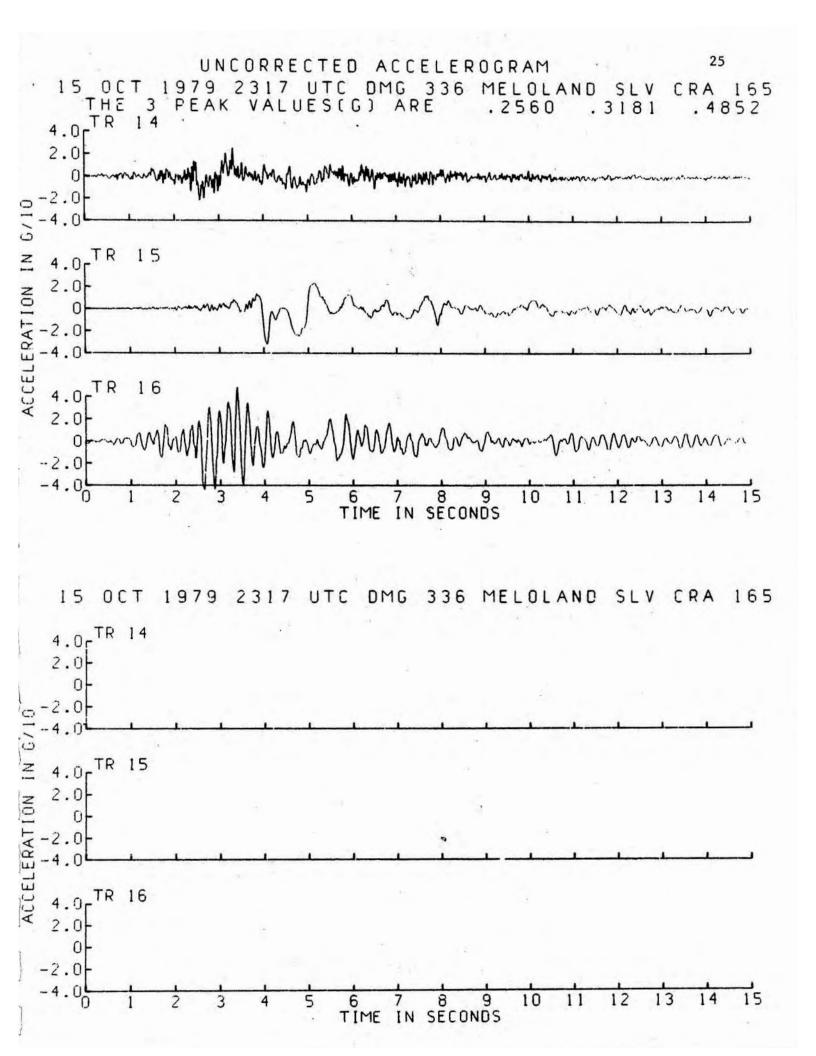
#### APPENDIX

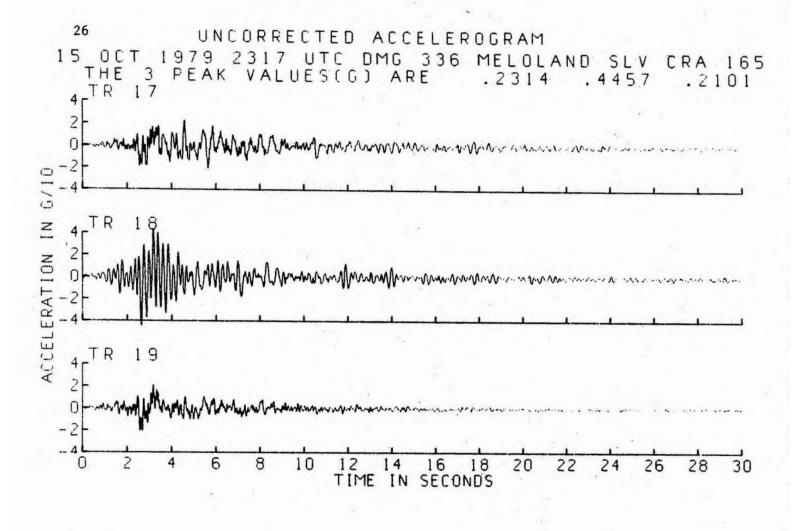
The appendix contains computer plots of the following processings of each accelerogram:

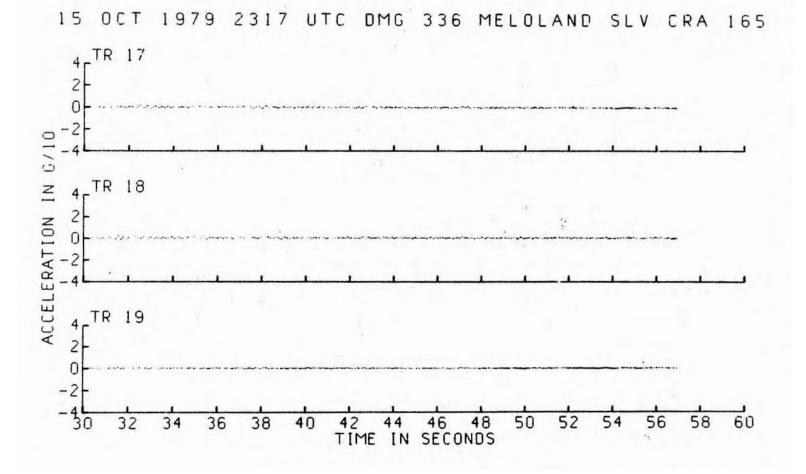
uncorrected accelerogram (57 or 58 sec. and 15 sec. duration);
corrected acceleration, velocity and displacement (56 sec. duration);
response spectrum (tripartite);
Fourier amplitude spectrum (log scale and linear scale).
duration spectra
spectra of amplitudes sustained for any given number of cycles

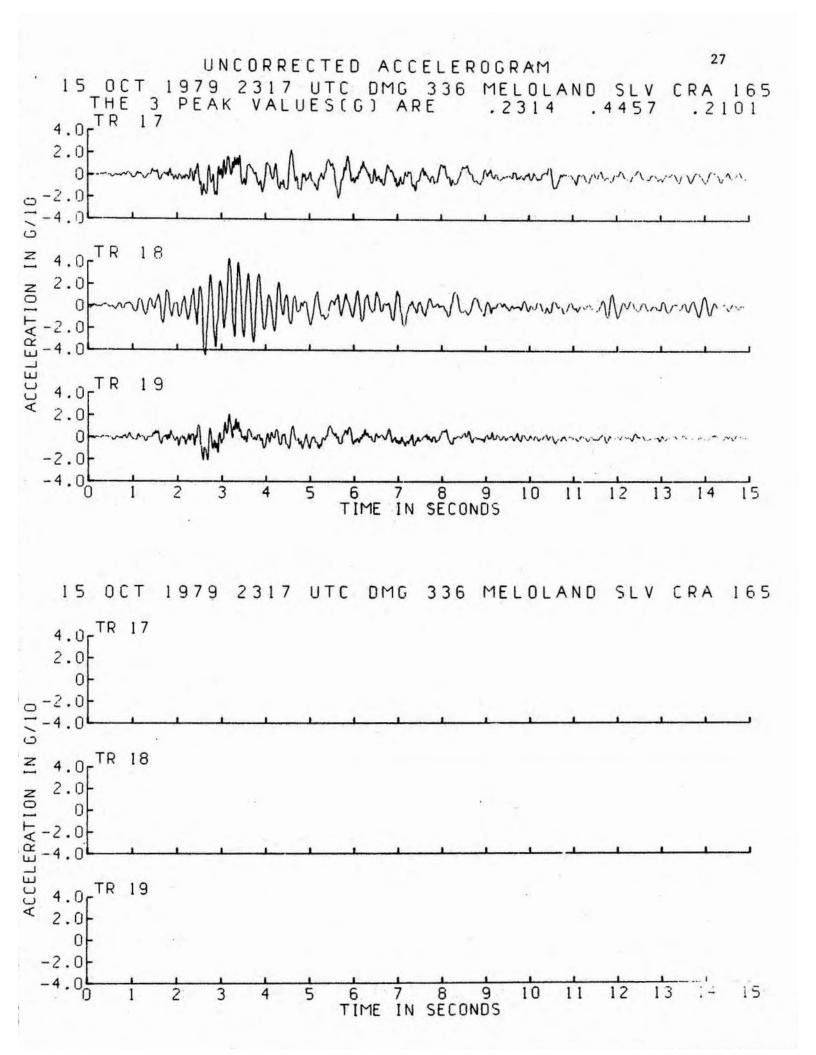


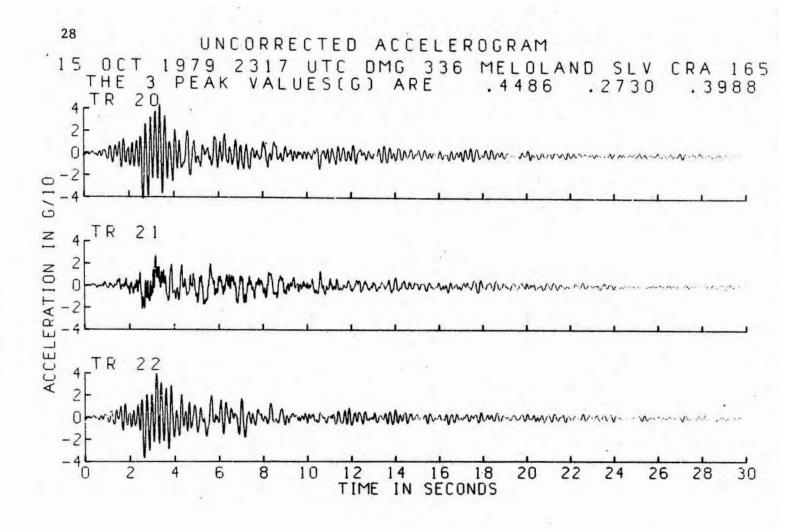


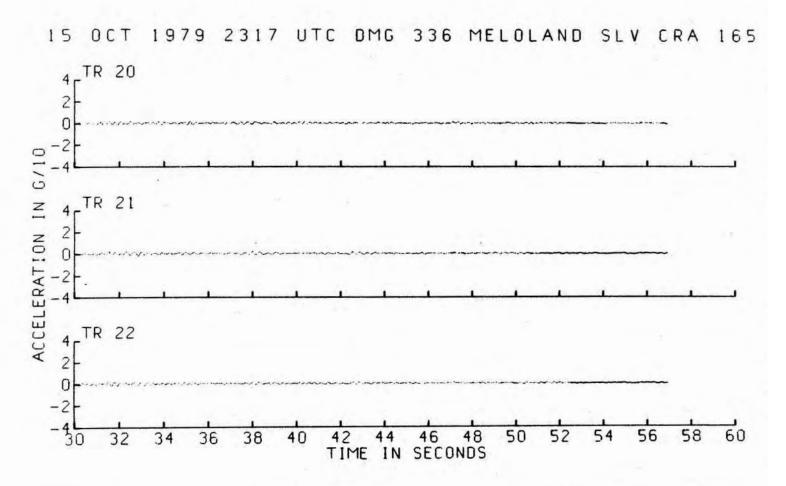


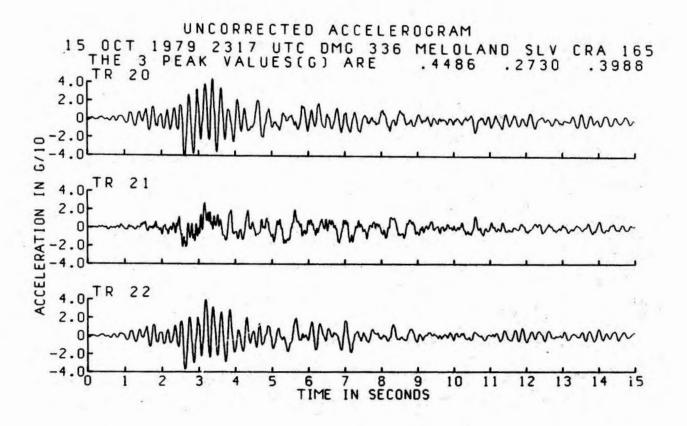


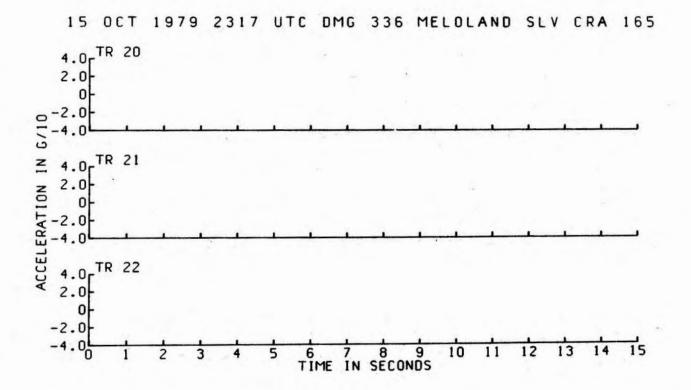


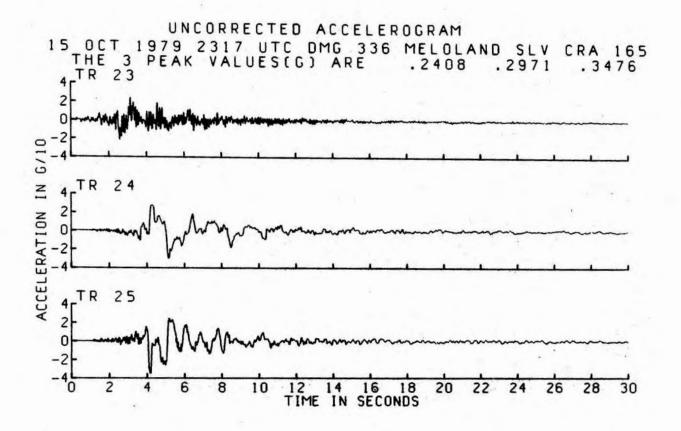




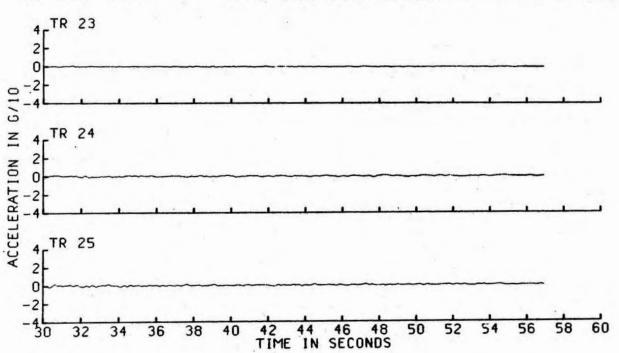


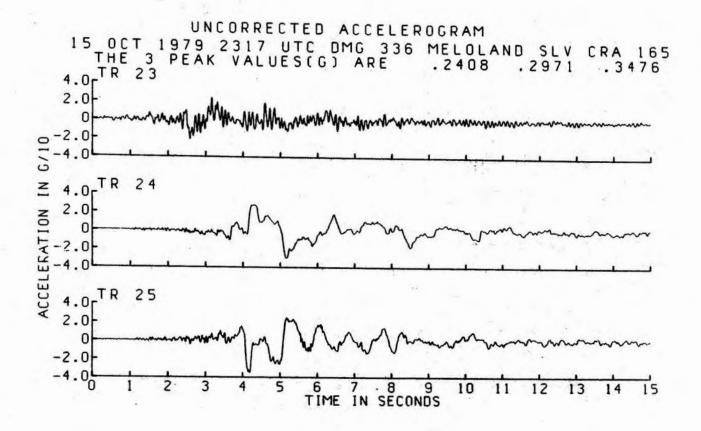


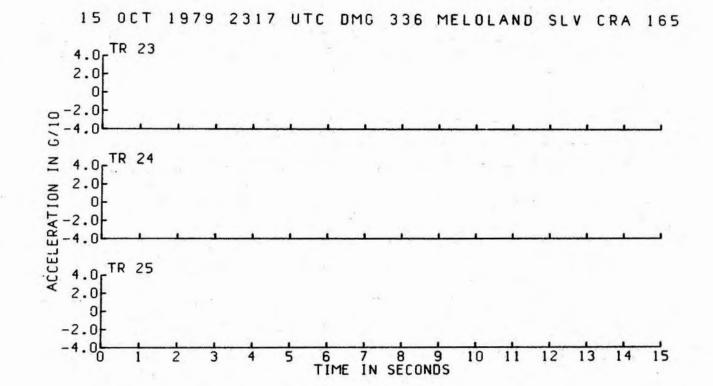




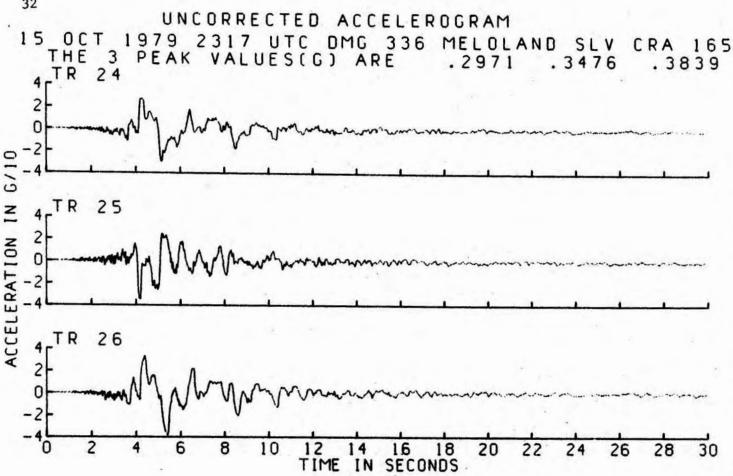


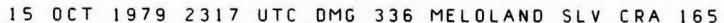


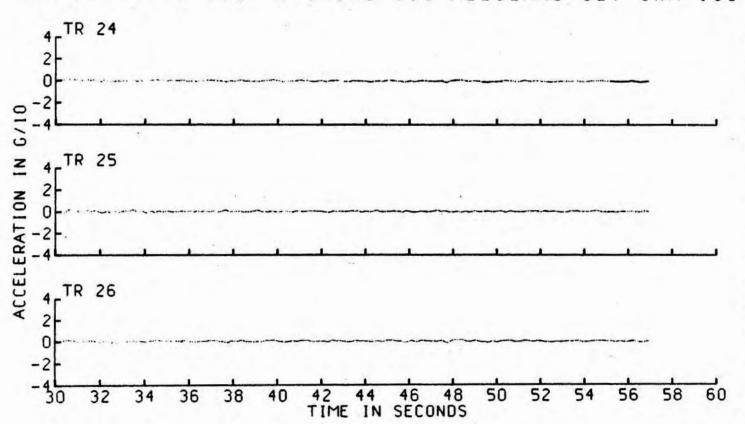


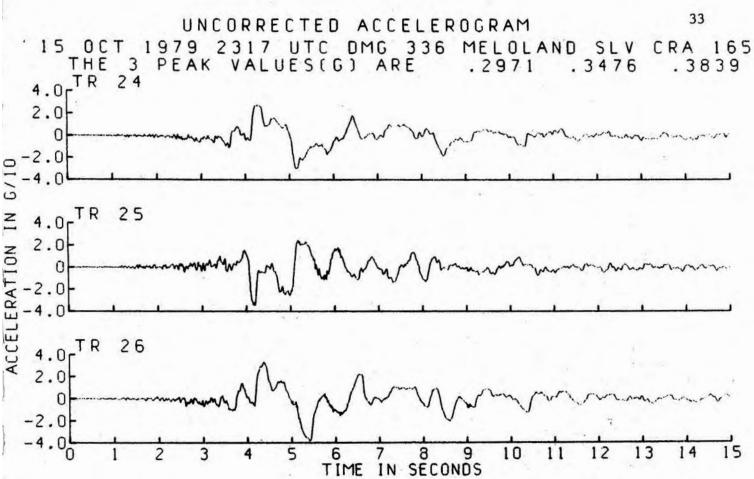


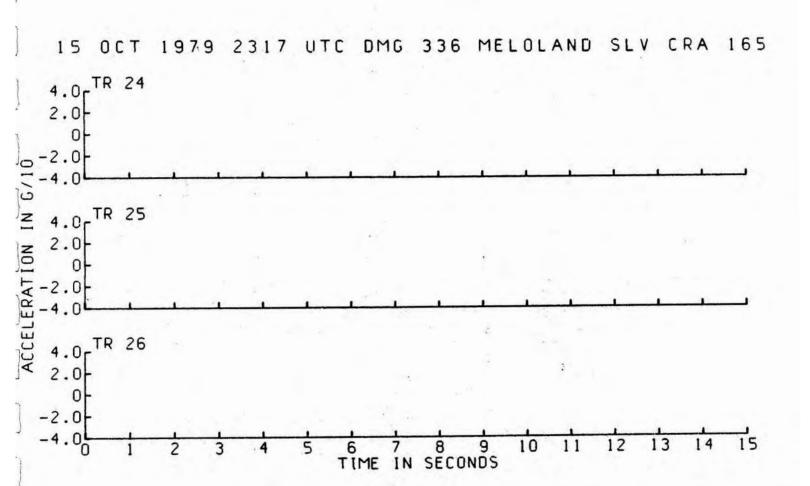


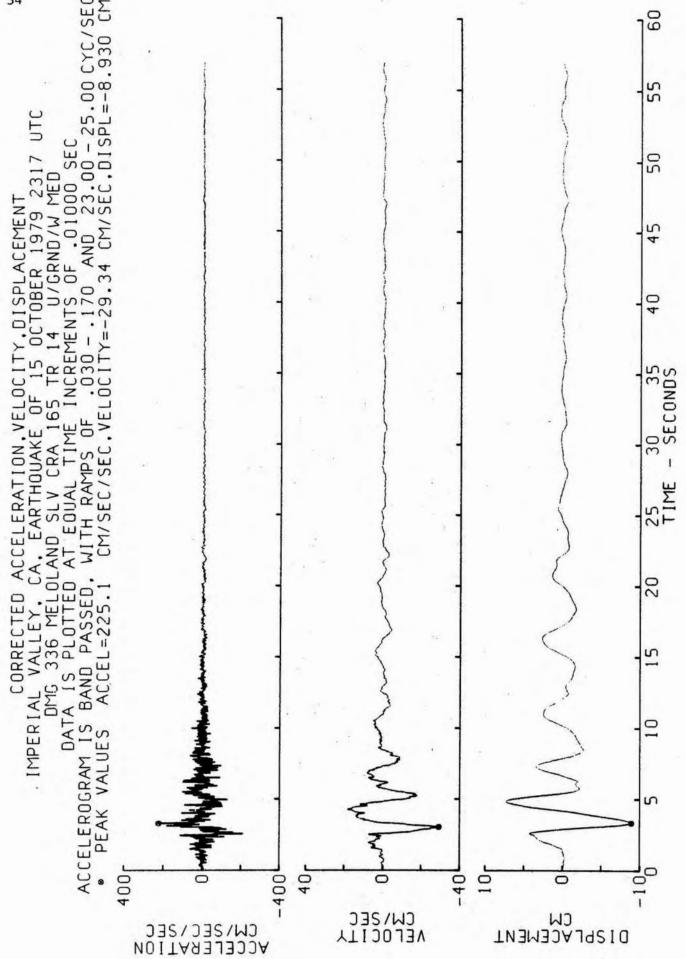






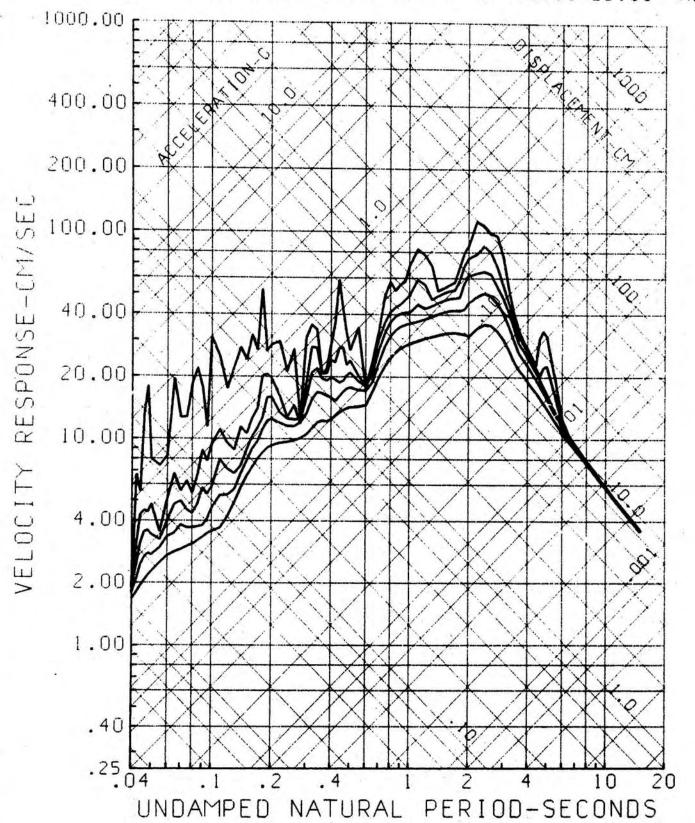


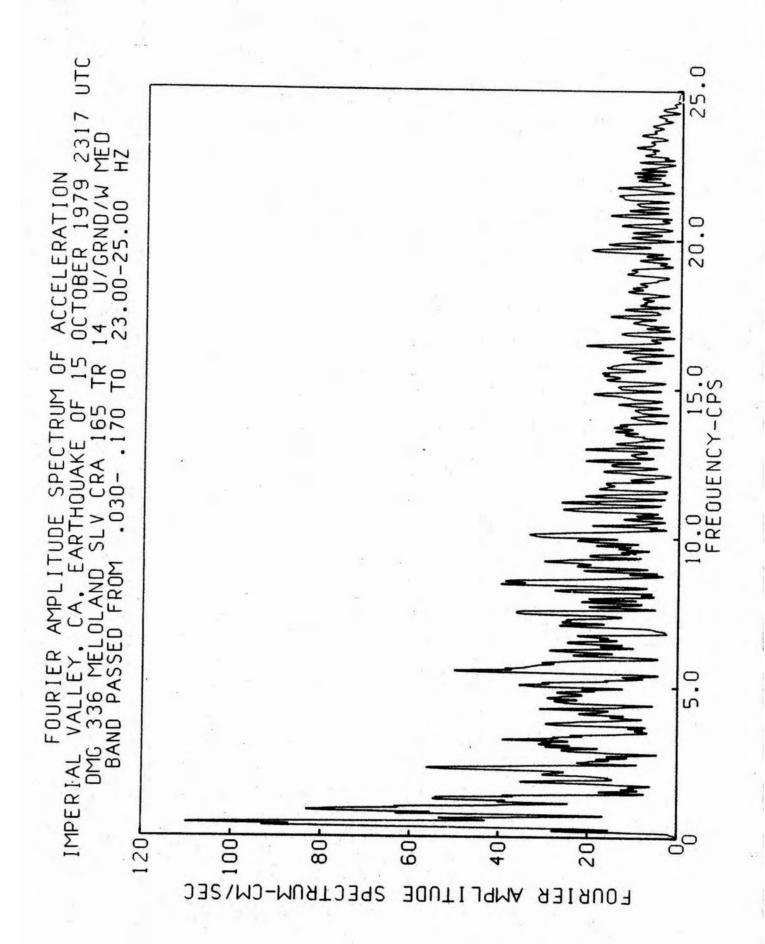


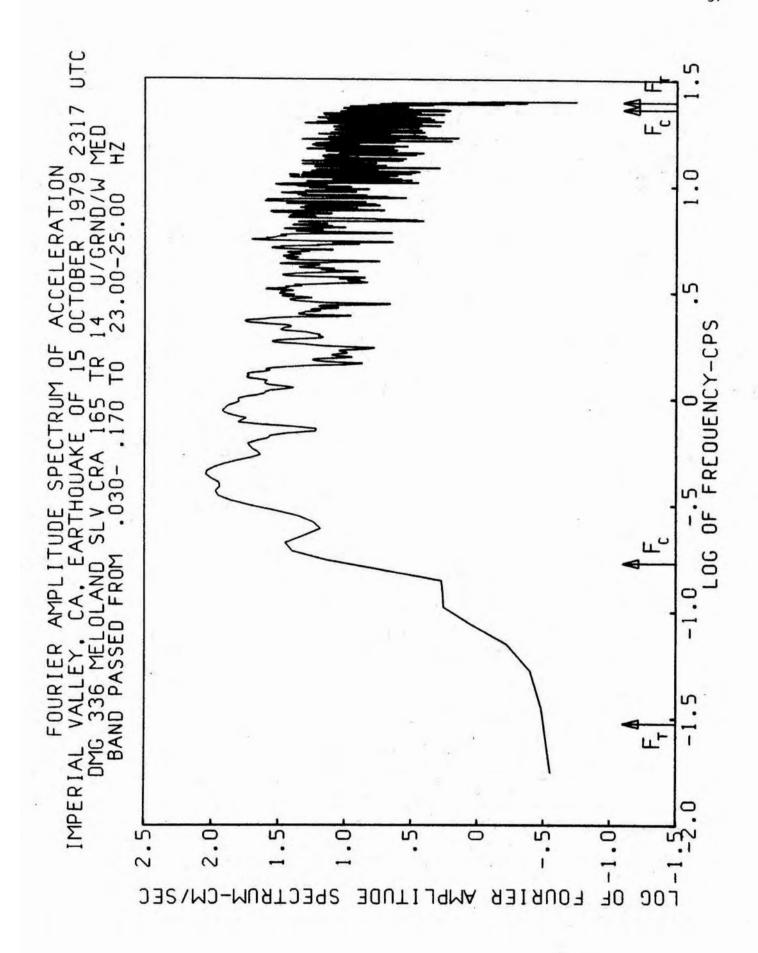


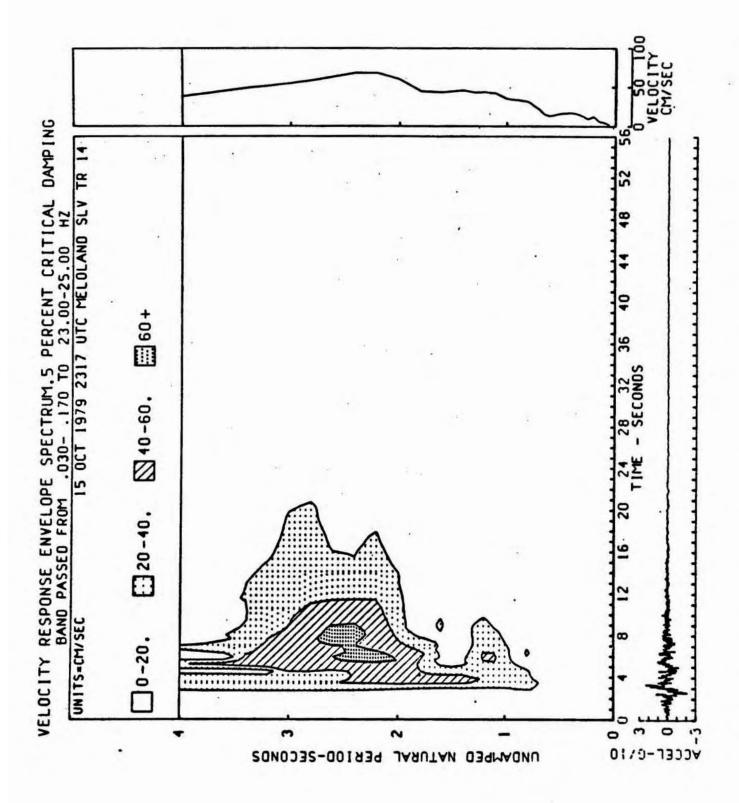
RESPONSE SPECTRA

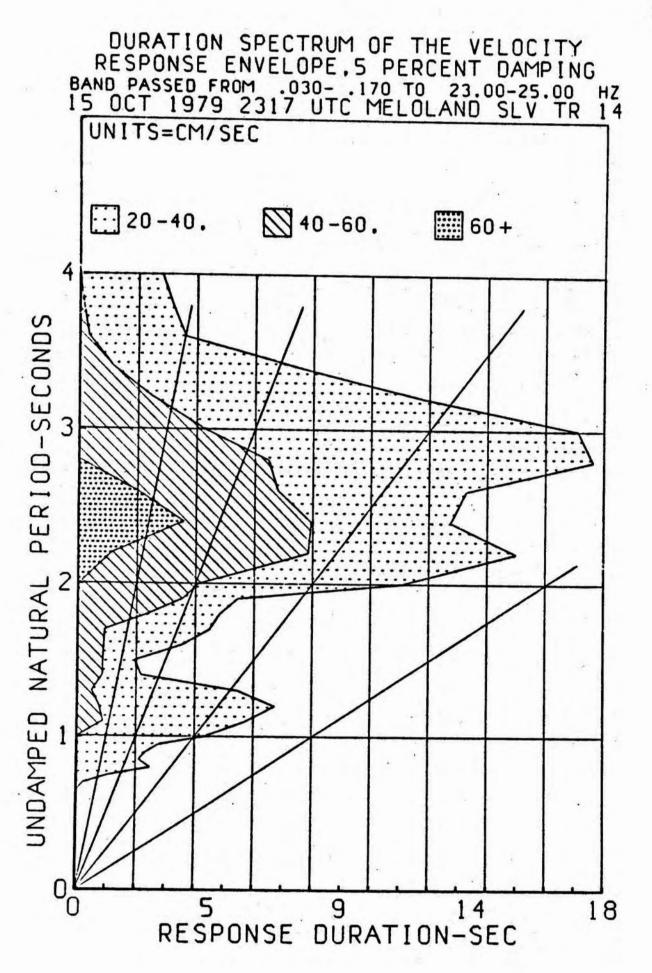
15 OCT 1979 2317 UTC MELOLAND SLV TR 14 0.2.5.10,20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



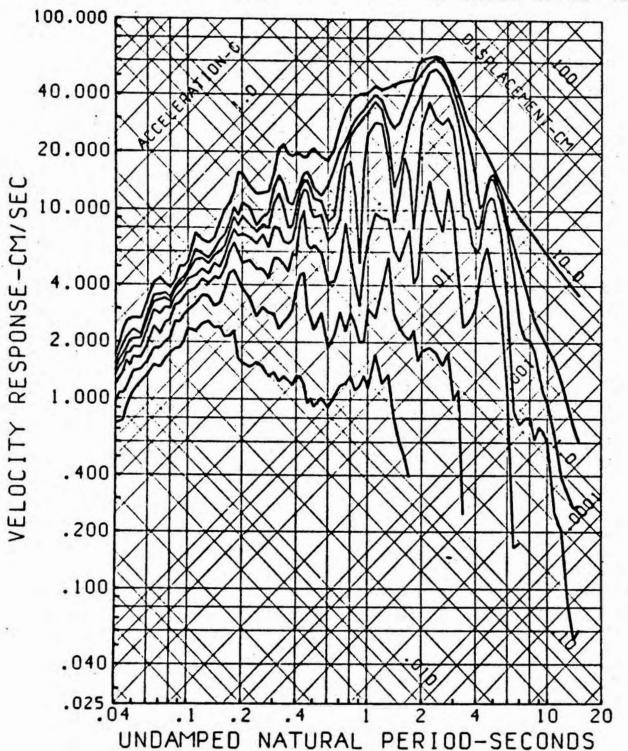


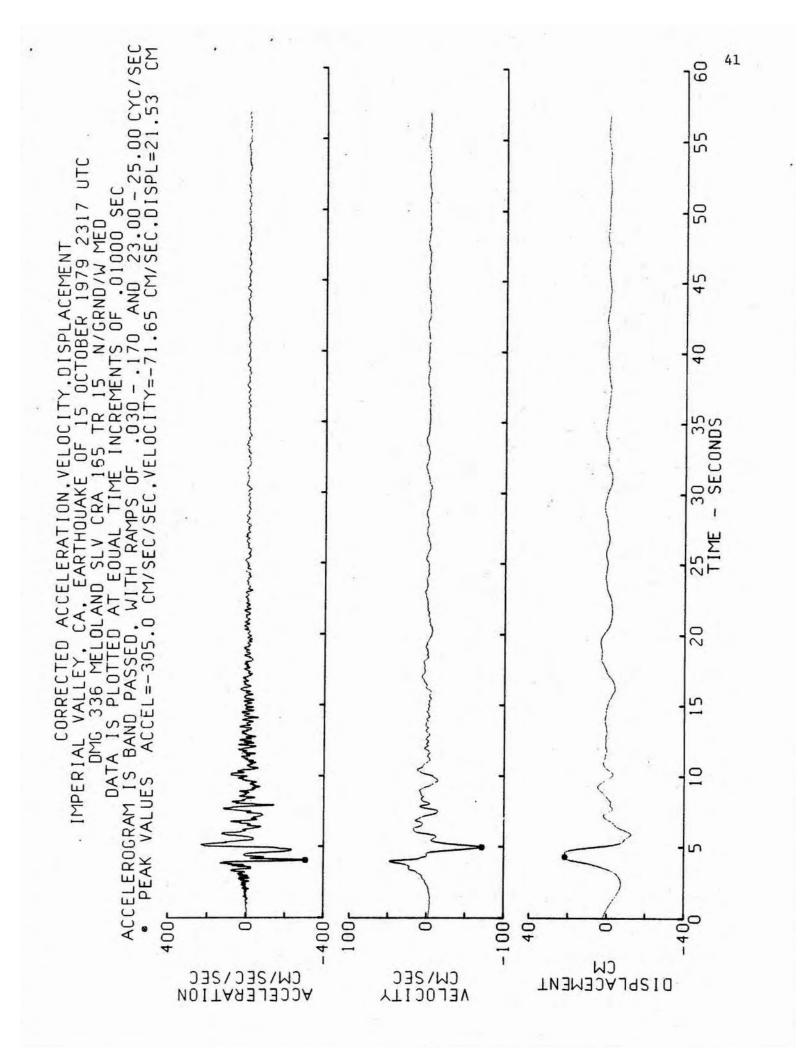




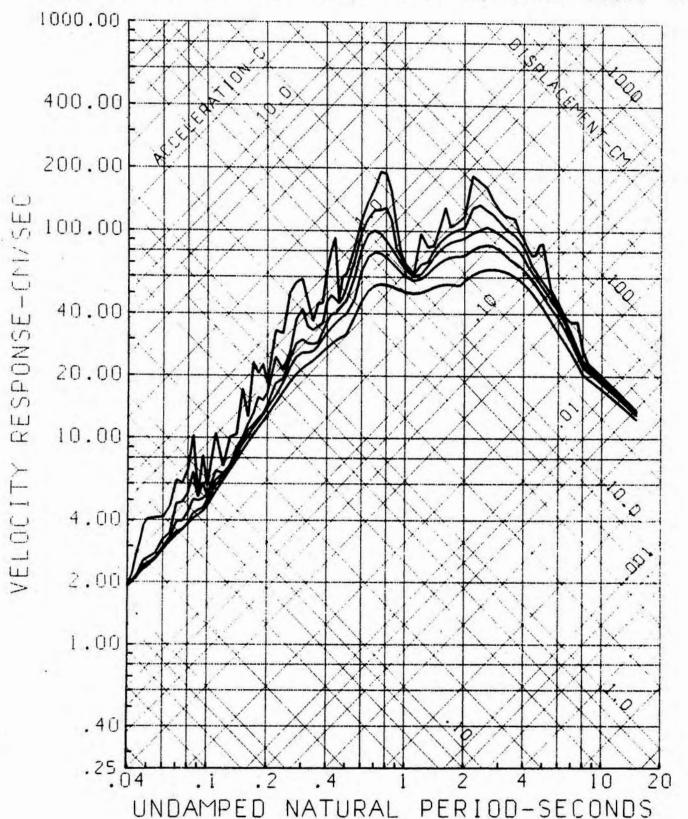


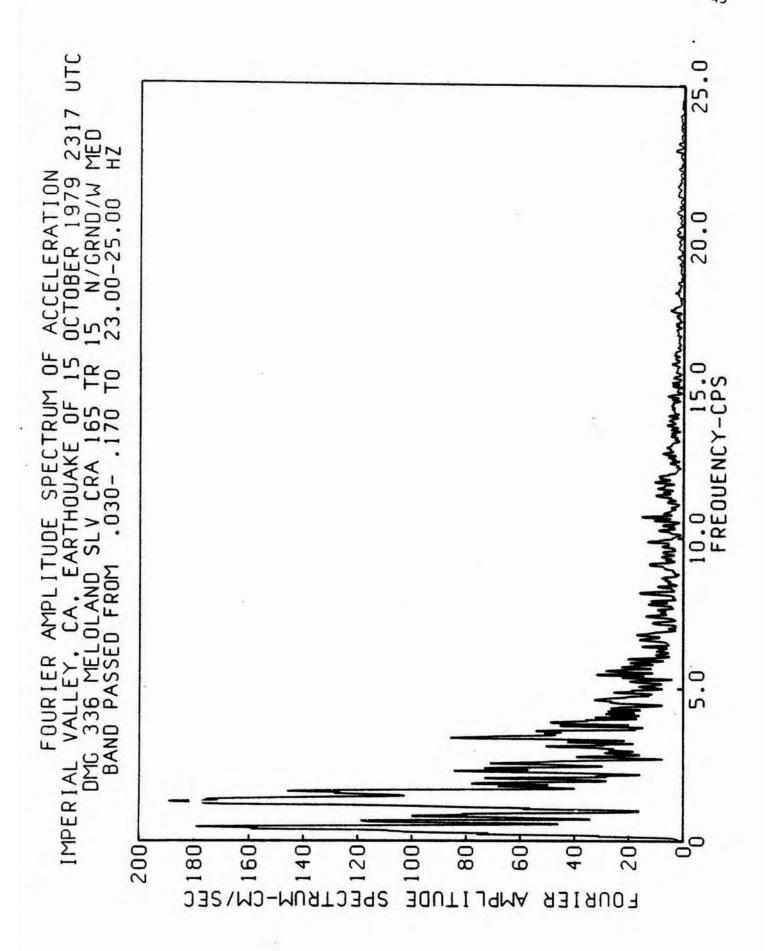
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 14 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

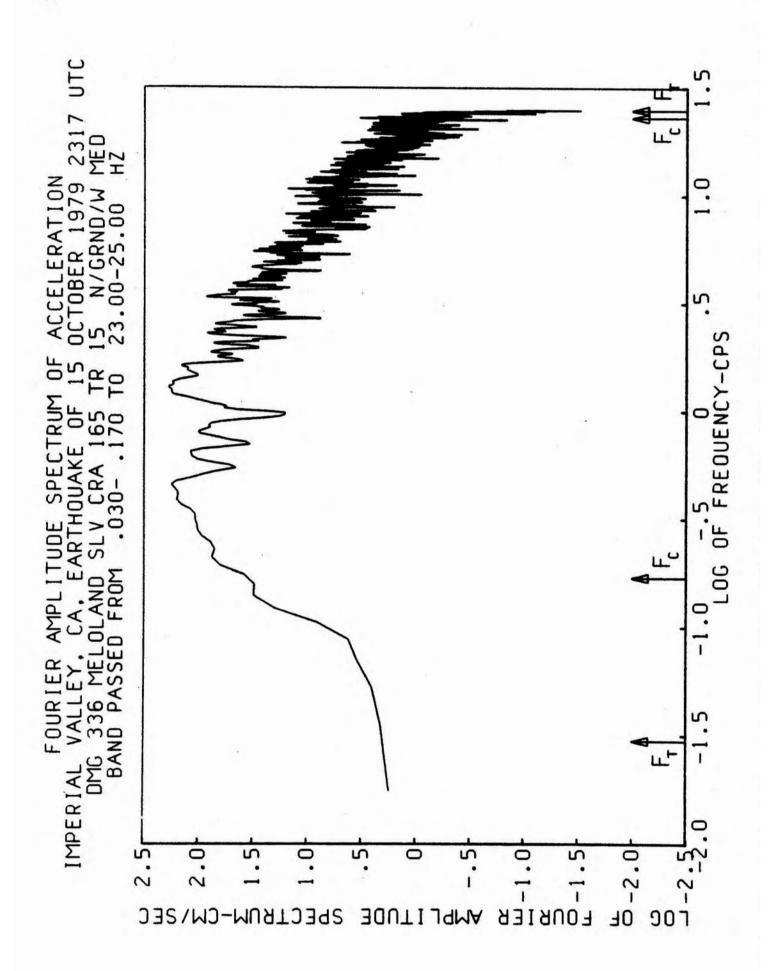


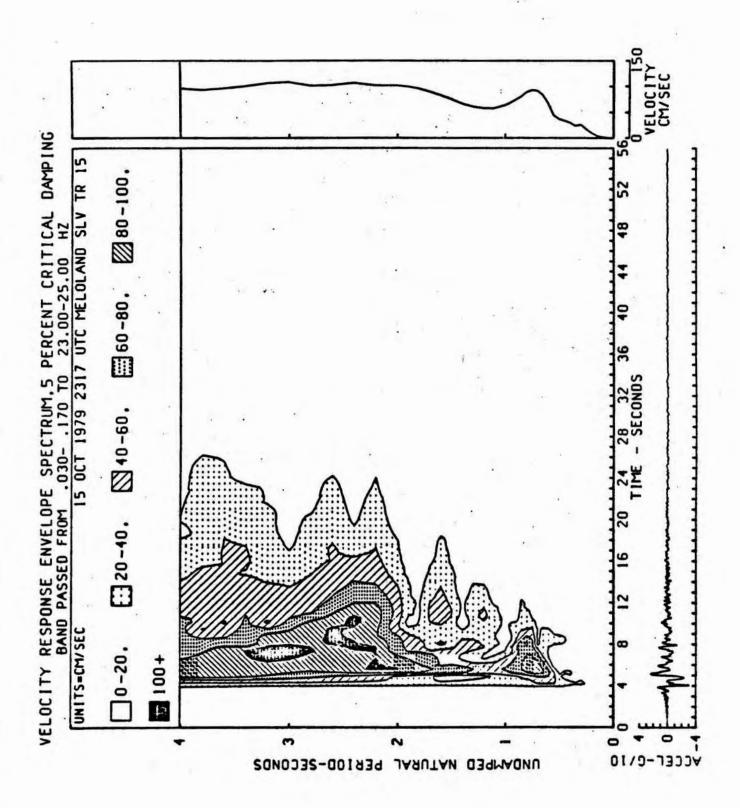


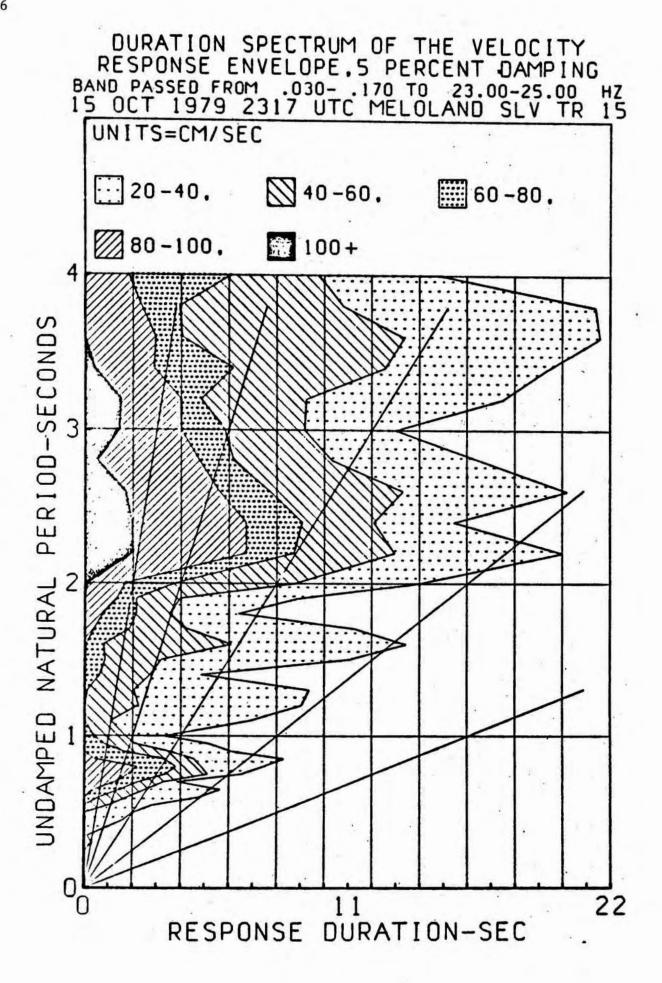
RESPONSE SPECTRA
15 OCT 1979 2317 UTC MELOLAND SLV TR 15
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



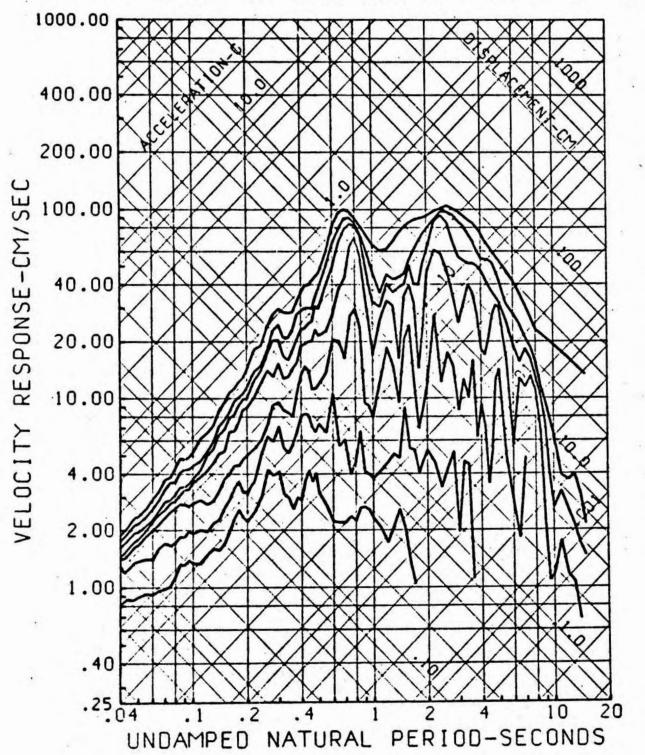








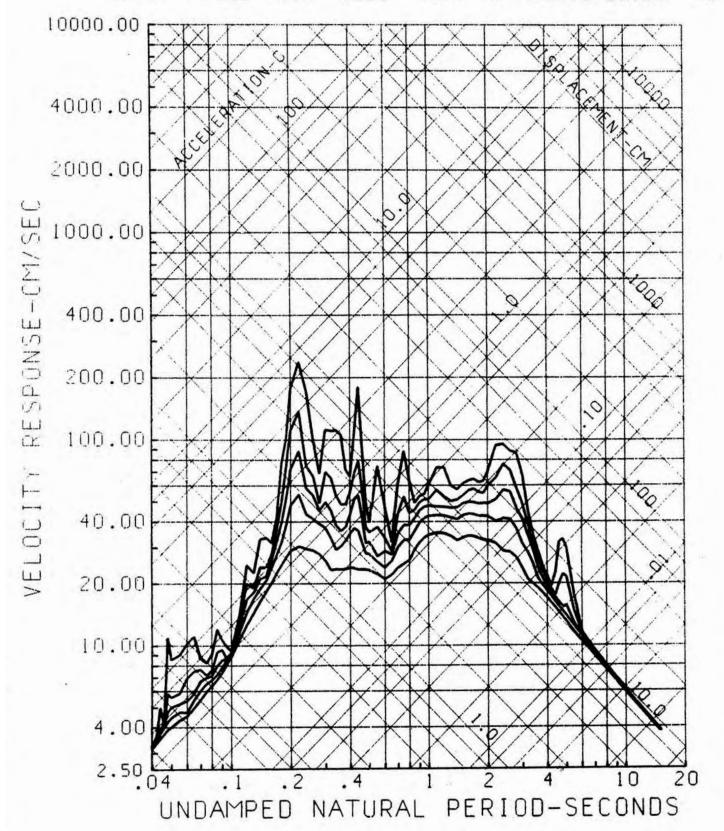
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 15 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

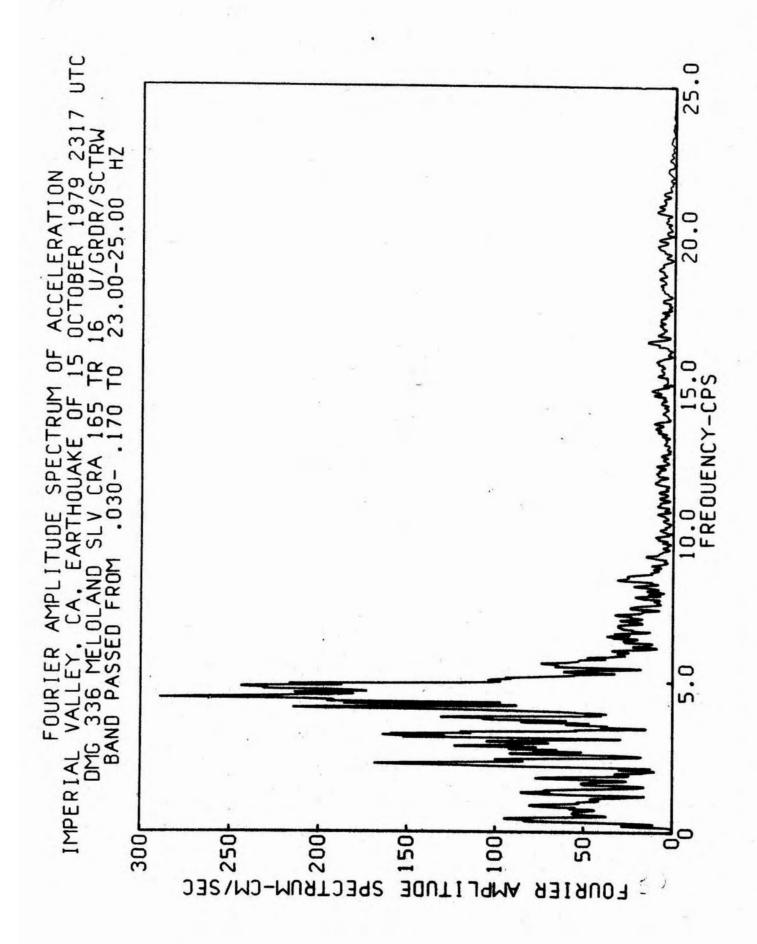


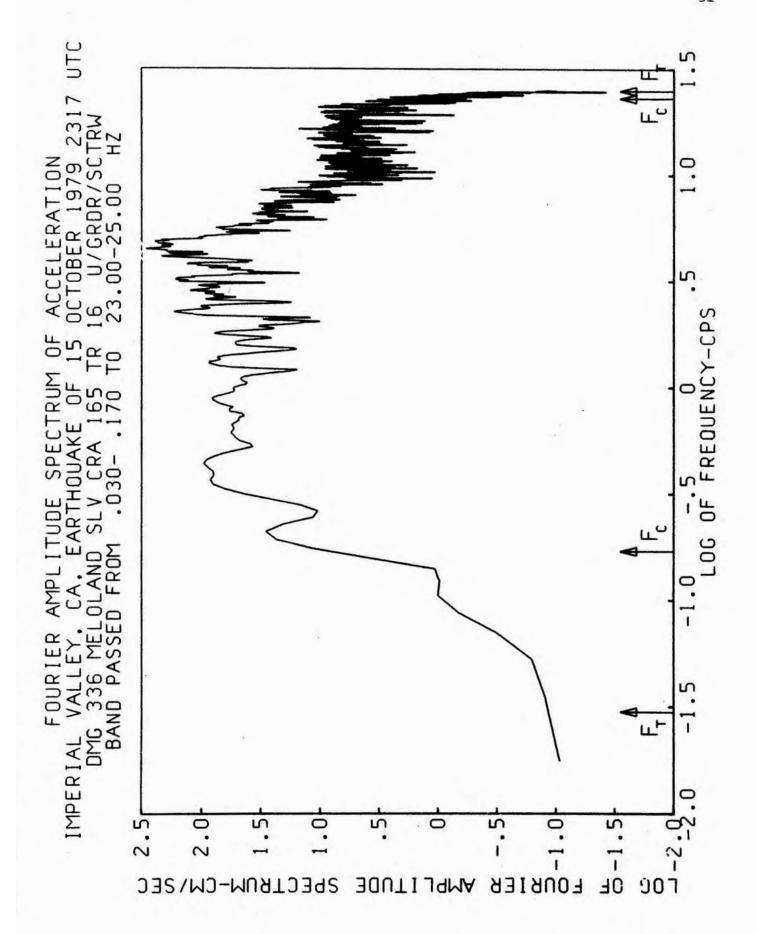
ACCELERATION CM/SEC/SEC

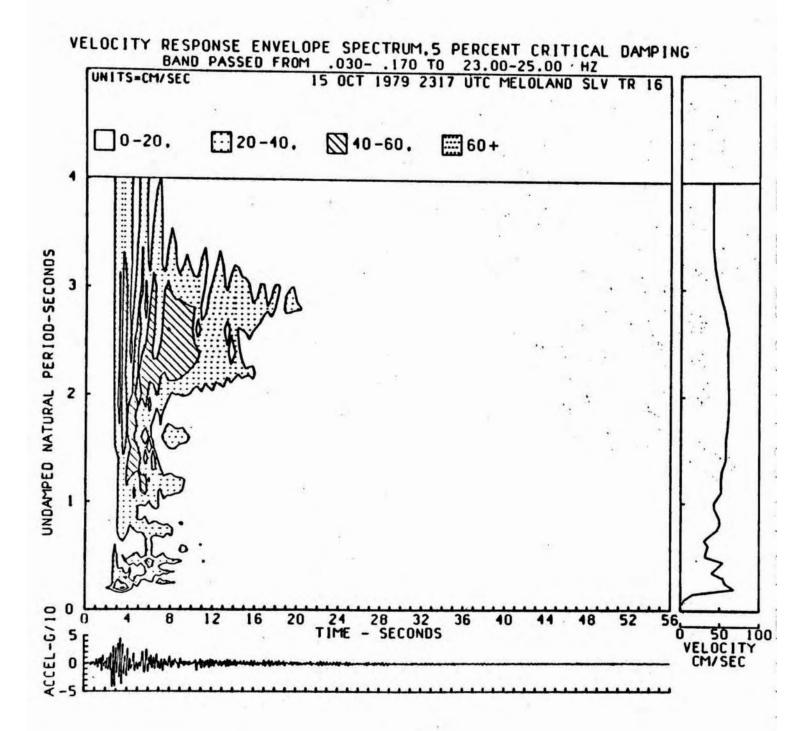
RESPONSE SPECTRA

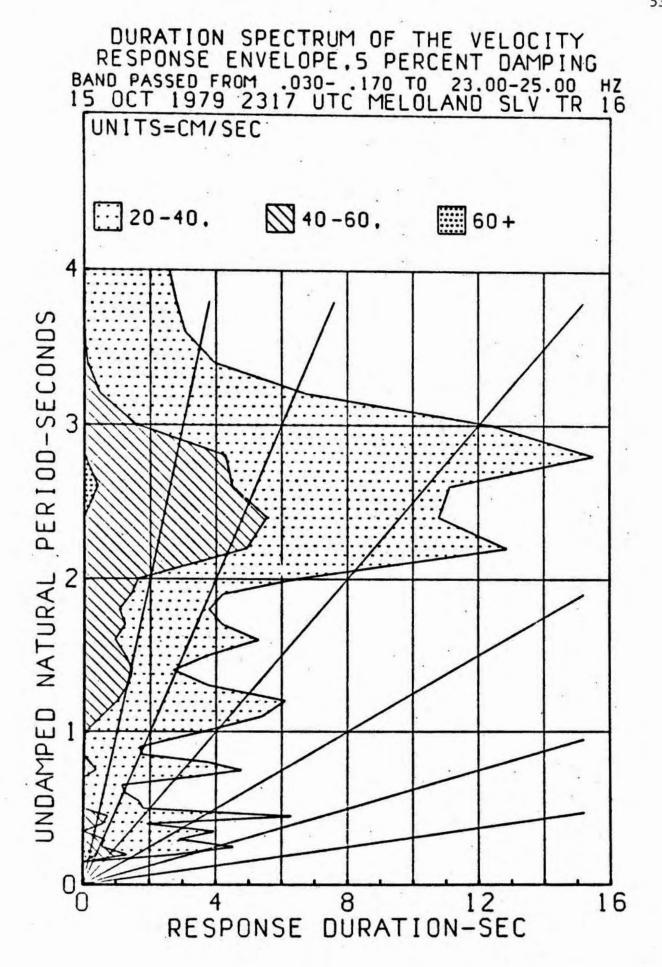
15 OCT 1979 2317 UTC MELOLAND SLV TR 16 0.2,5,10,20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



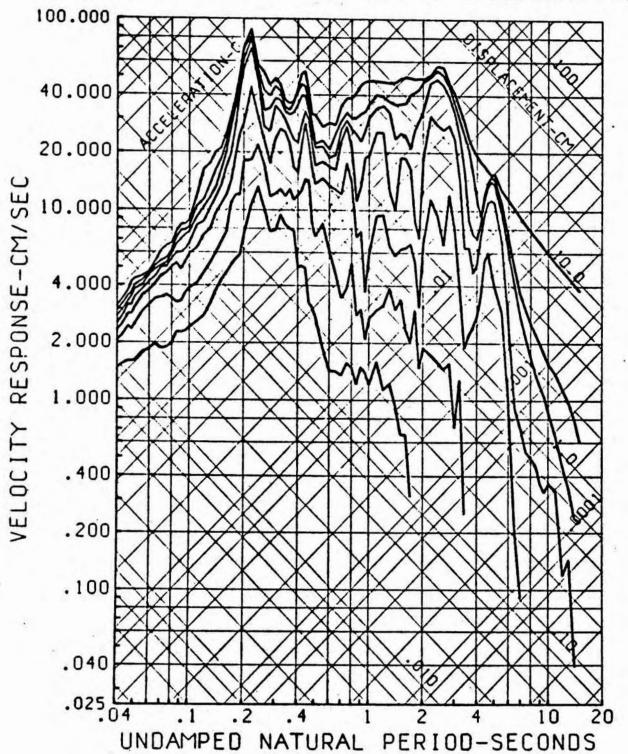


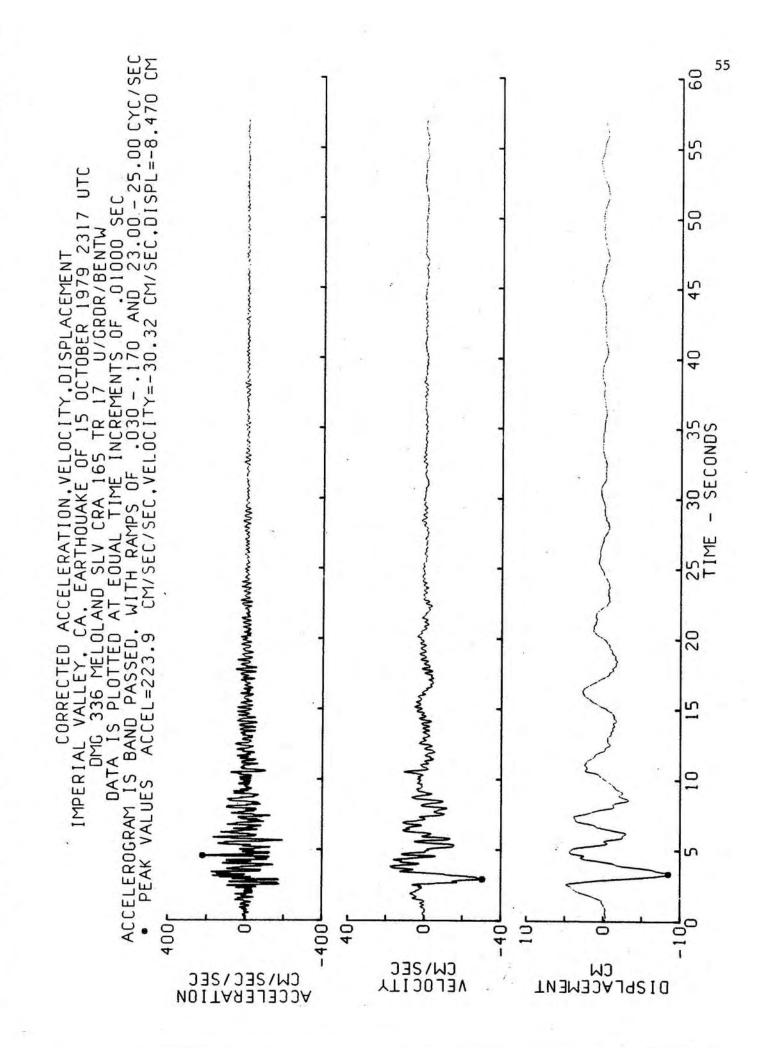






SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 16 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

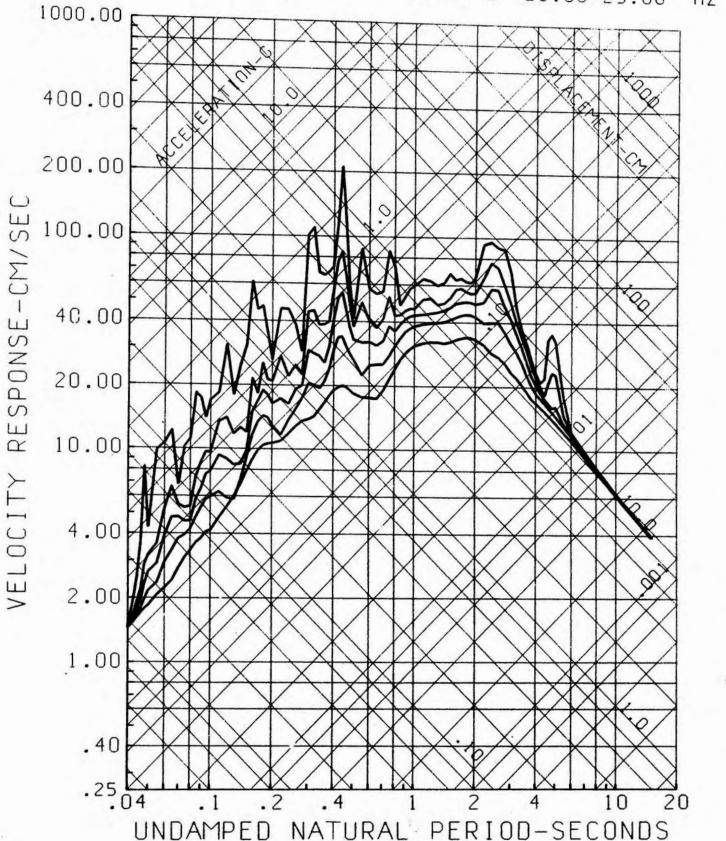


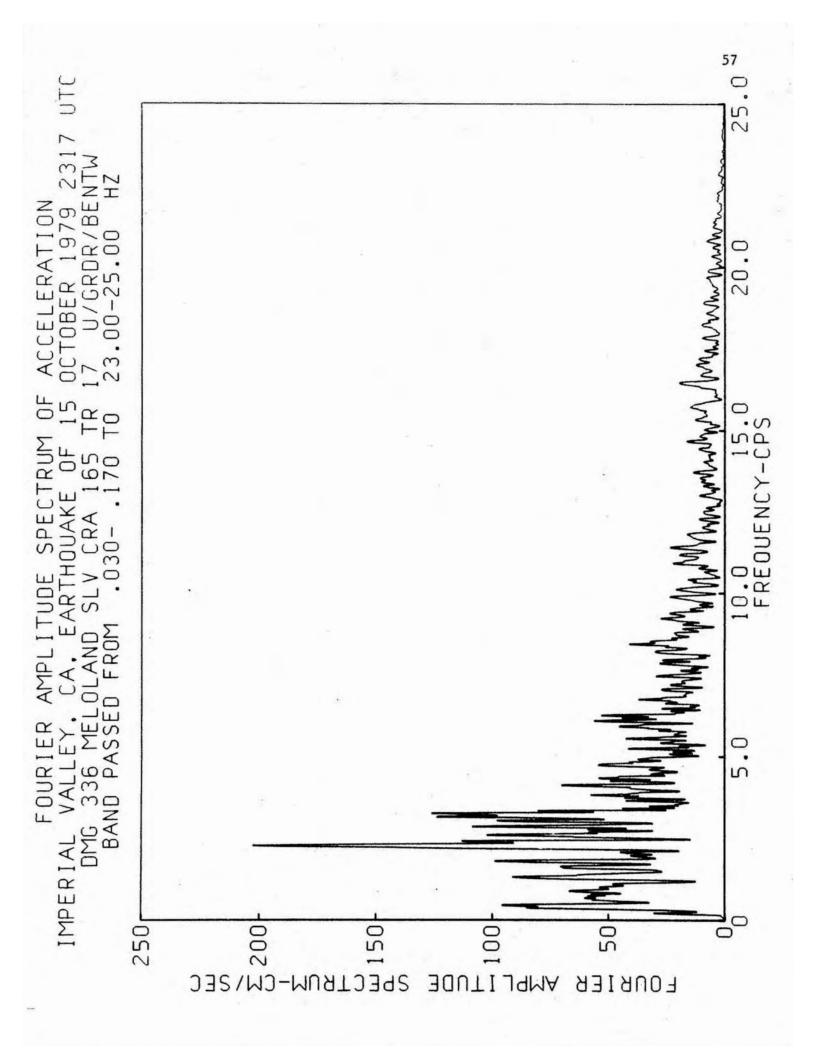


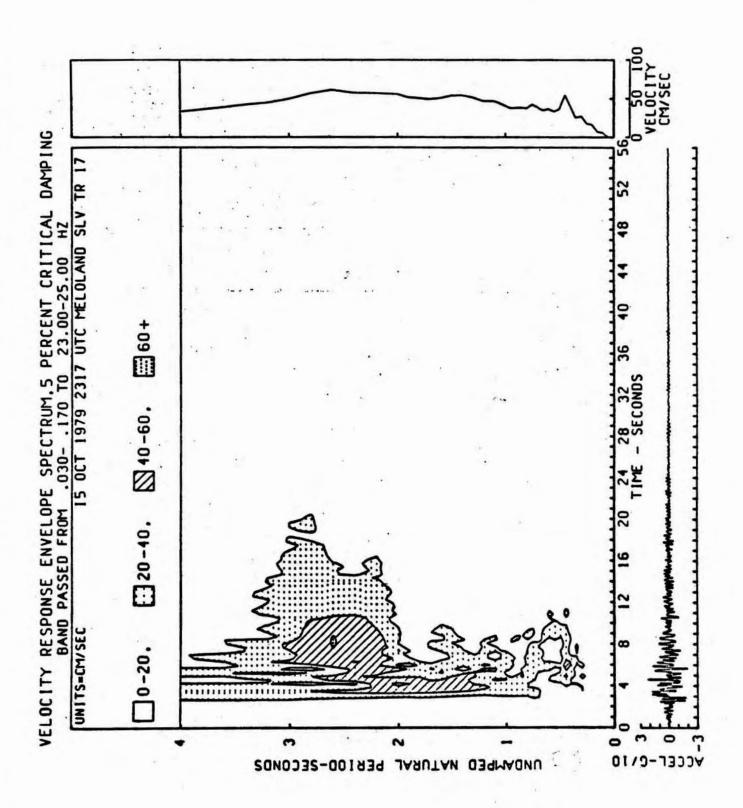
RESPONSE SPECTRA

15 OCT 1979 2317 UTC MELULAND SLV TR 17

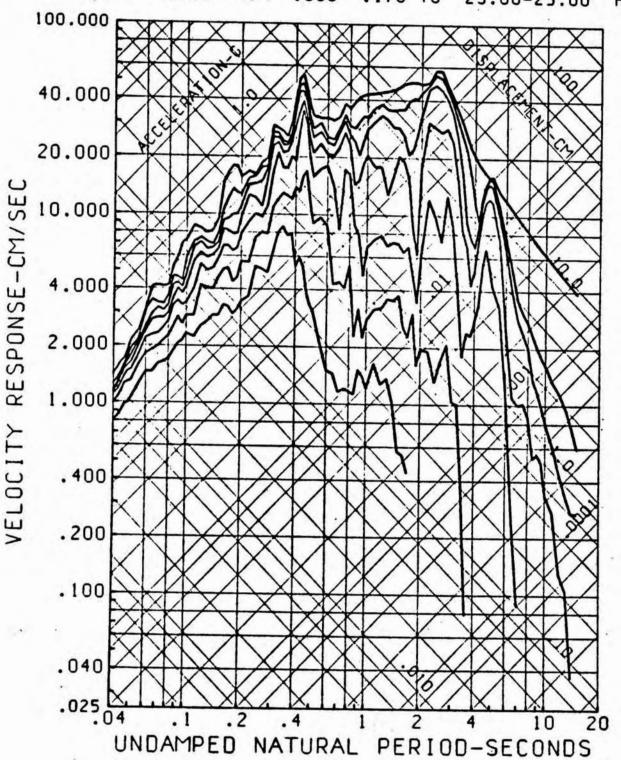
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

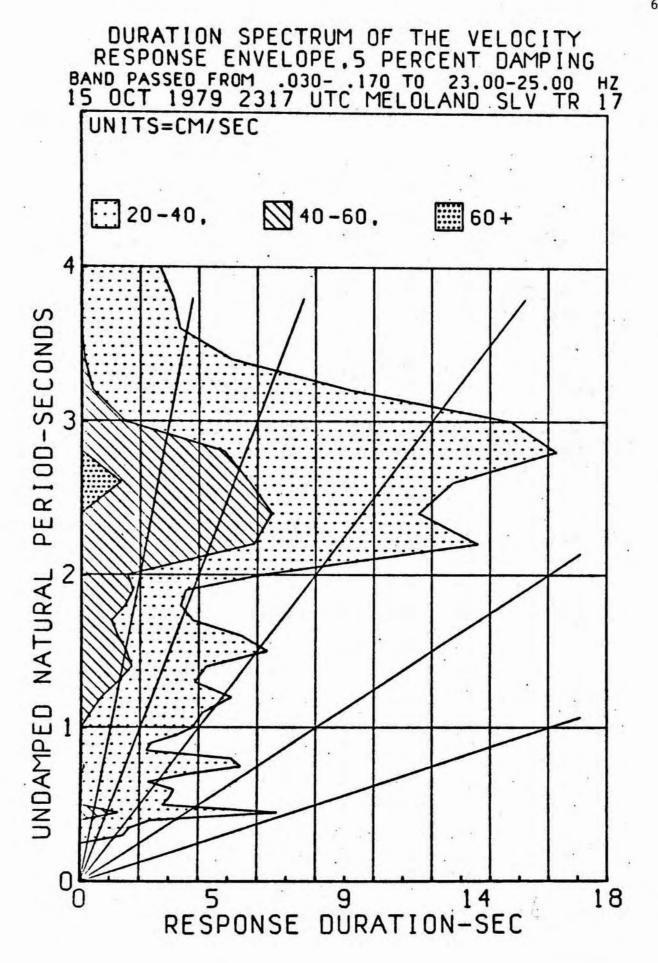


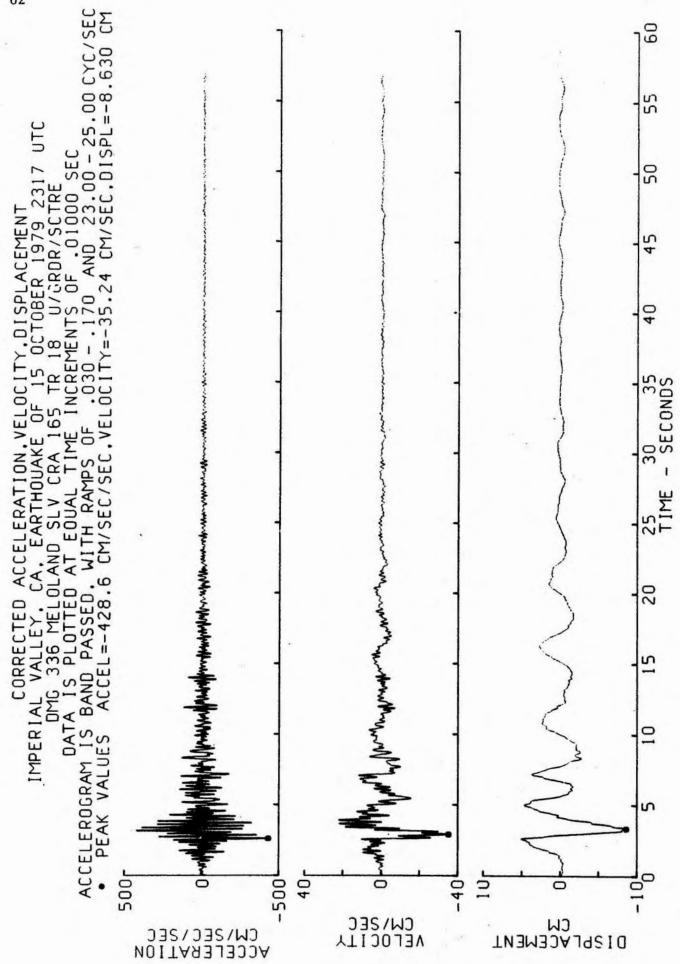




SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 17 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

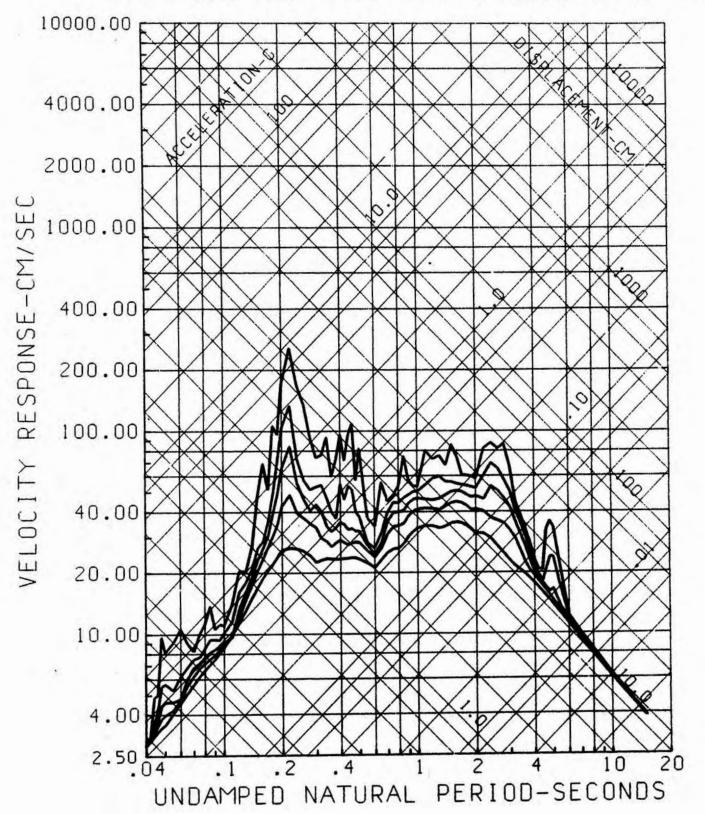


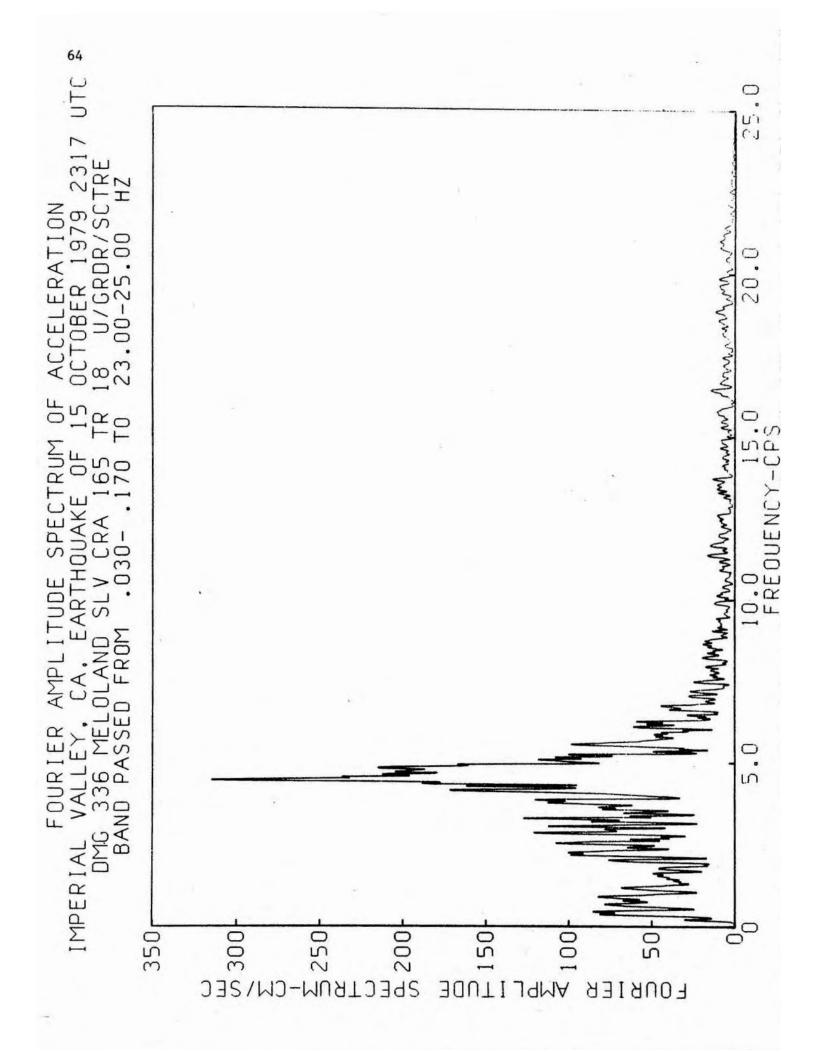


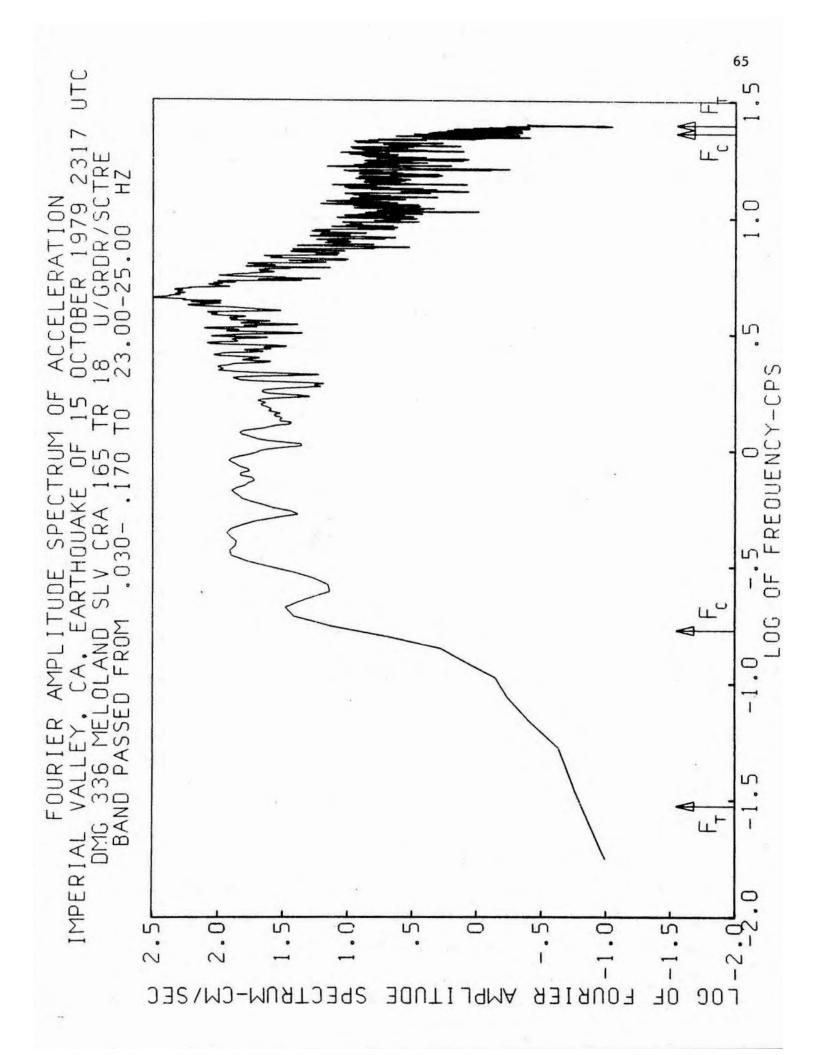


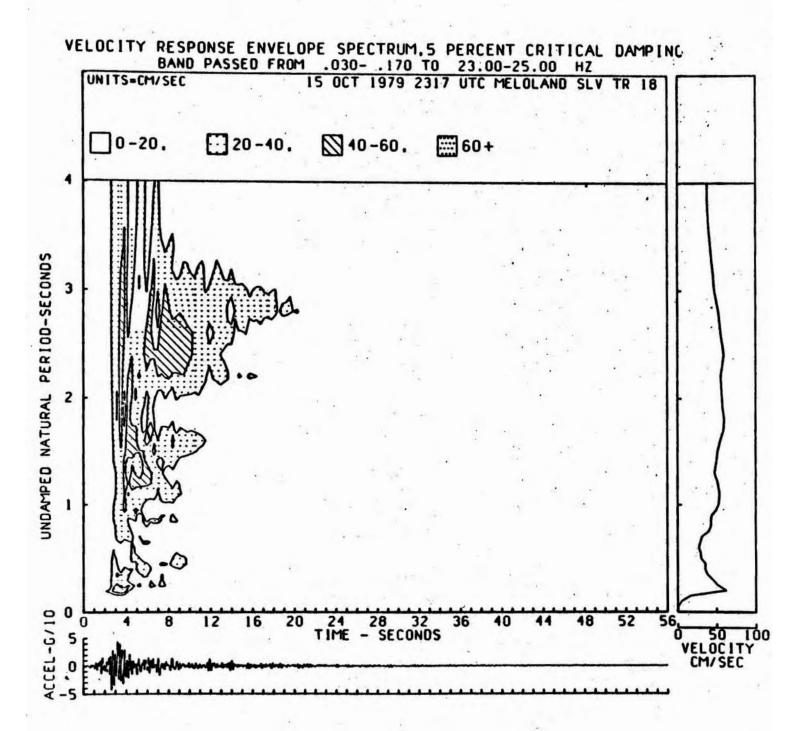
## RESPONSE SPECTRA

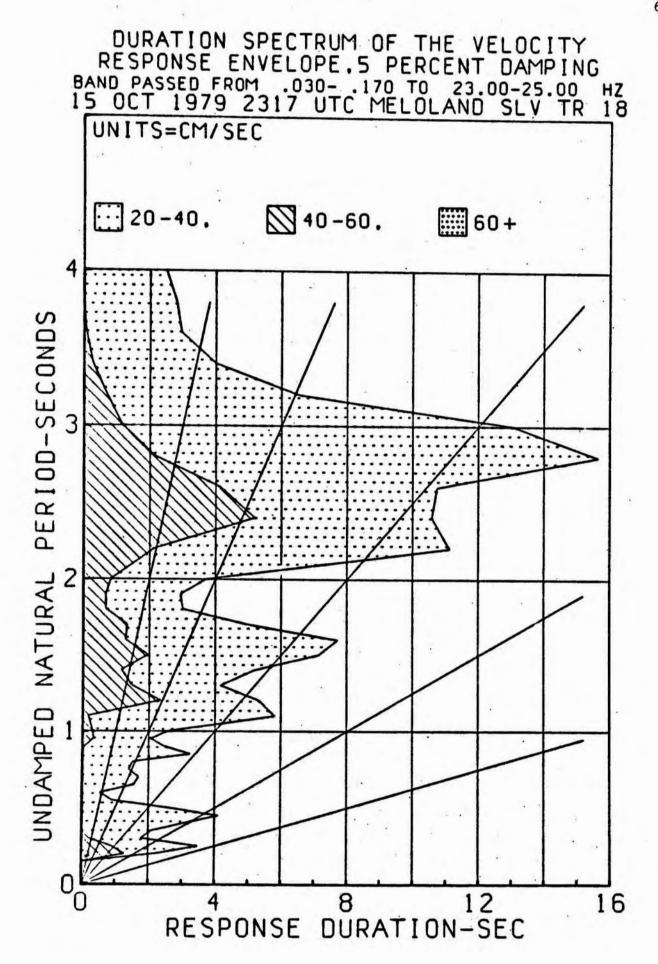
15 OCT 1979 2317 UTC MELOLAND SLV TR 18 0,2,5,10,20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



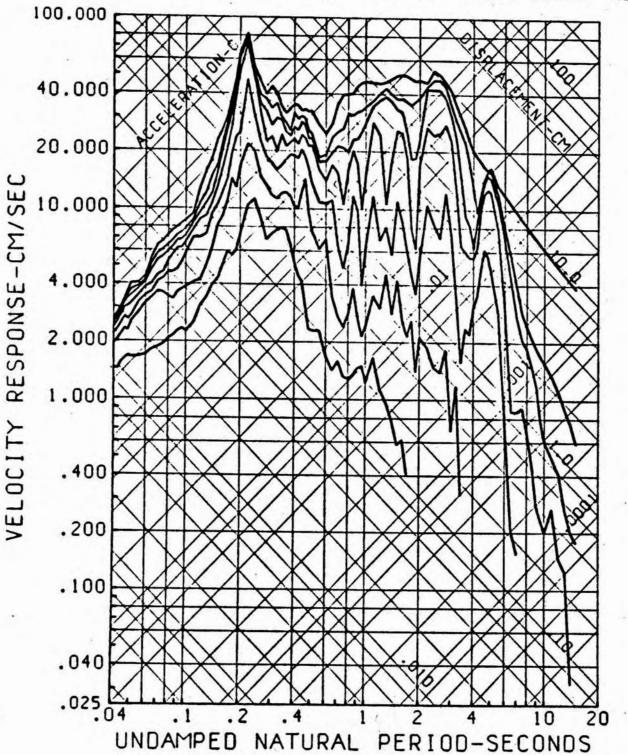


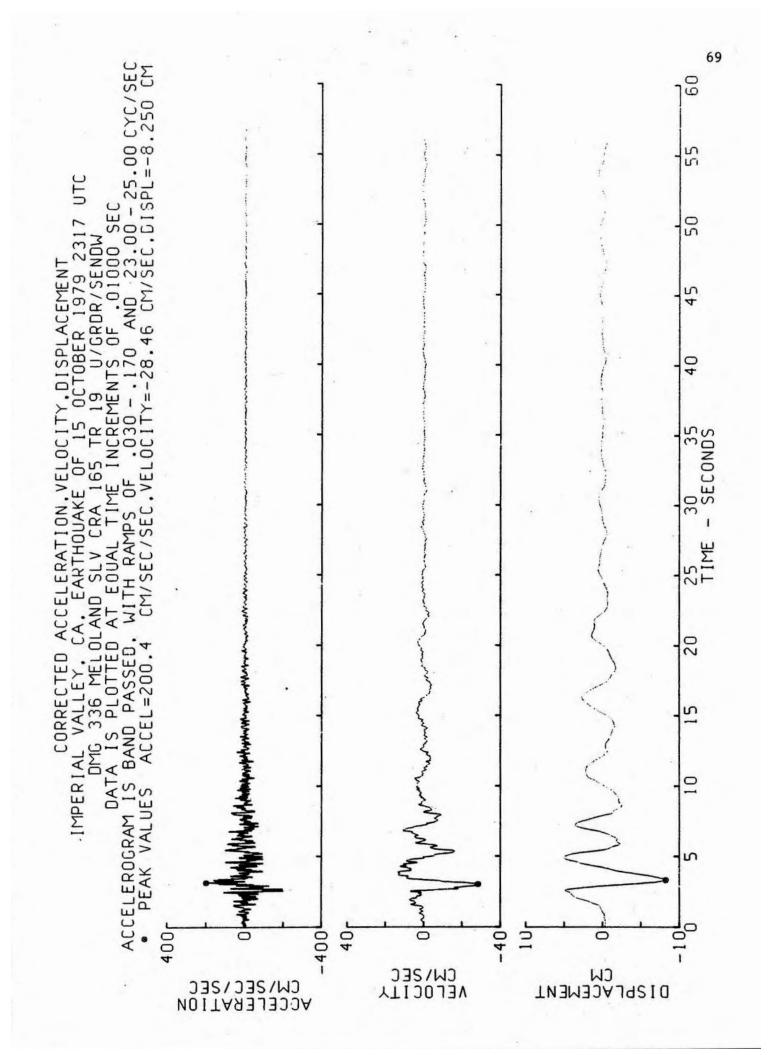






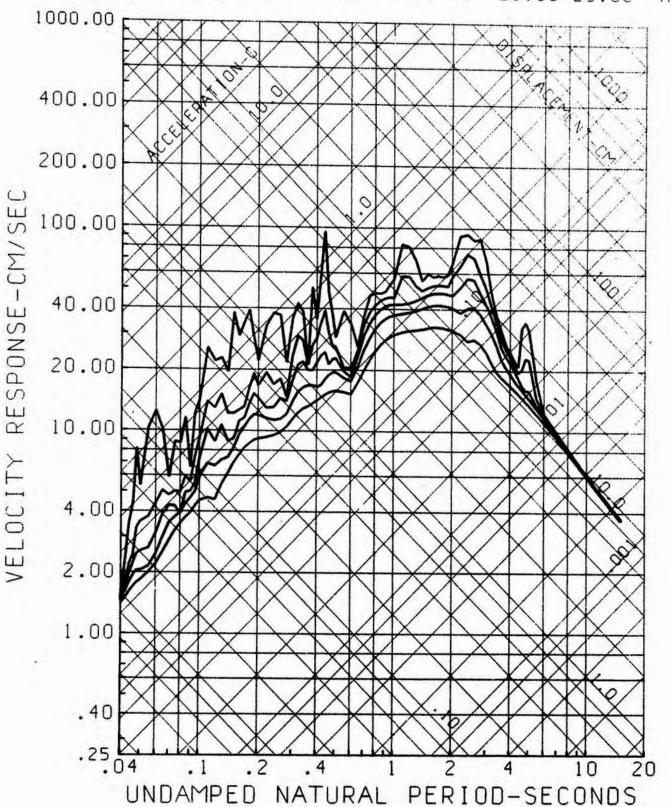
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 18 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

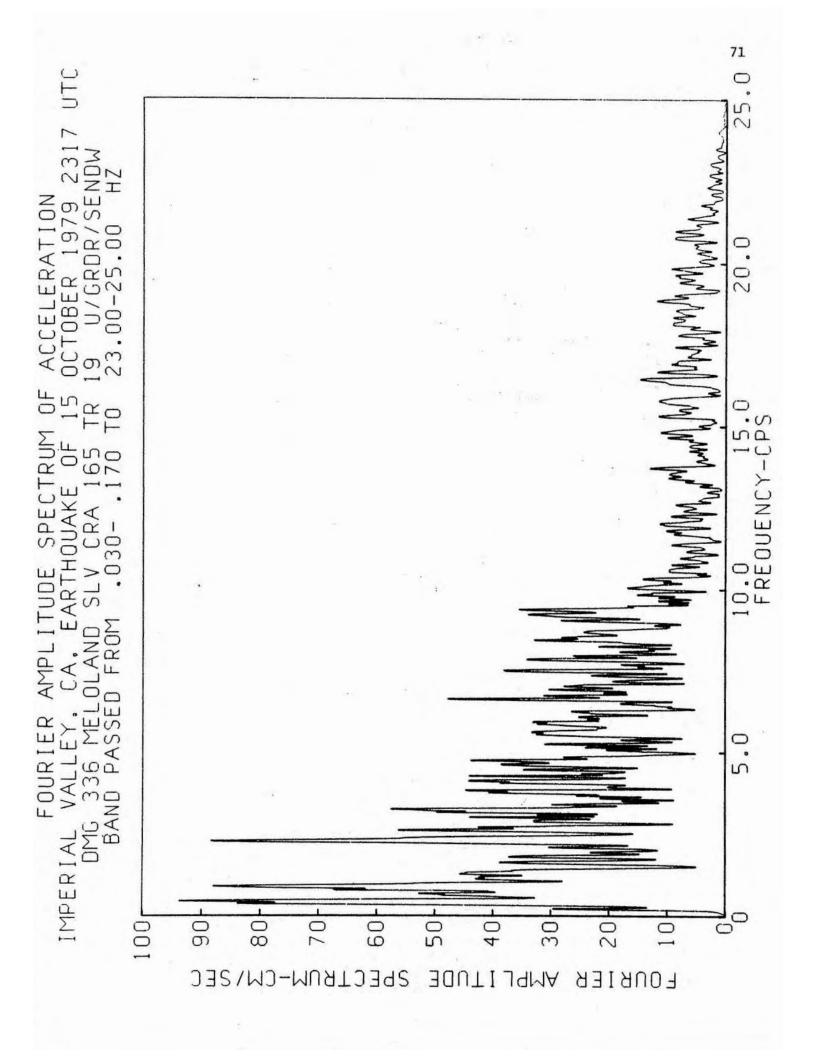


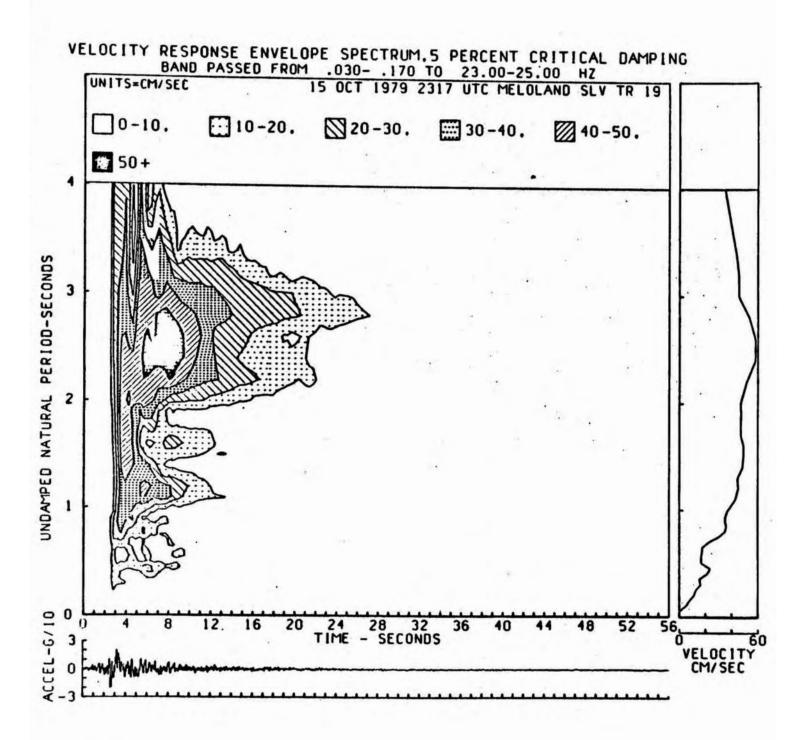


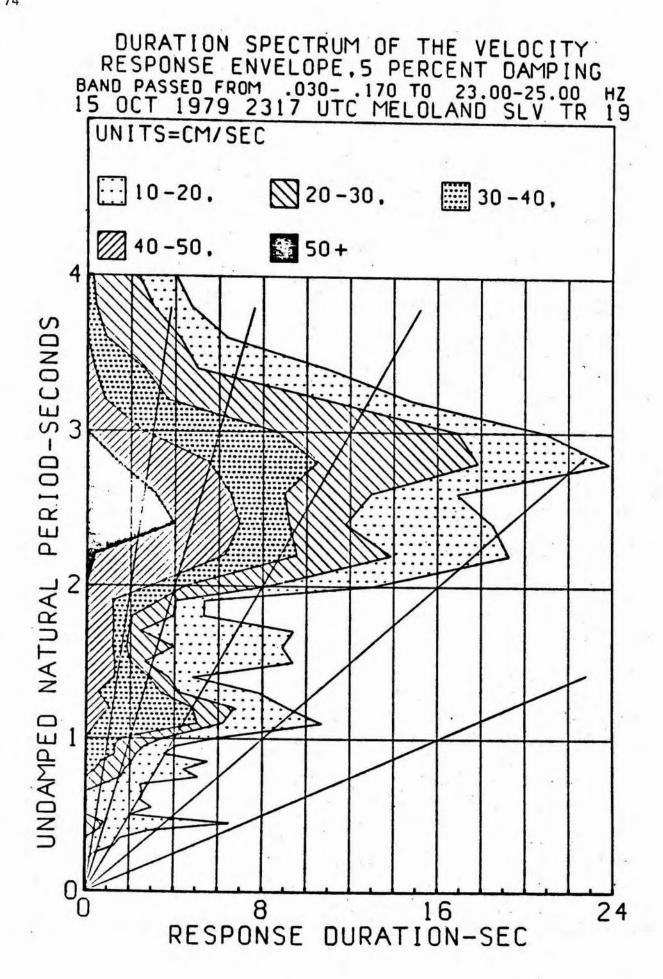
RESPONSE SPECTRA

15 OCT 1979 2317 UTC MELOLAND SLV TR 19
0.2.5.10.20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

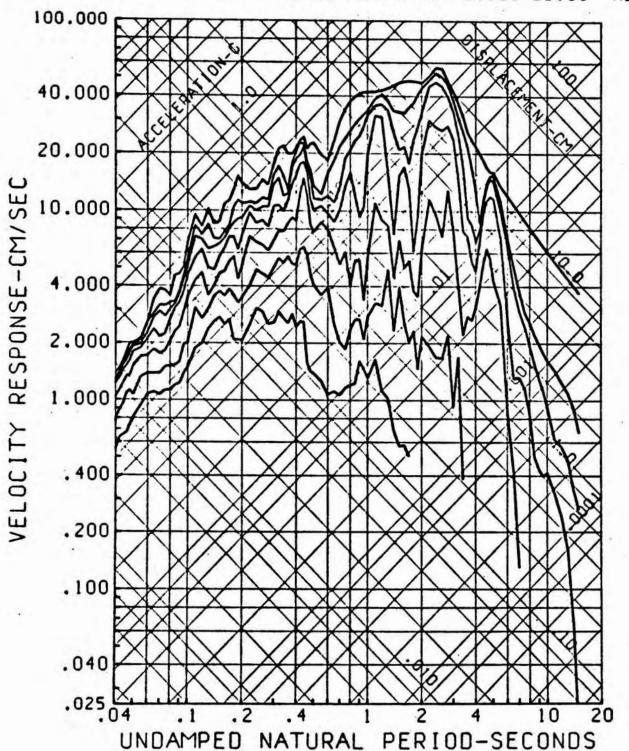




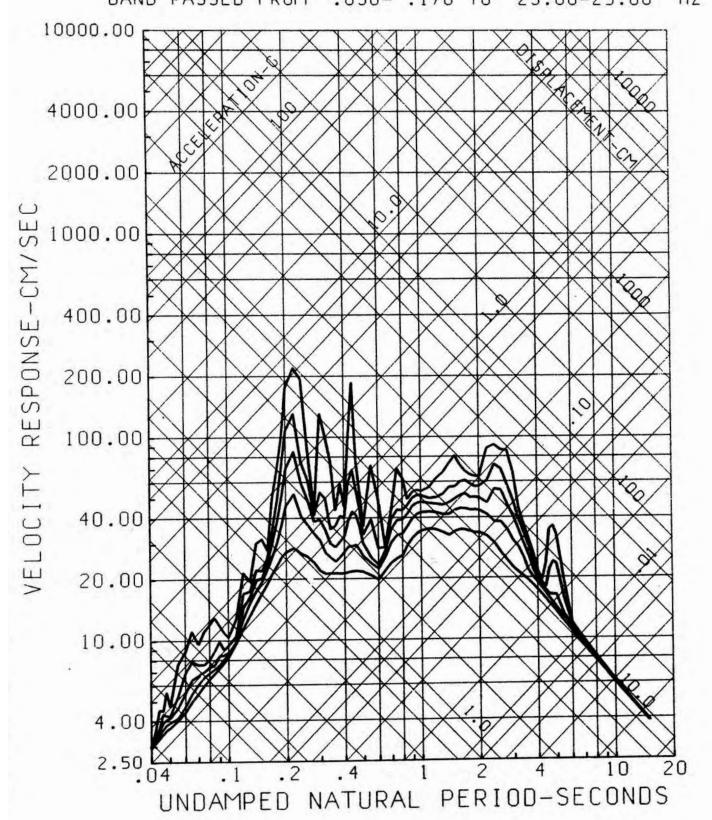


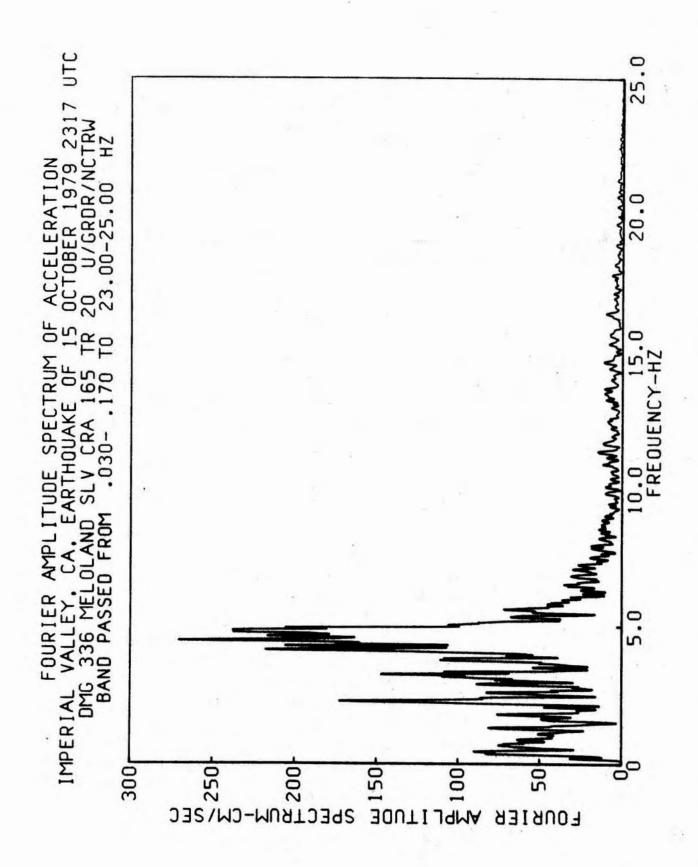


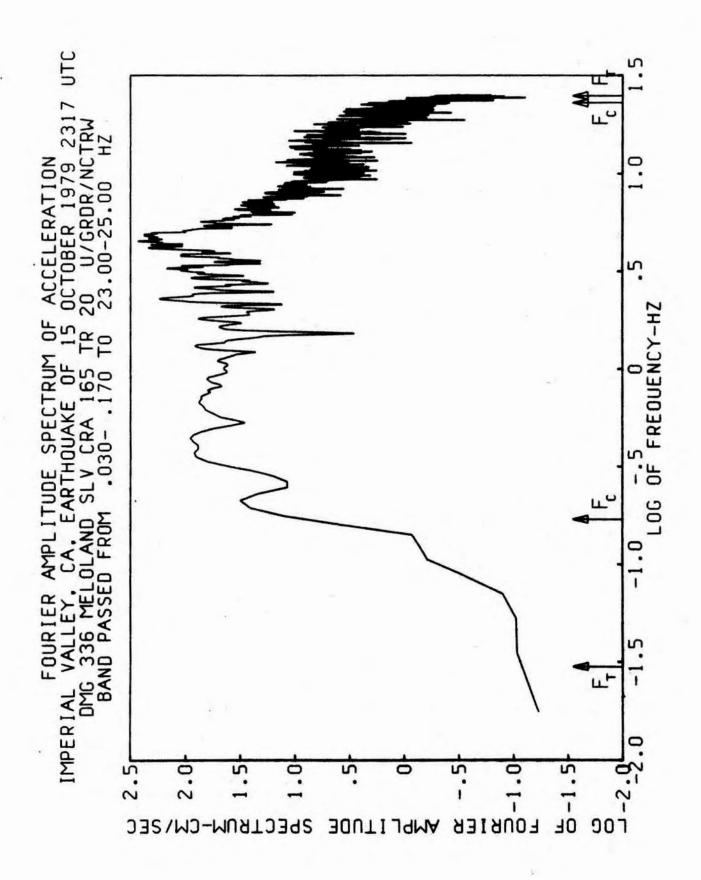
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 19 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

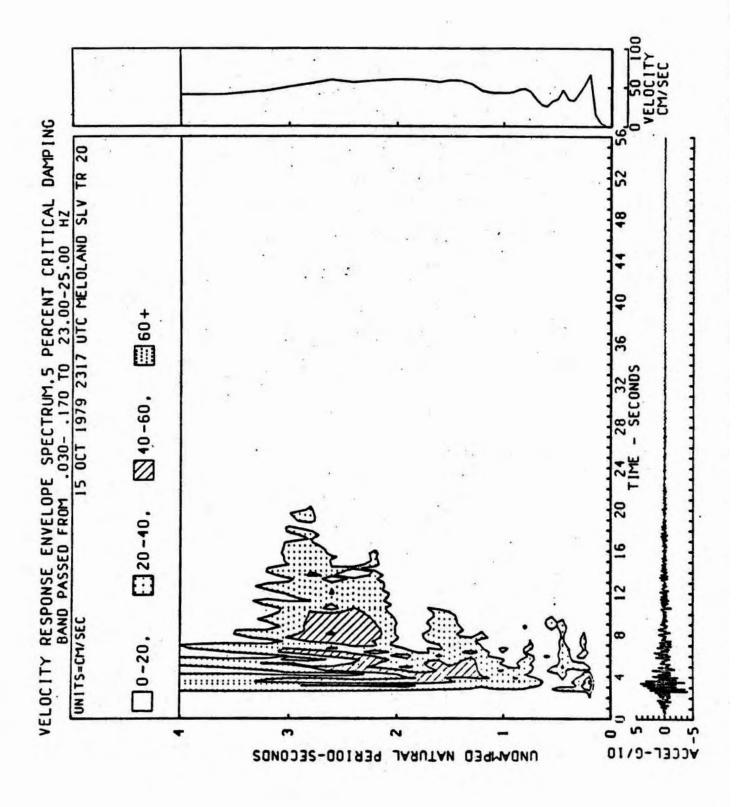


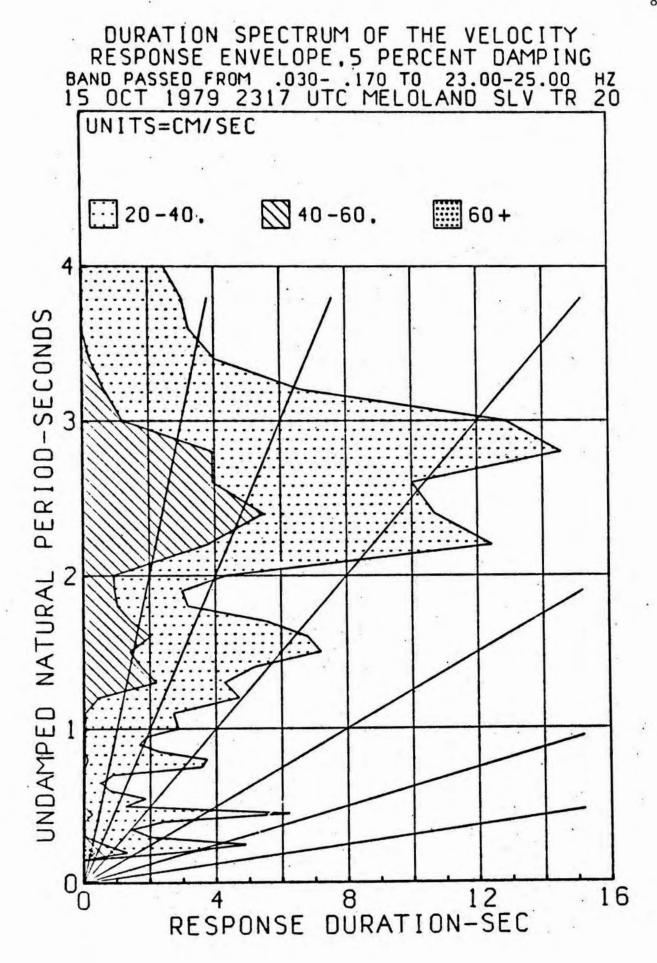
RESPONSE SPECTRA
15 OCT 1979 2317 UTC MELOLAND SLV TR 20
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



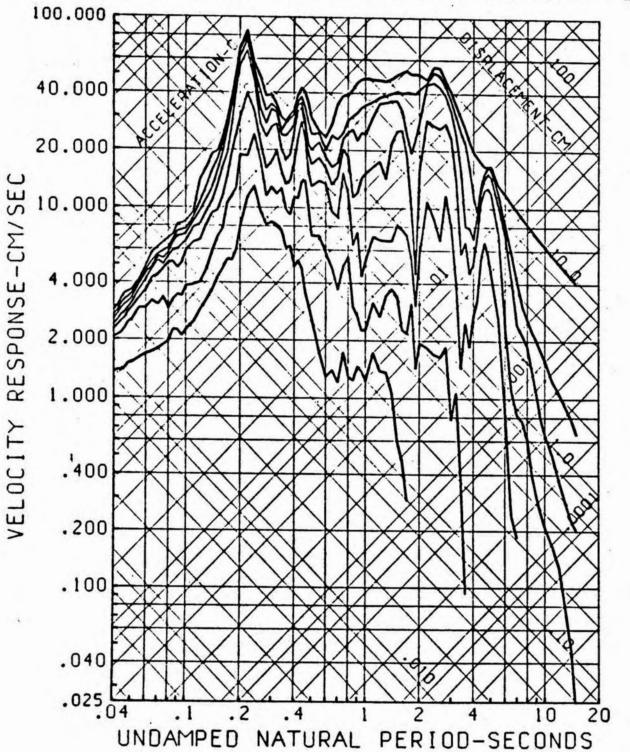


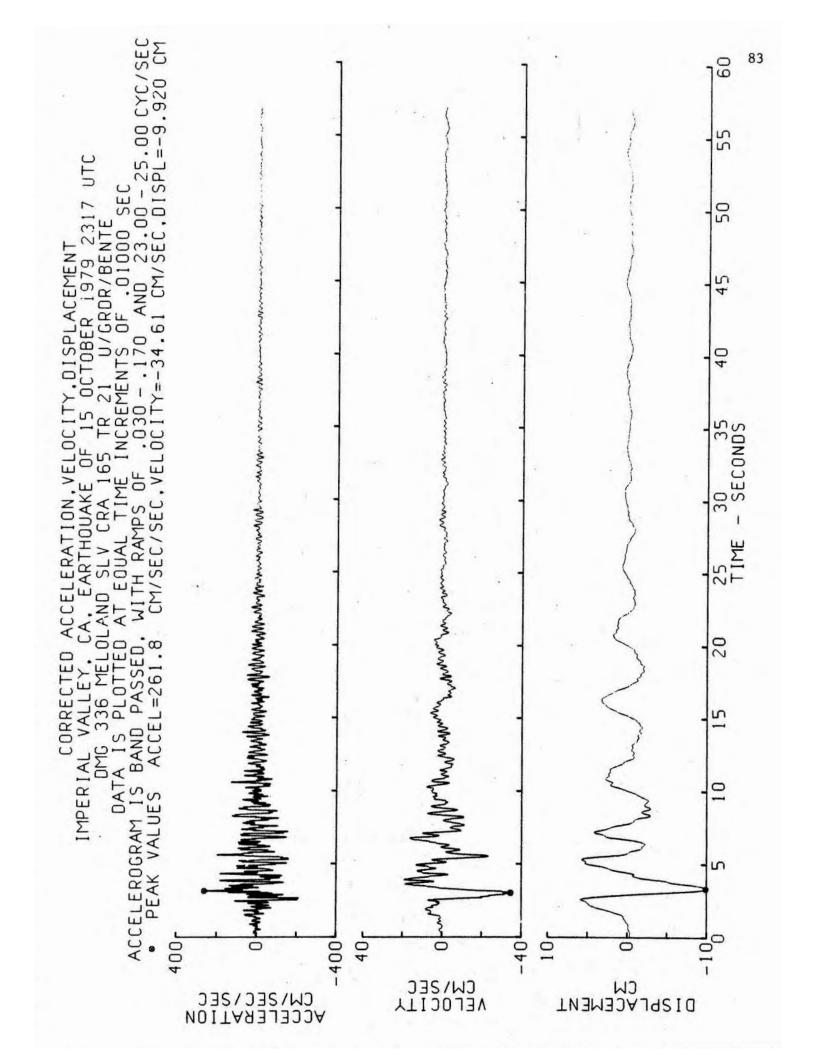




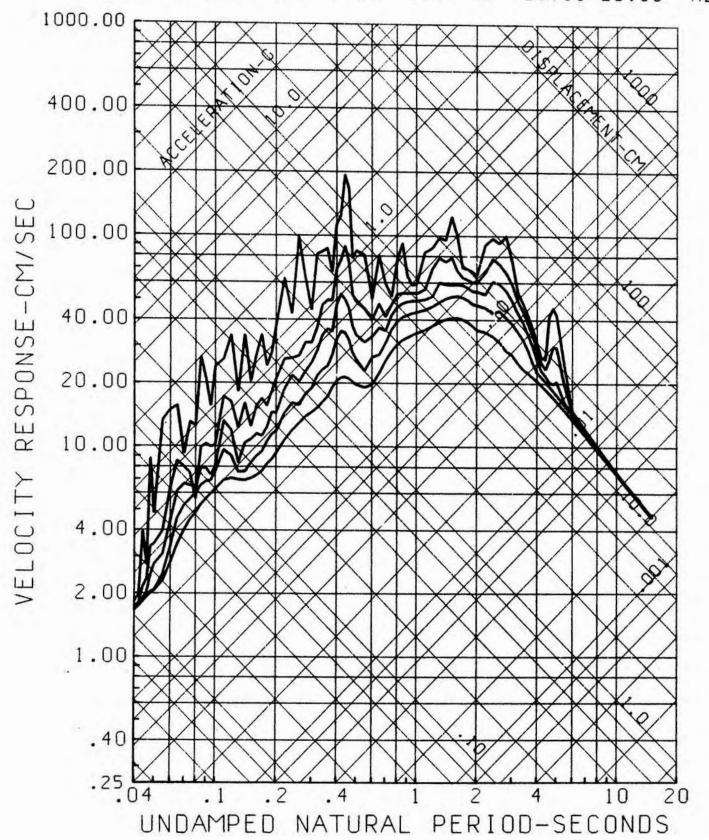


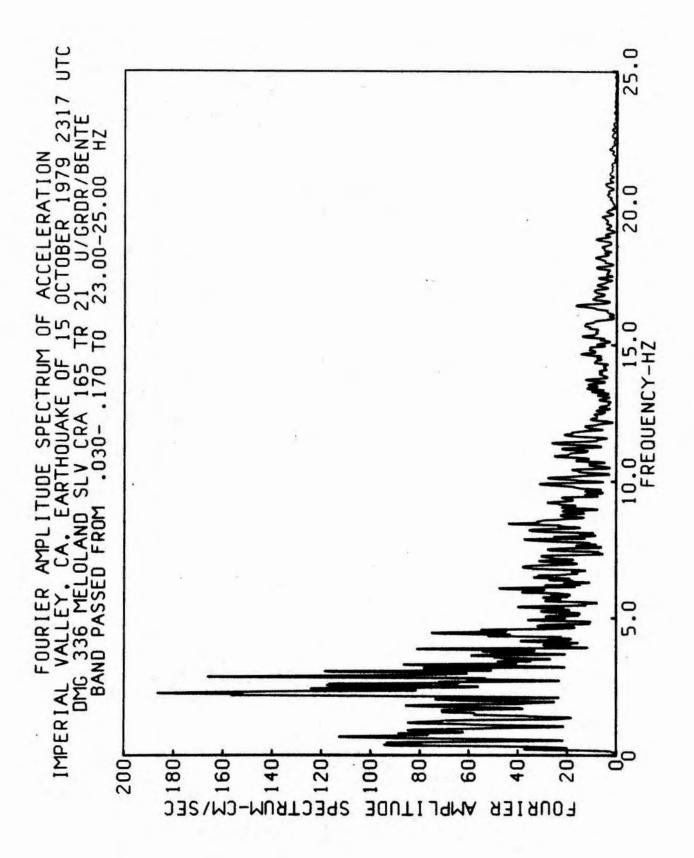
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 20 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

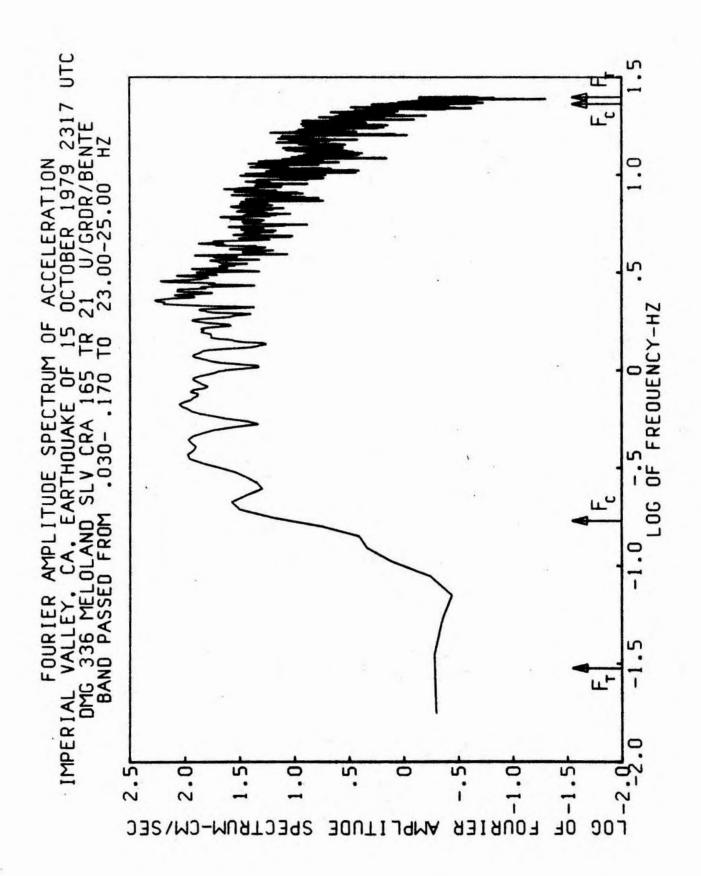


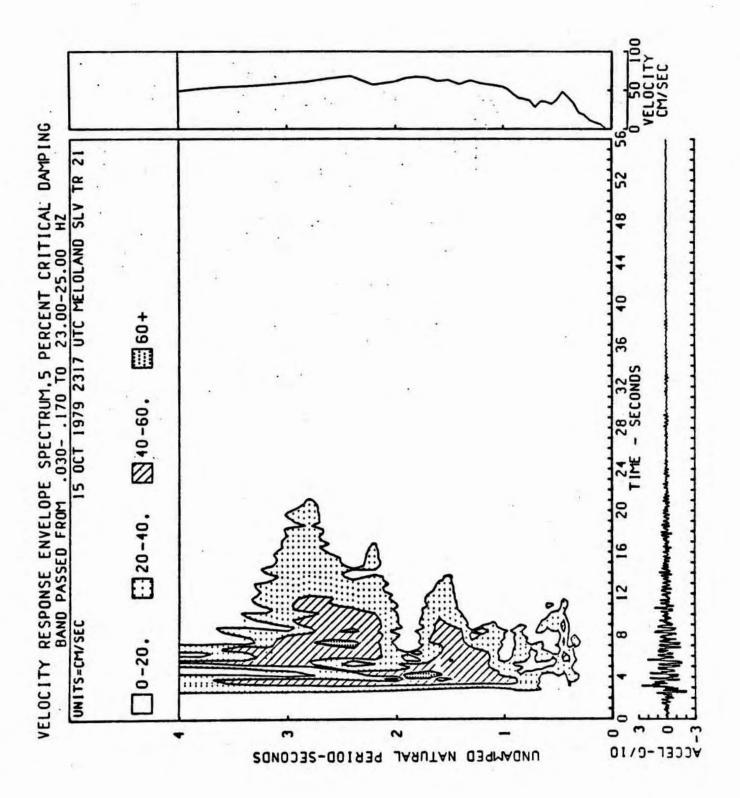


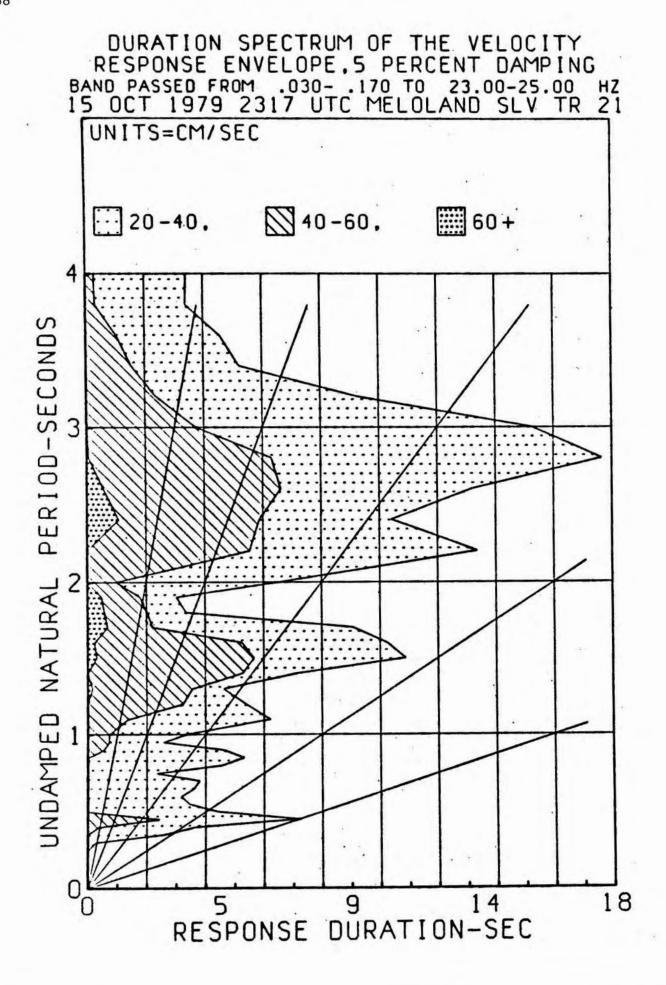
## RESPONSE SPECTRA 15 OCT 1979 2317 UTC MELOLAND SLV TR 21 0,2,5,10,20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



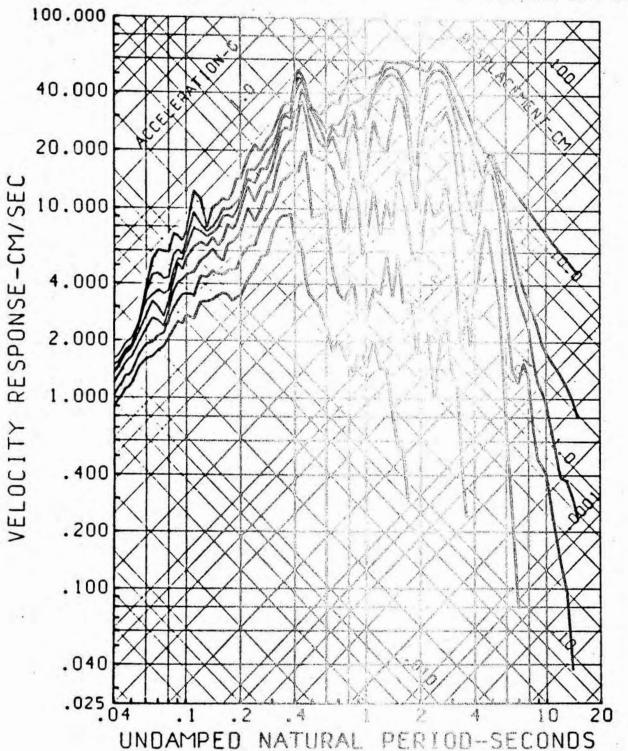






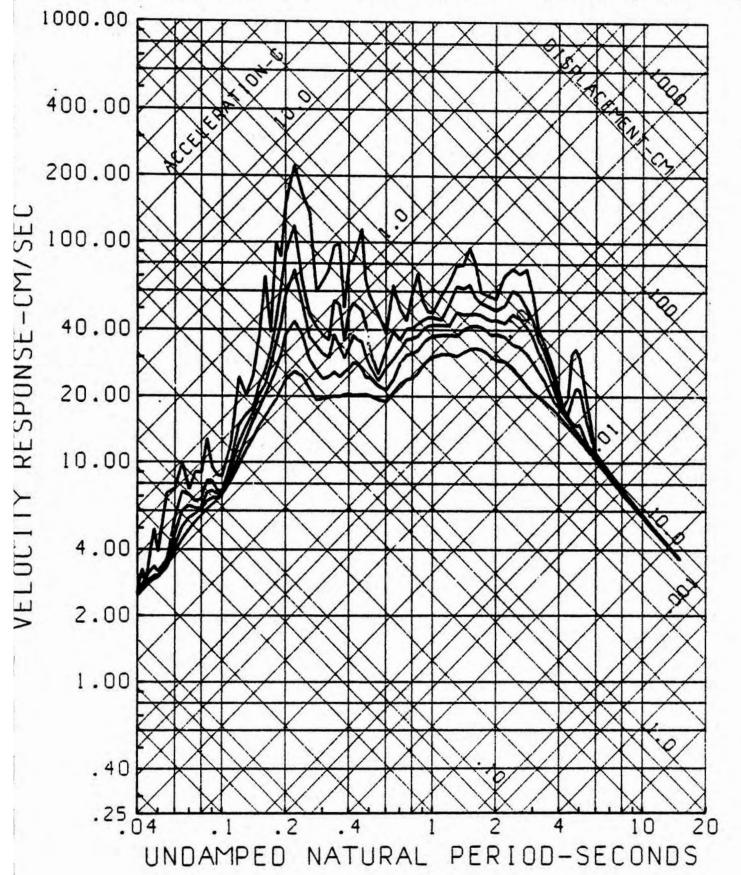


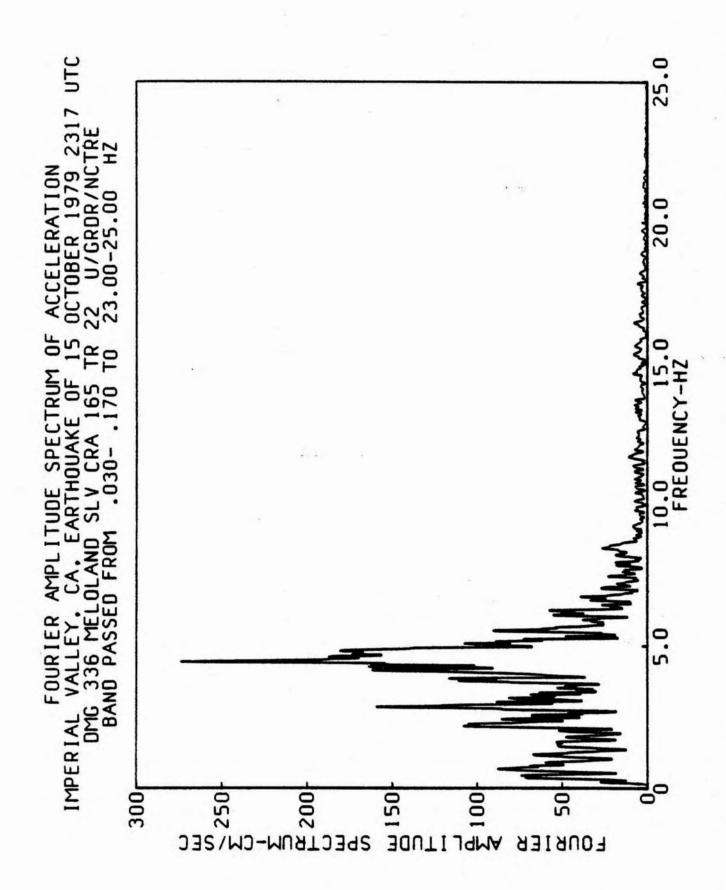
SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC MELDIAND SLV TR 21
5 PERCENT UNITION DAMPING
BAND PASSED FROM .030-.170 TO 23.00-25.00 HZ

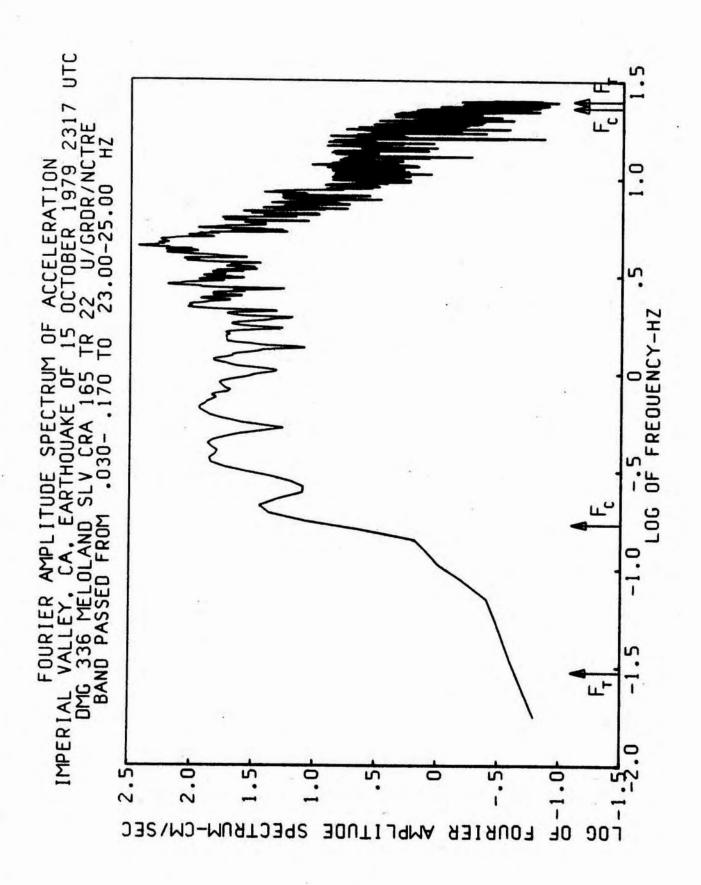


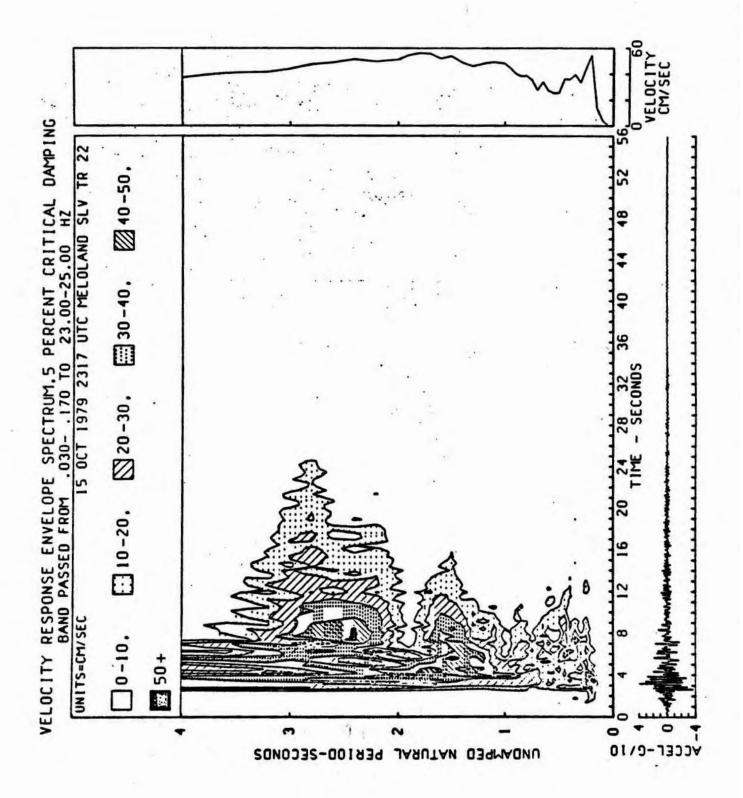
RESPONSE SPECTRA 15 OCT 1979 2317 UTC

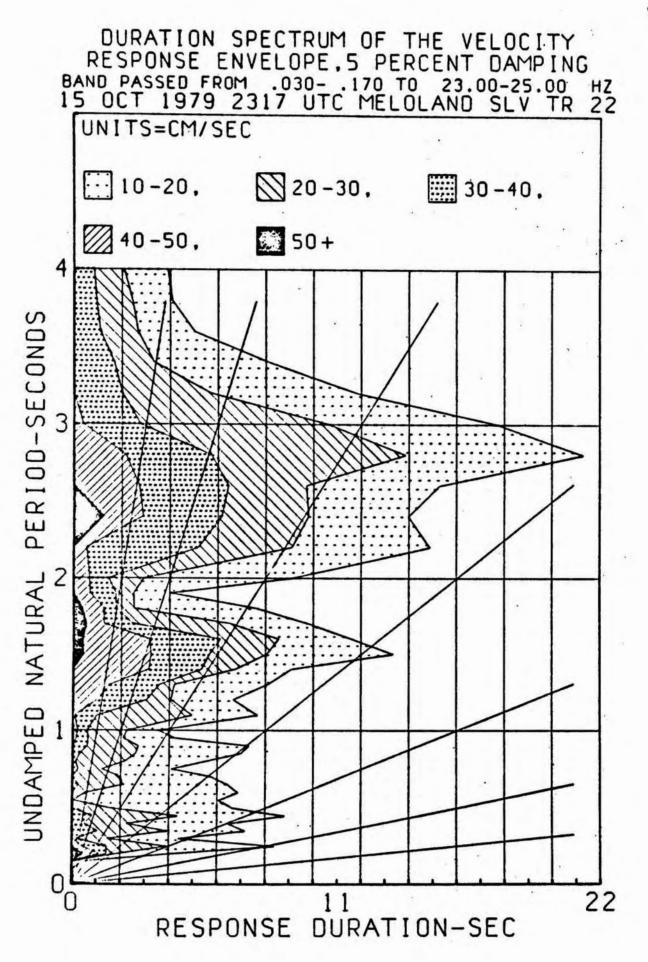
0.2.5.10.20 PERCENT BAND PASSED FROM .030- .17



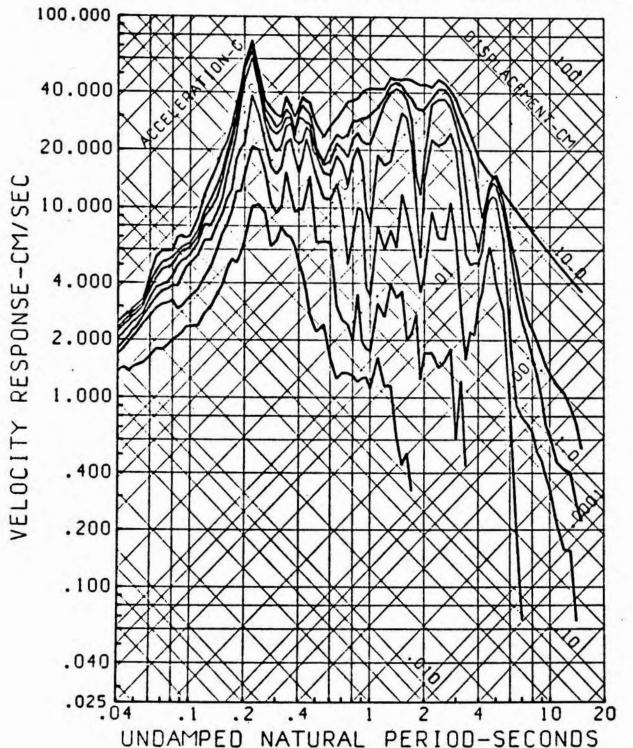


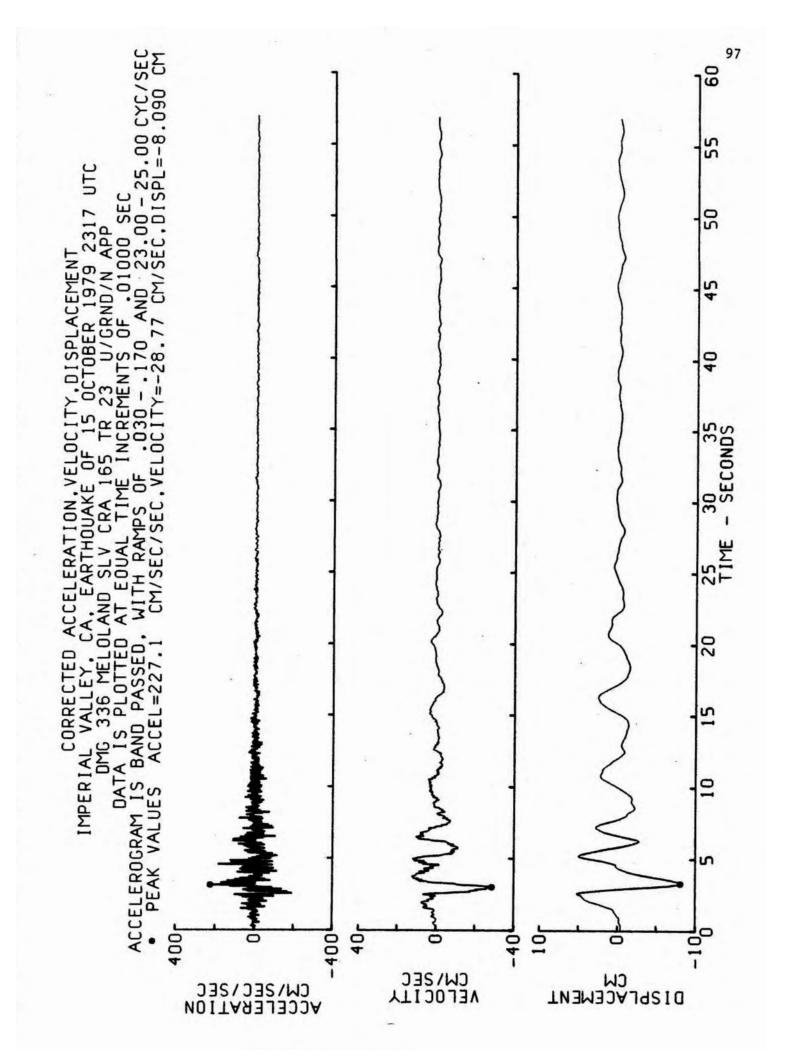






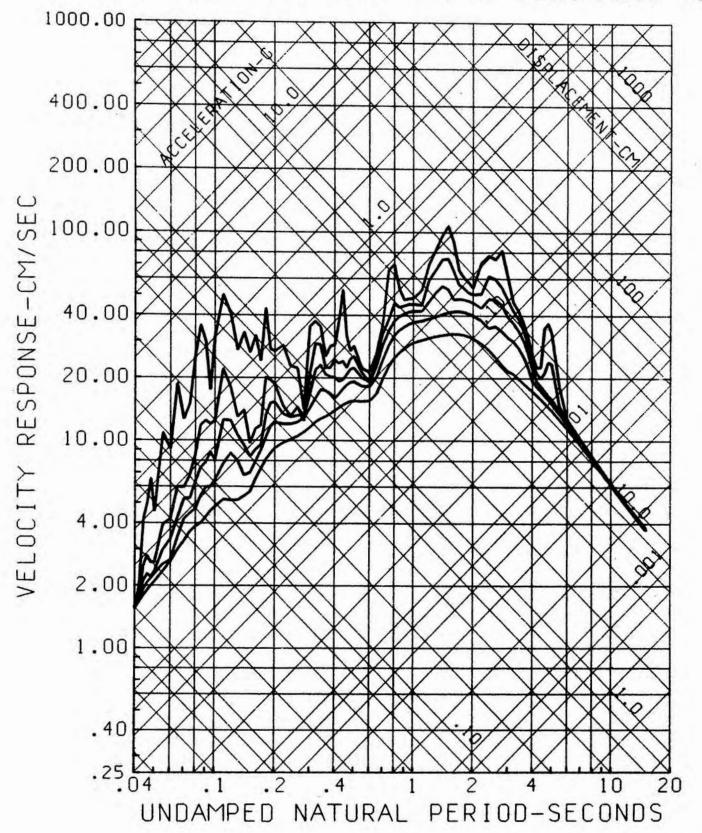
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 22 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

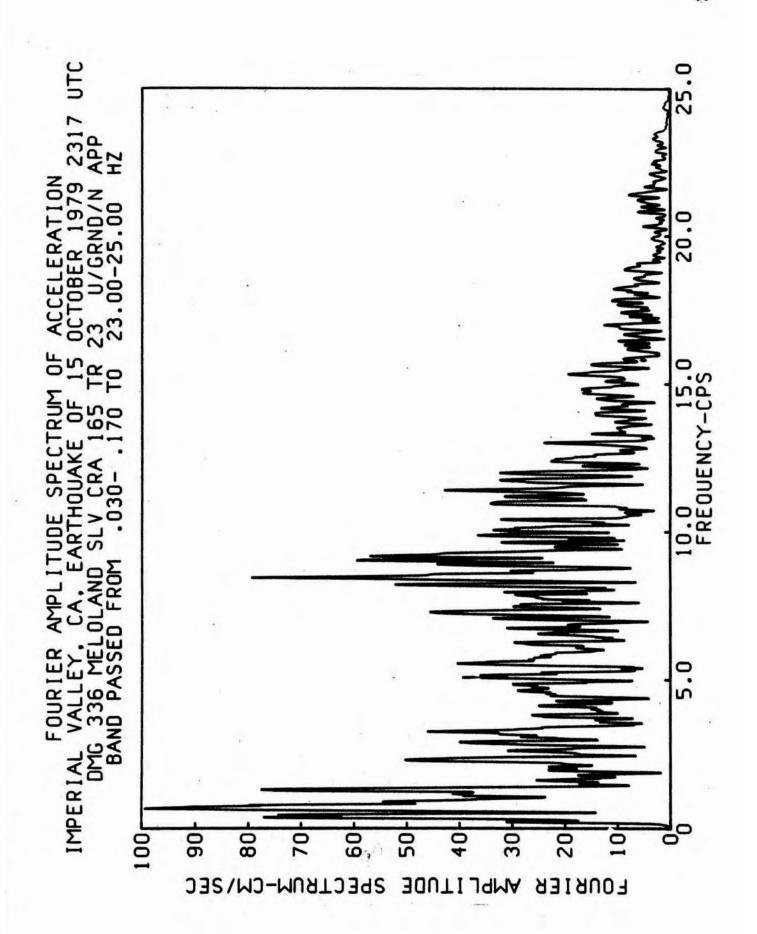


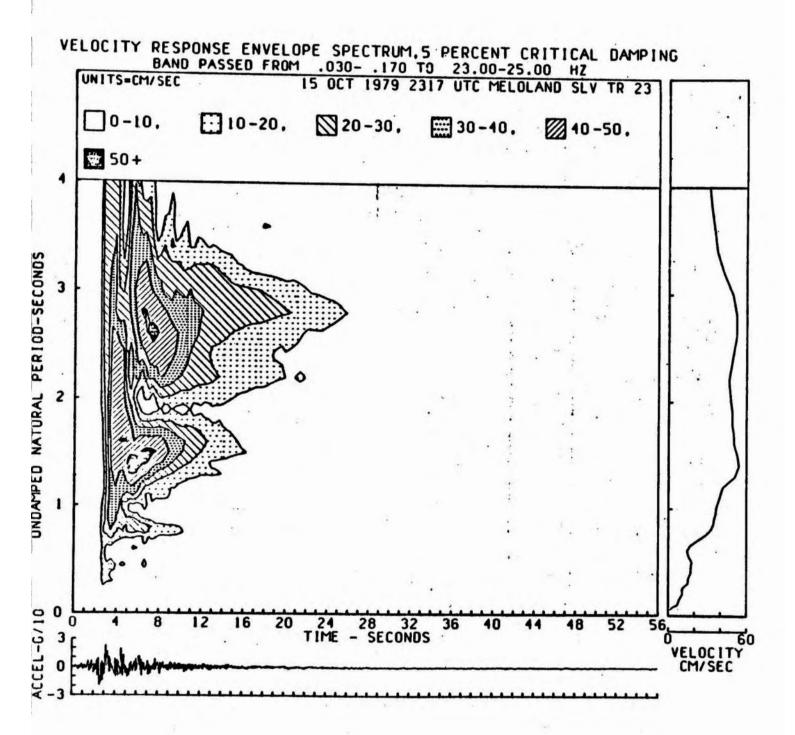


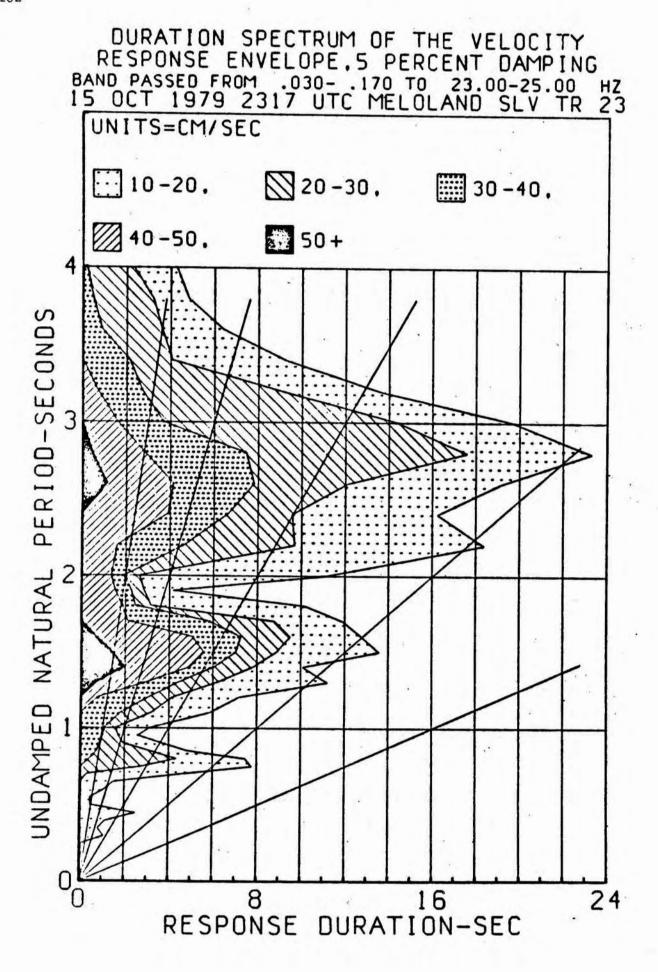
## RESPONSE SPECTRA

15 OCT 1979 2317 UTC MELOLAND SLV TR 23 0.2,5,10,20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

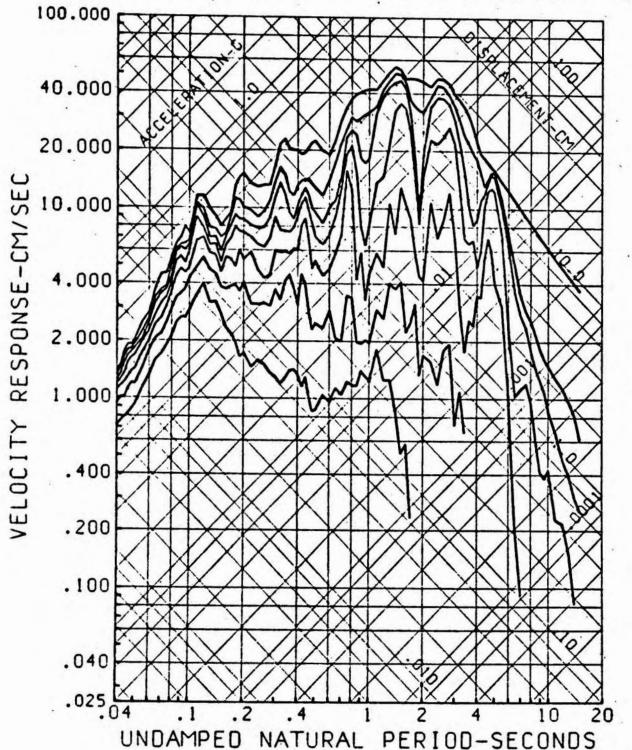


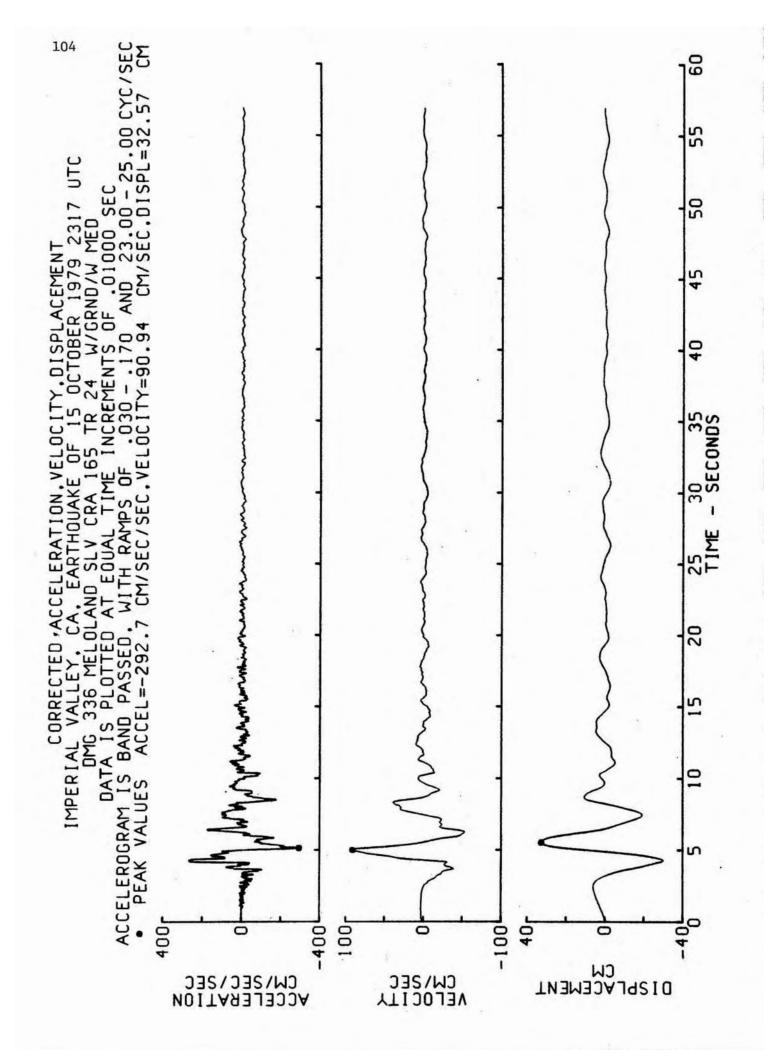






SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 23 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

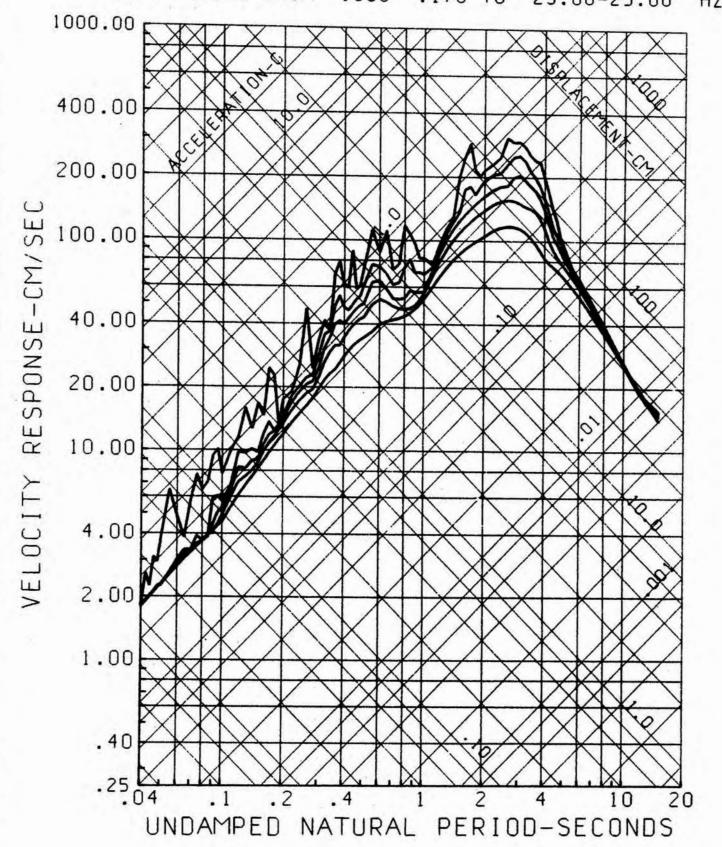


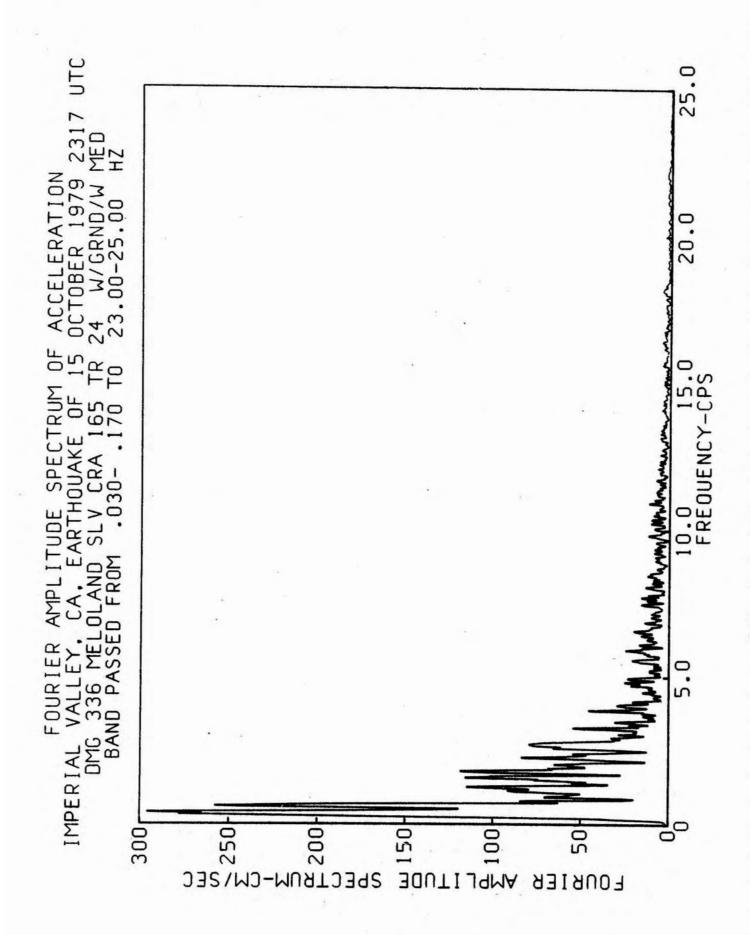


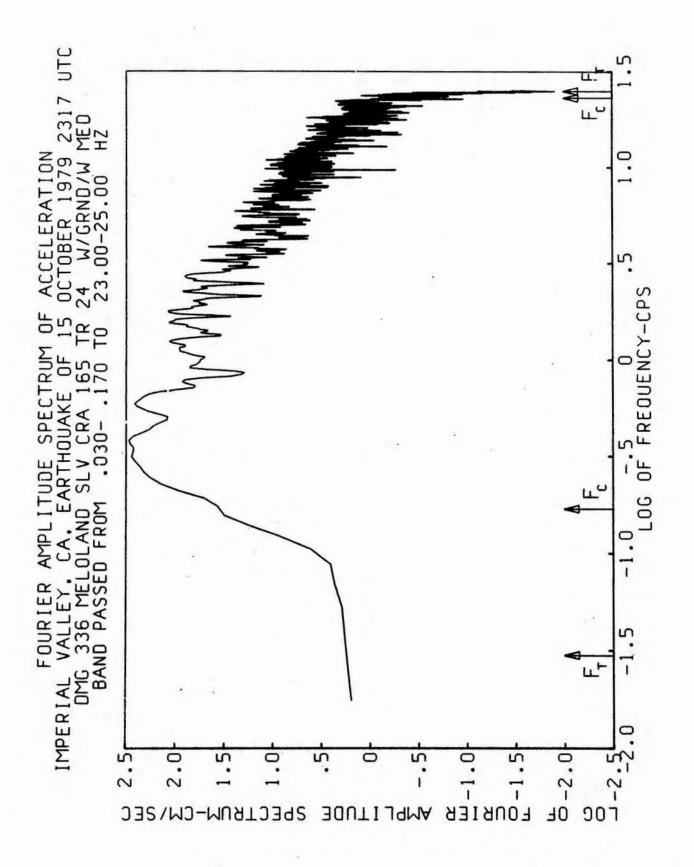
RESPONSE SPECTRA

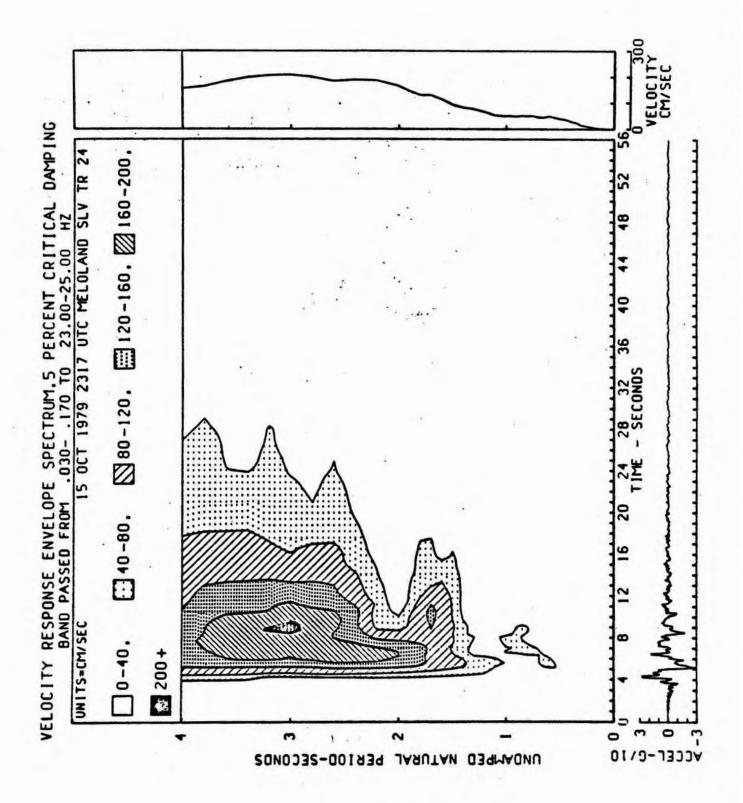
15 OCT 1979 2317 UTC MELOLAND SLV TR 24

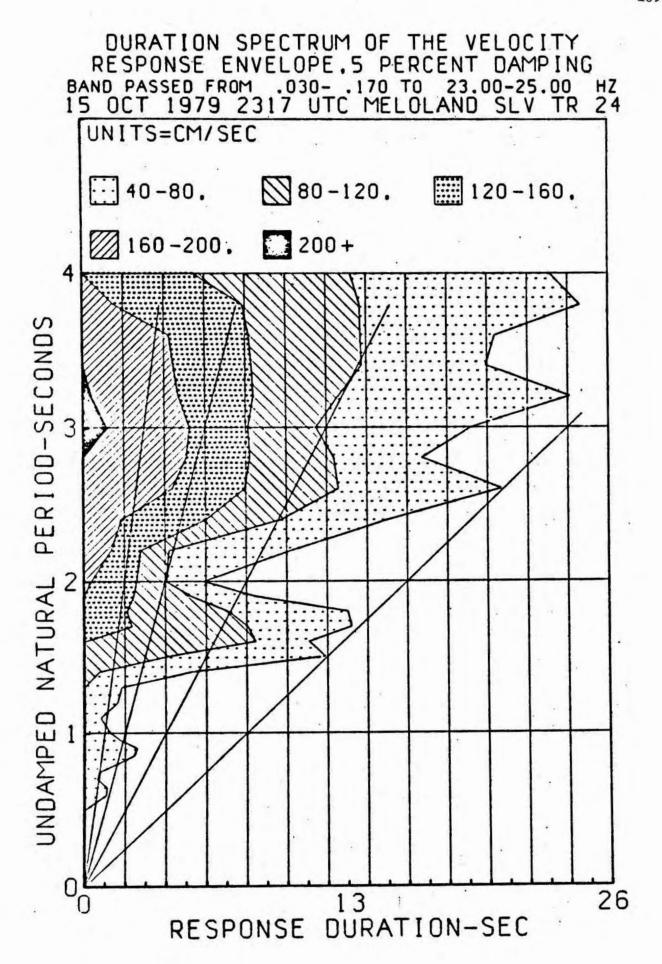
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



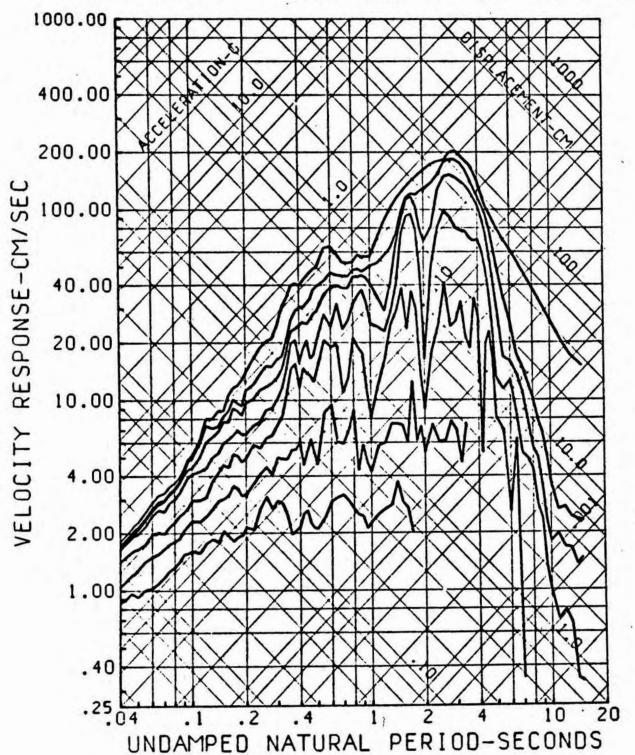


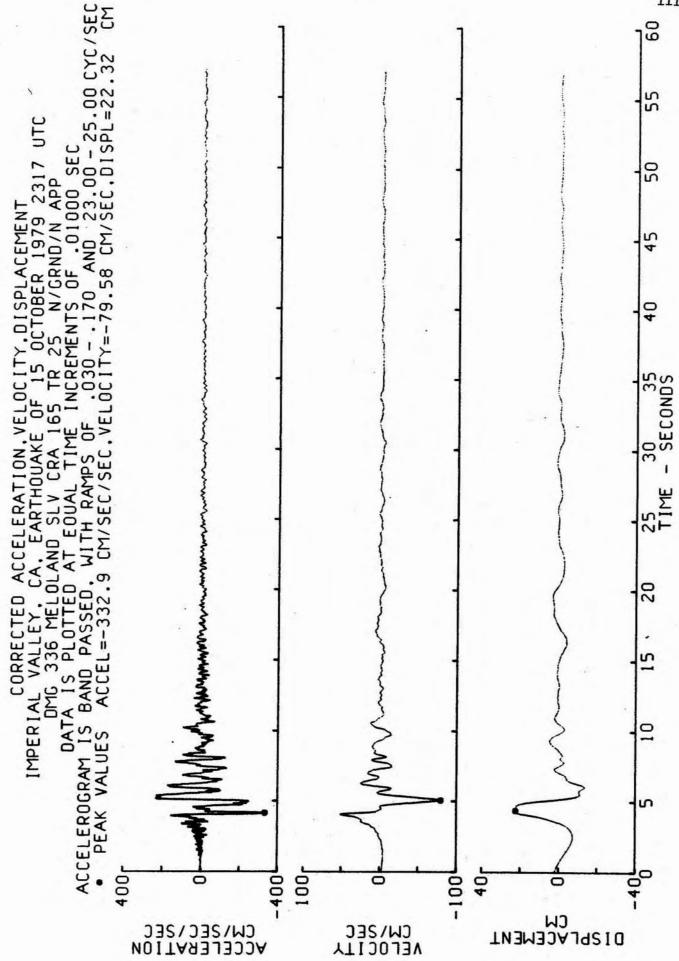






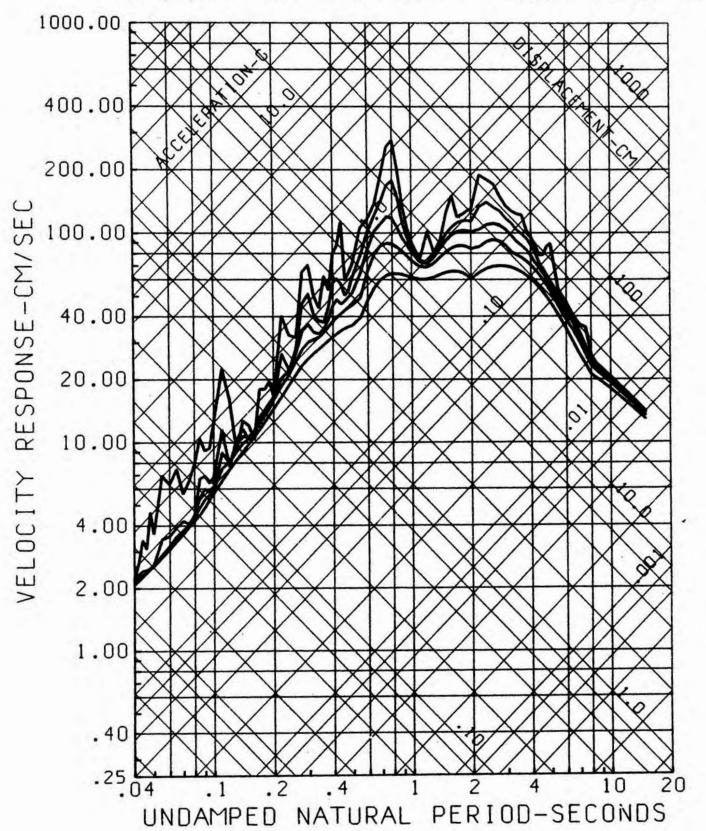
SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC MELOLAND SLV TR 24
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

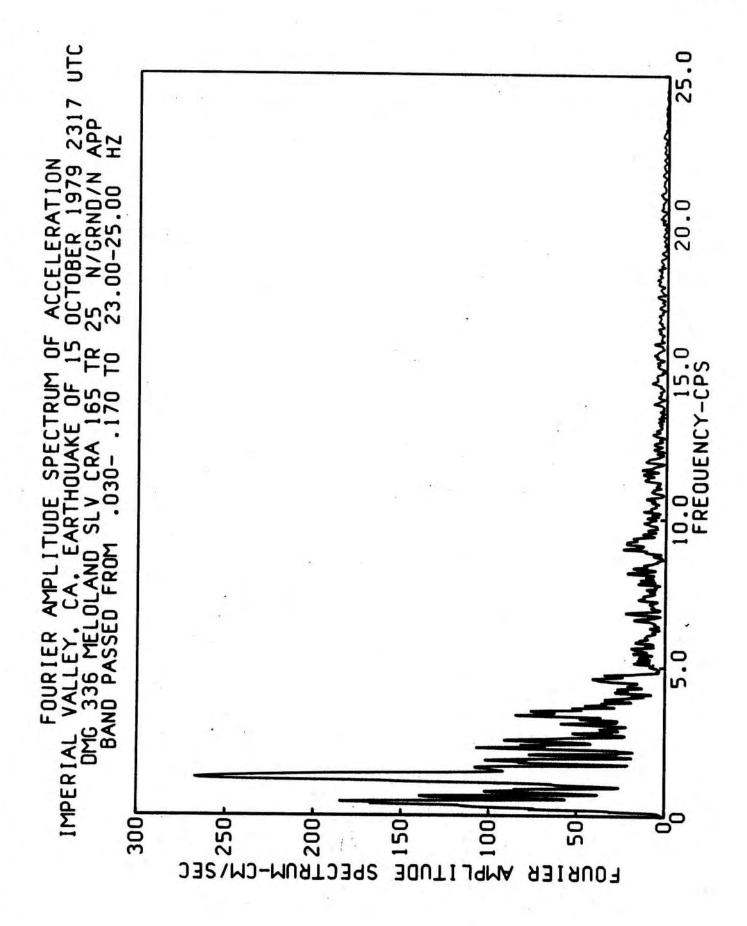


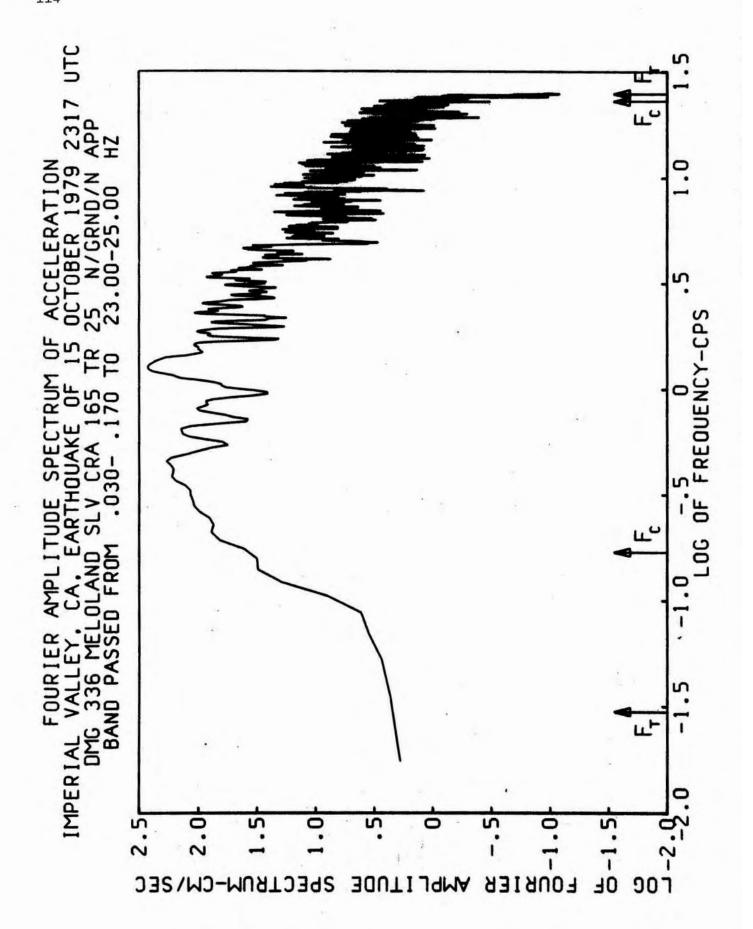


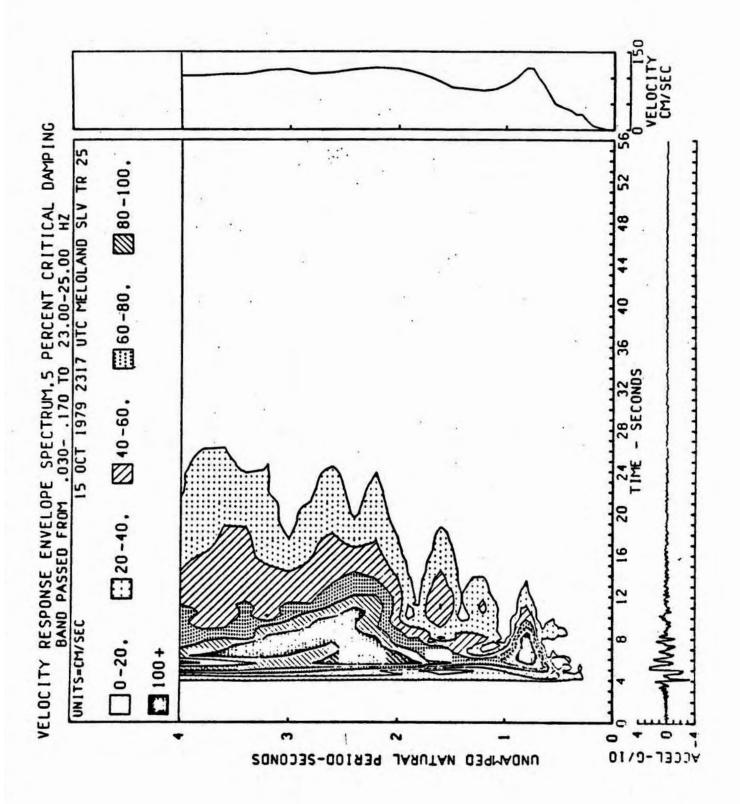
## RESPONSE SPECTRA

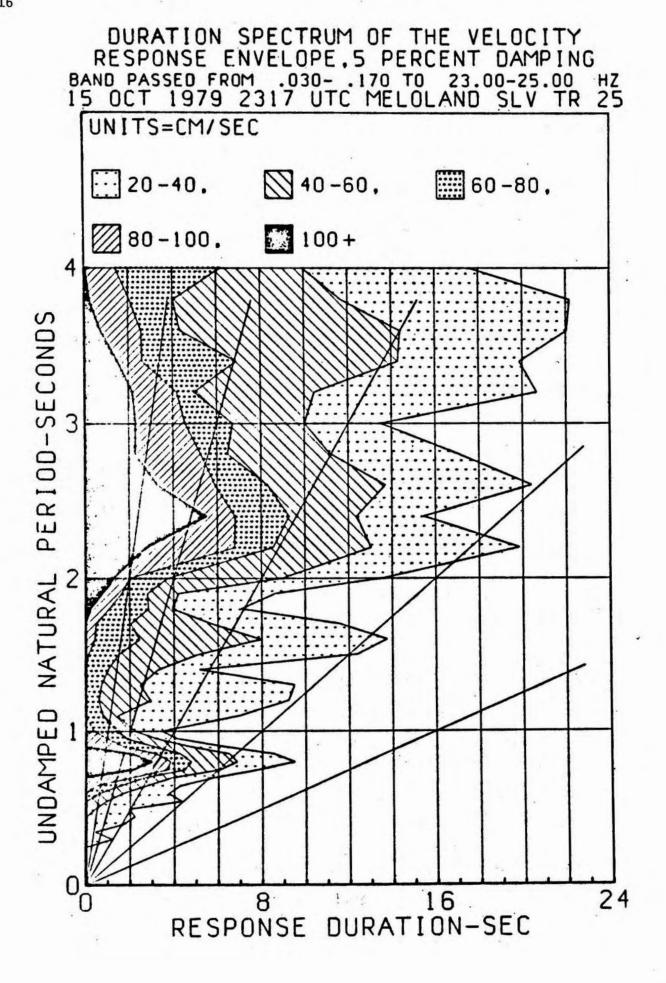
15 OCT 1979 2317 UTC MELOLAND SLV TR 25 0,2,5,10,20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



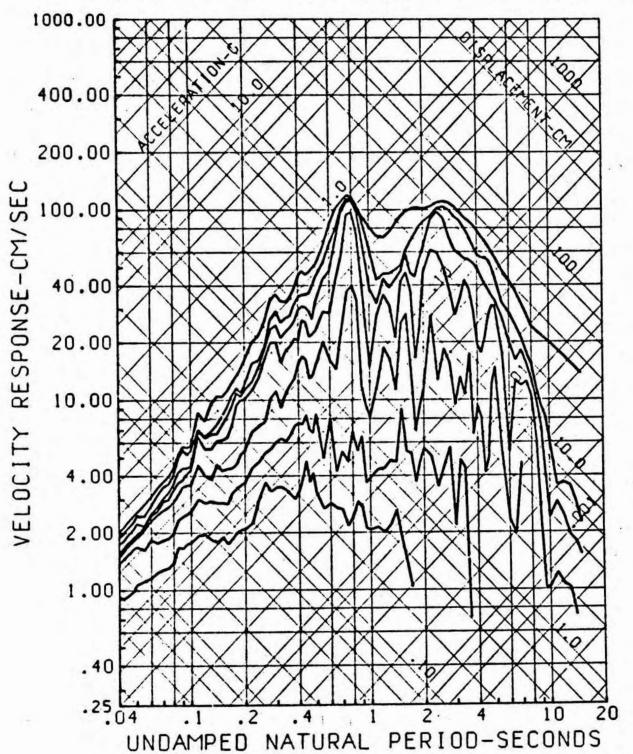


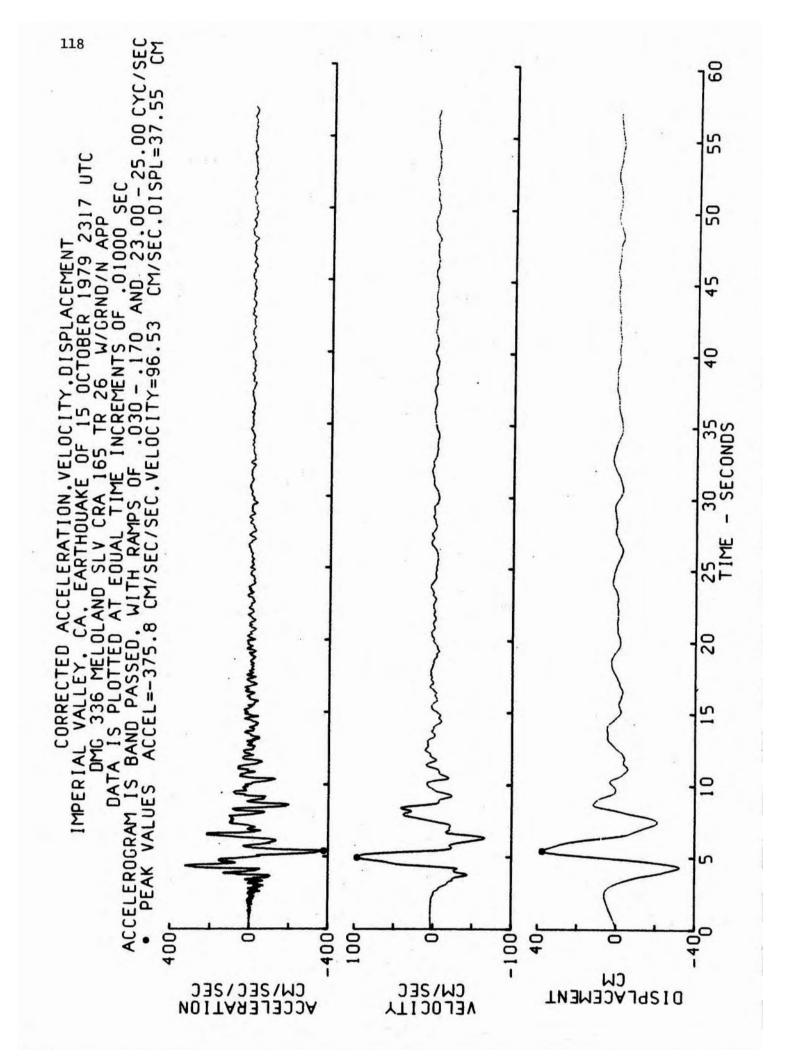






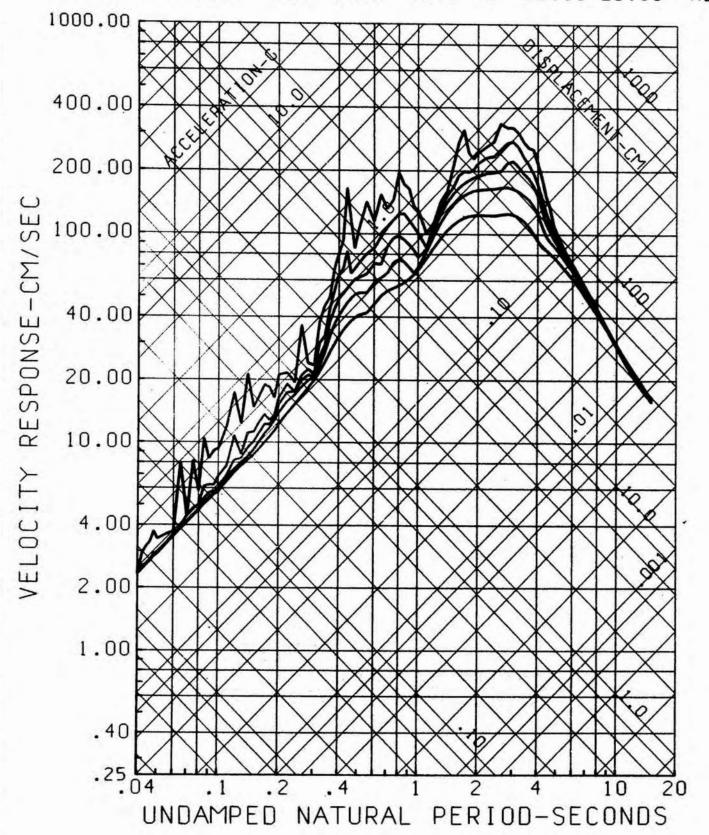
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 25 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

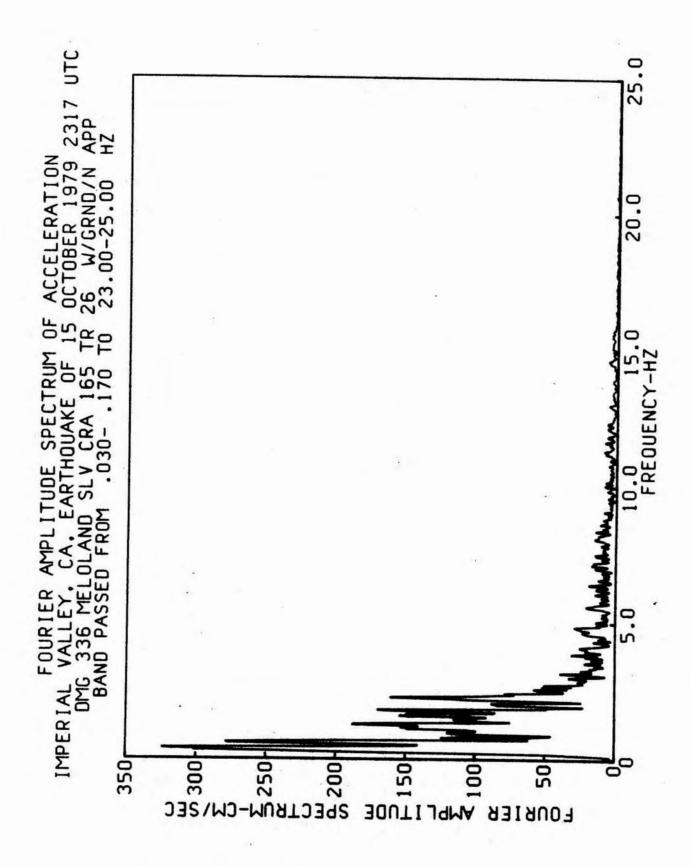


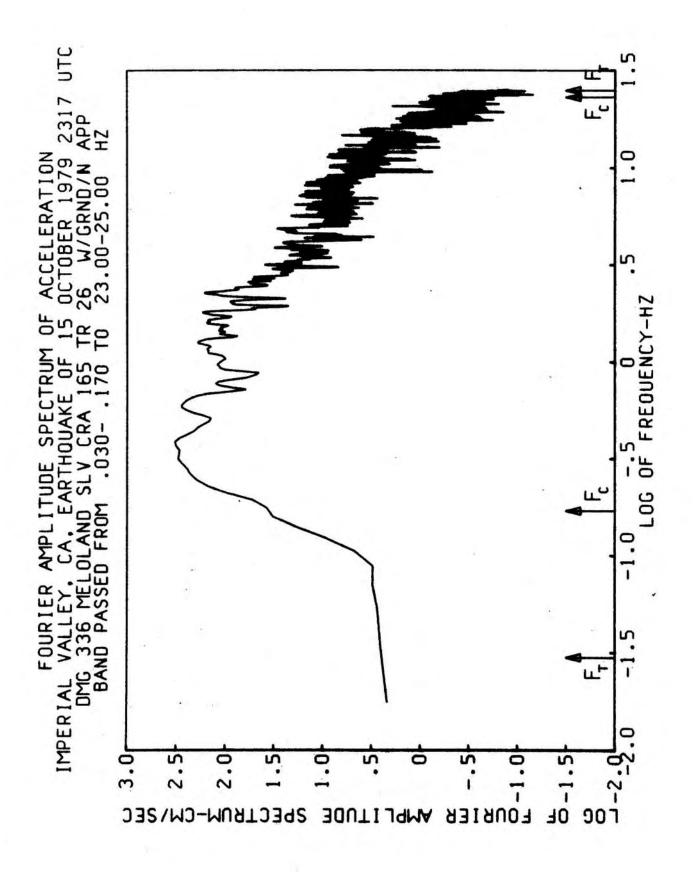


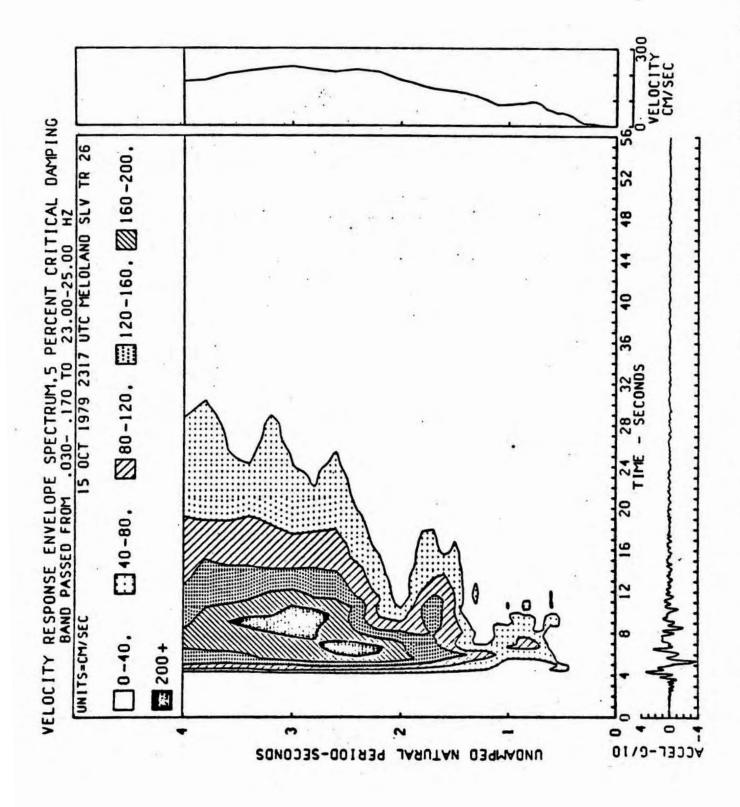
## RESPONSE SPECTRA

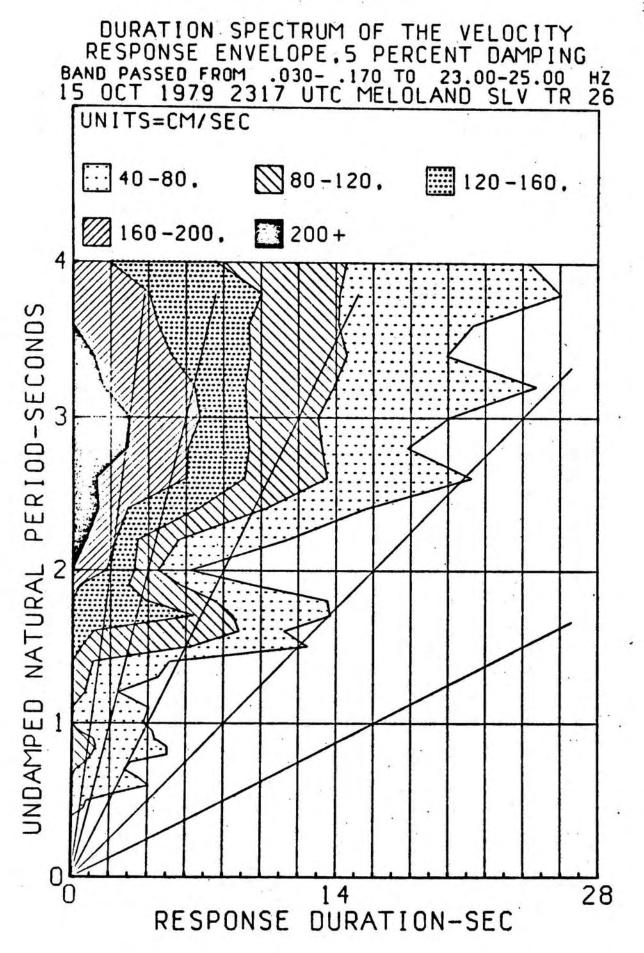
15 OCT 1979 2317 UTC MELOLAND SLV TR 26 0,2,5,10,20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



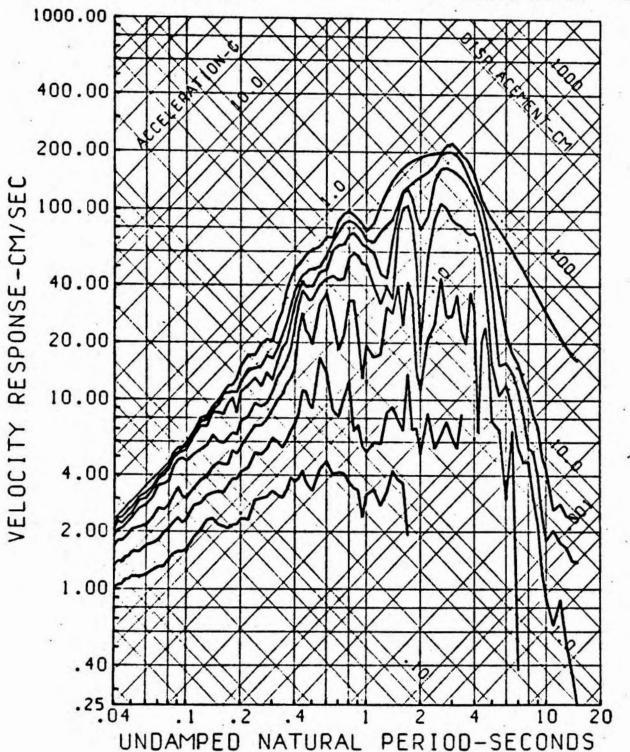


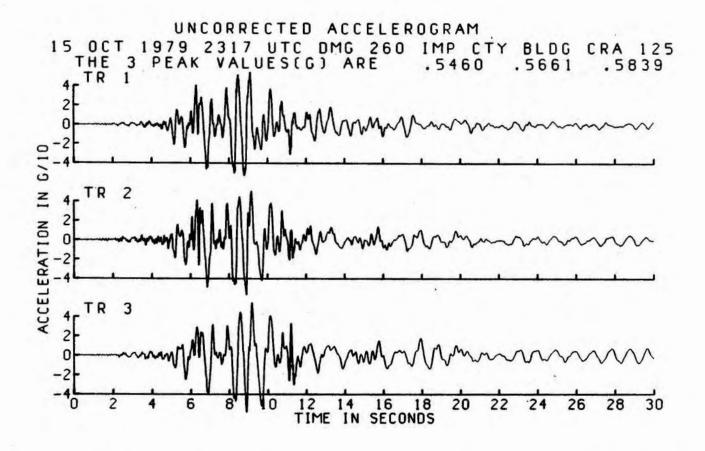




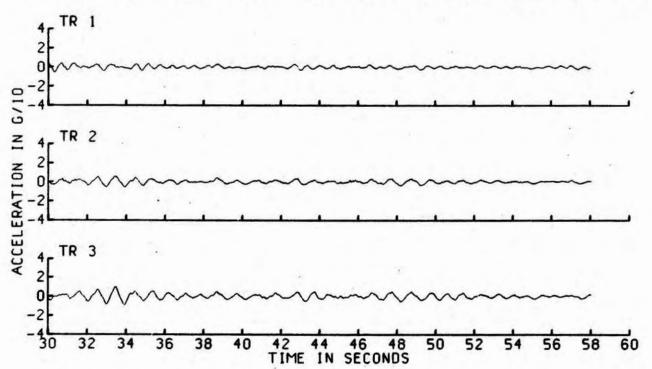


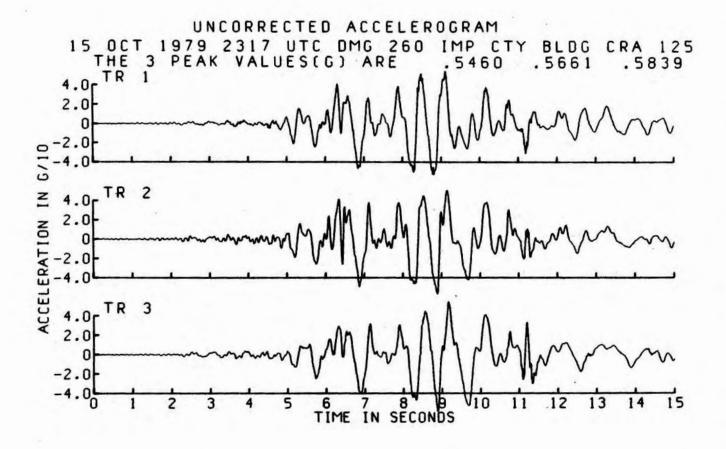
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC MELOLAND SLV TR 26 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

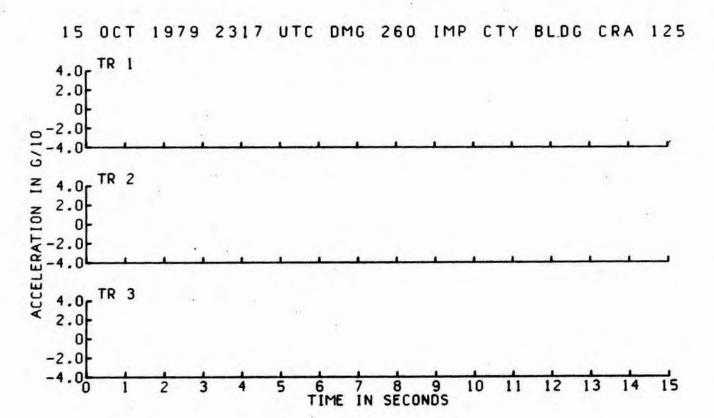




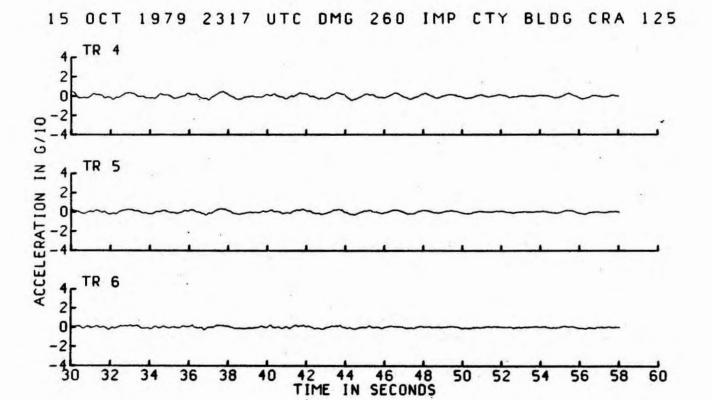


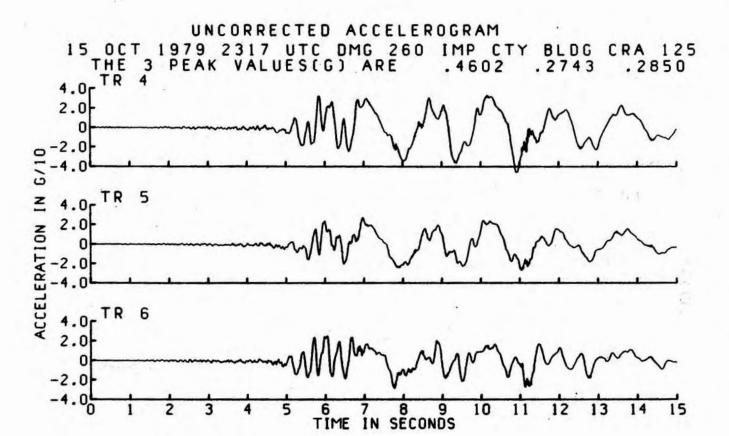


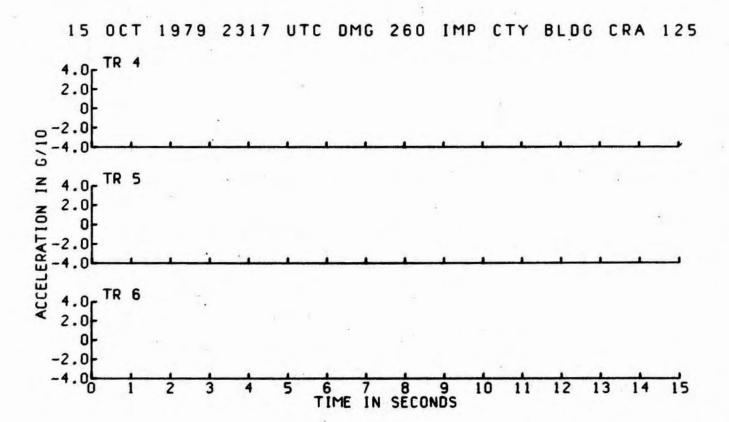


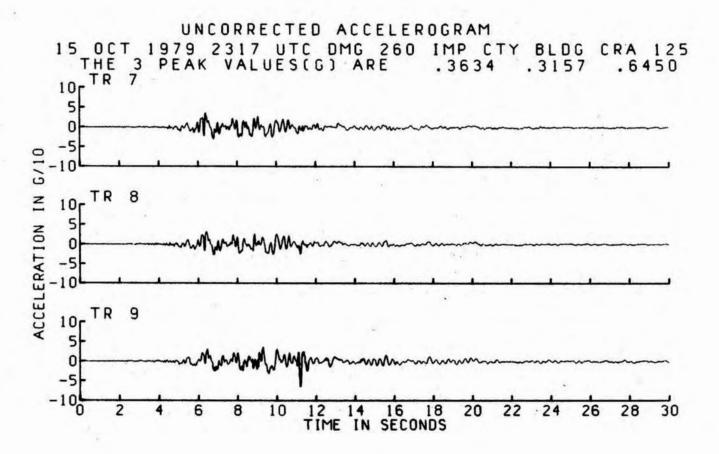


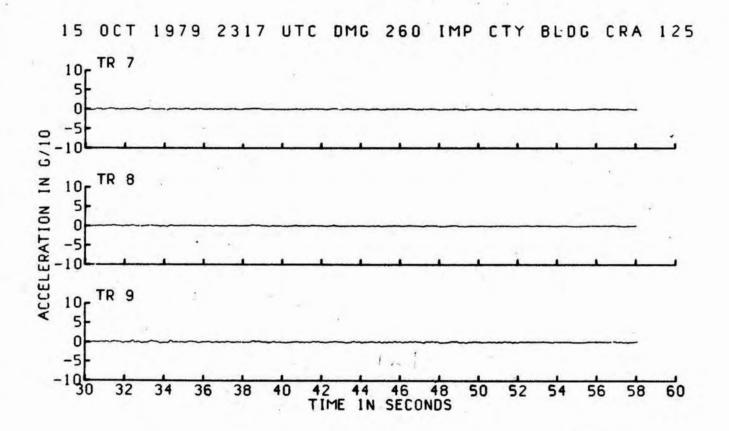
UNCORRECTED ACCELEROGRAM 15 OCT 1979 2317 UTC DMG 260 THE 3 PEAK VALUES(G) ARE IMP CTY BLDG .4602 .2743 .2850 ACCELERATION IN G/10 TR TR -2 -4L 12 14 16 18 TIME IN SECONDS 

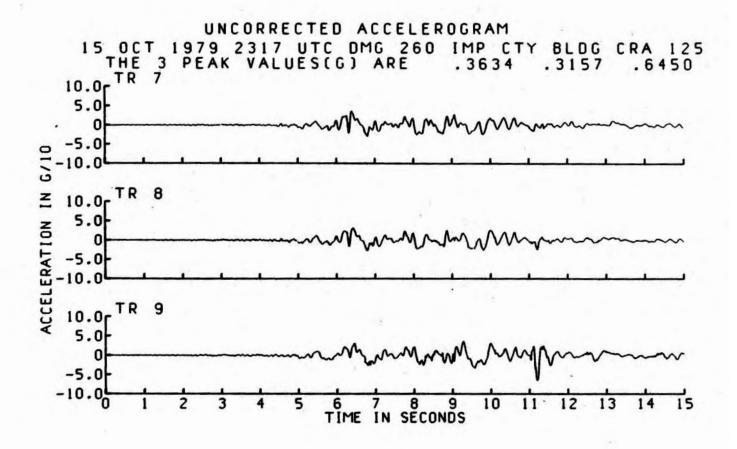


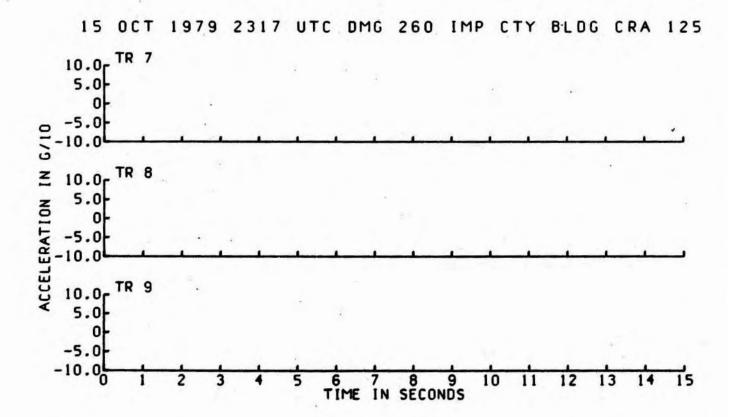


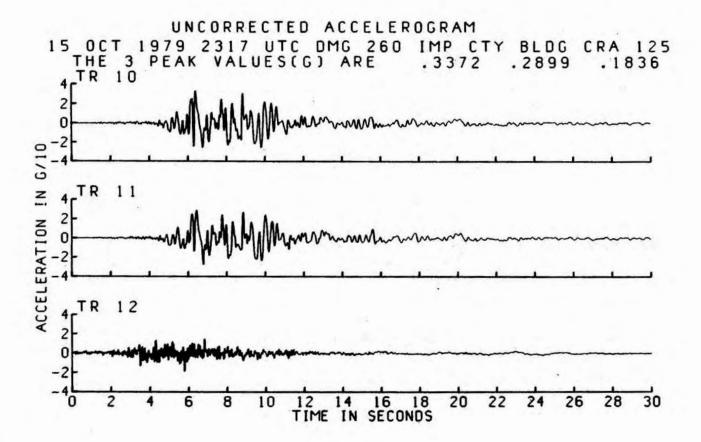


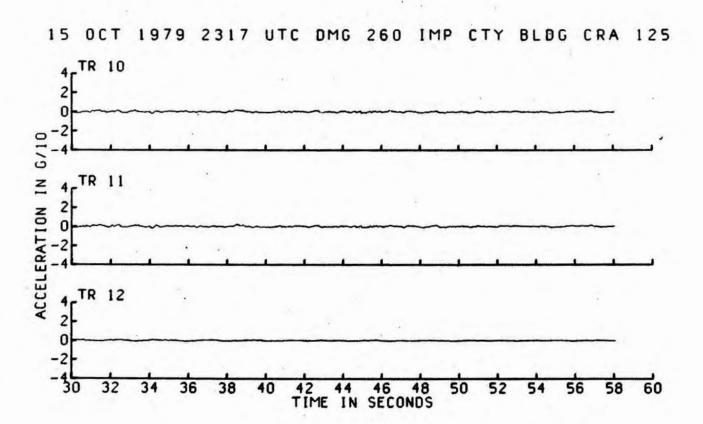


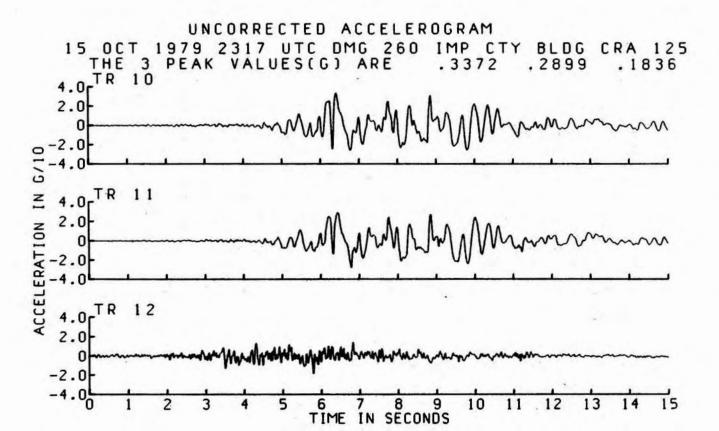


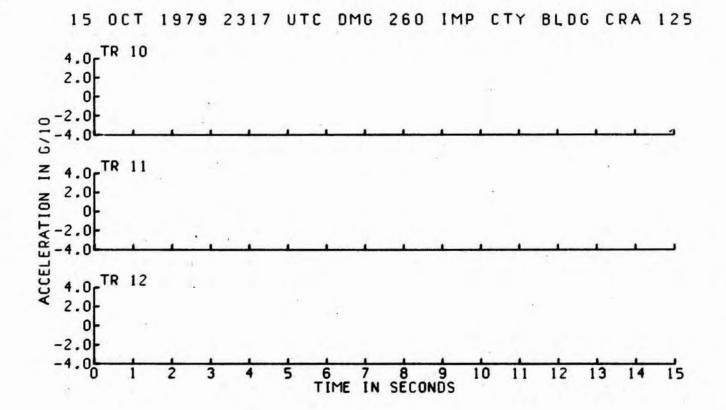


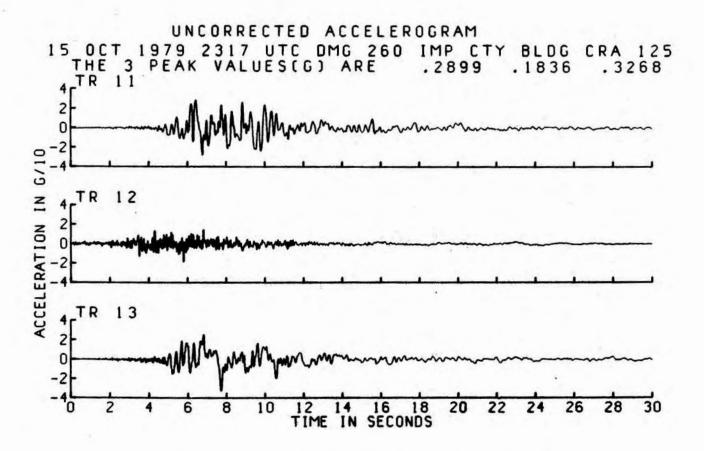




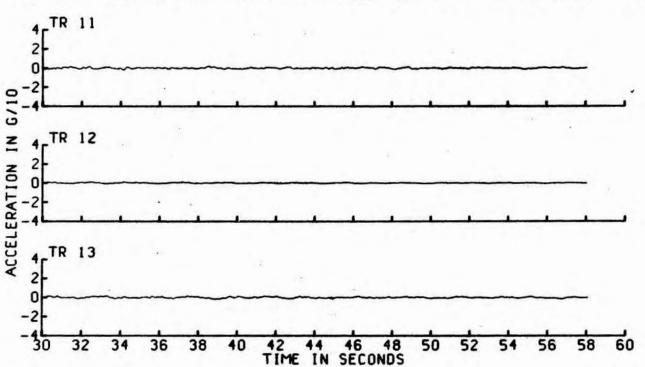


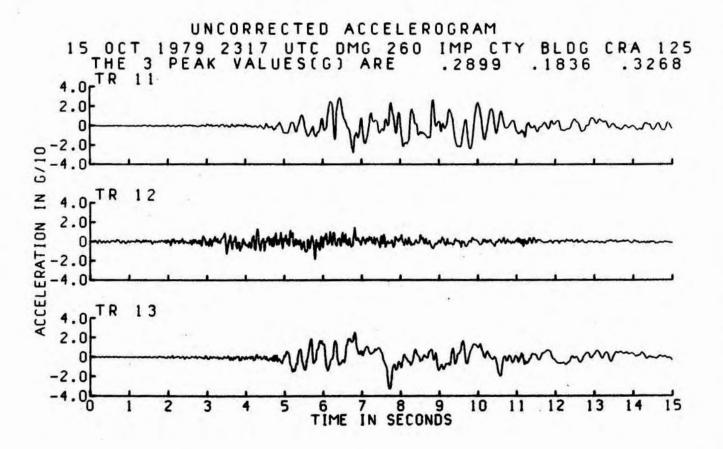


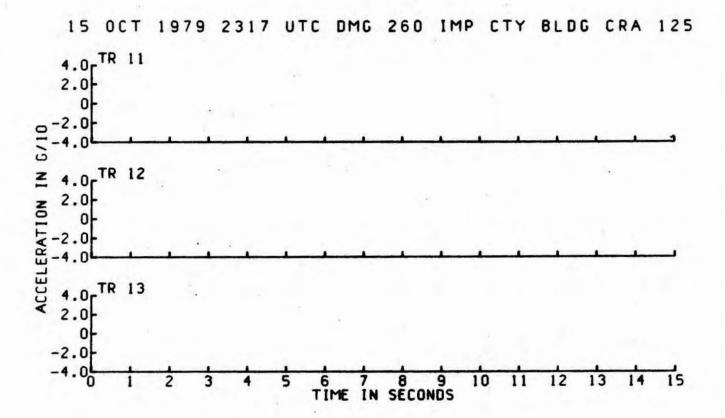


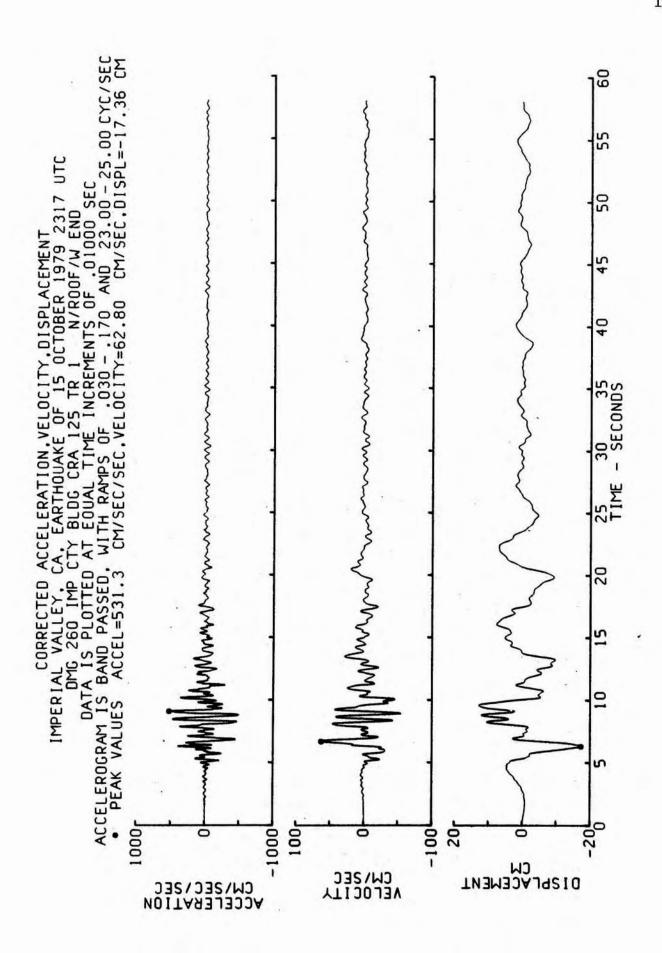




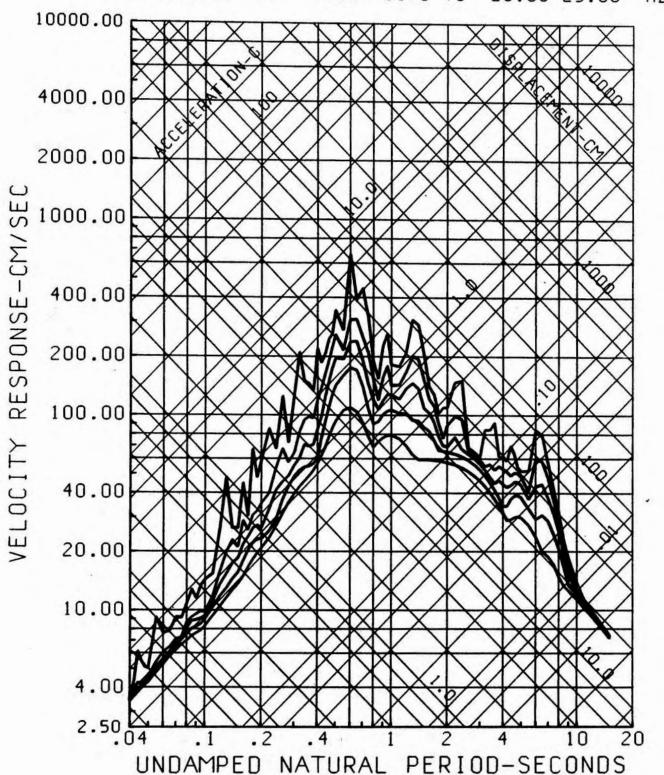


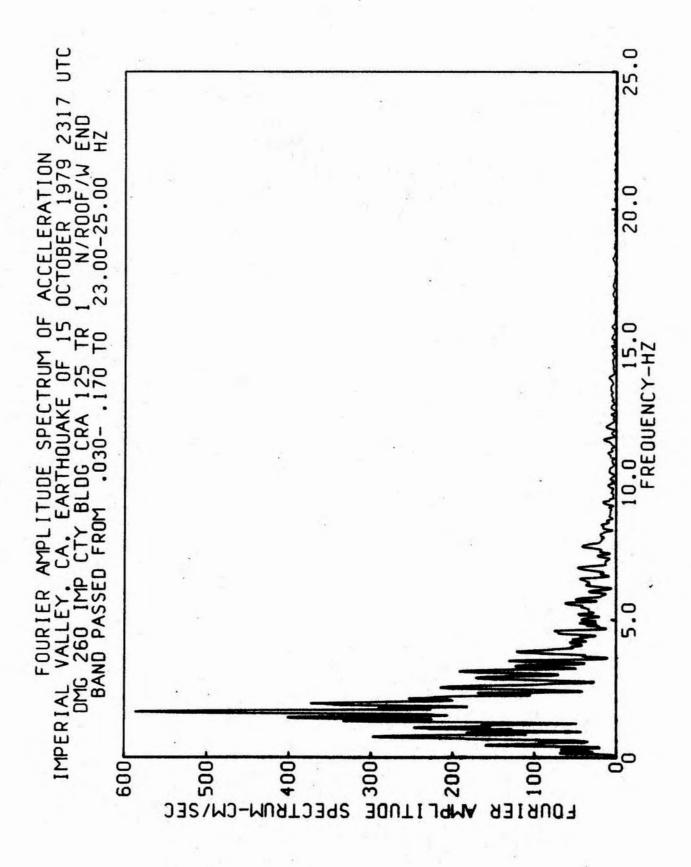


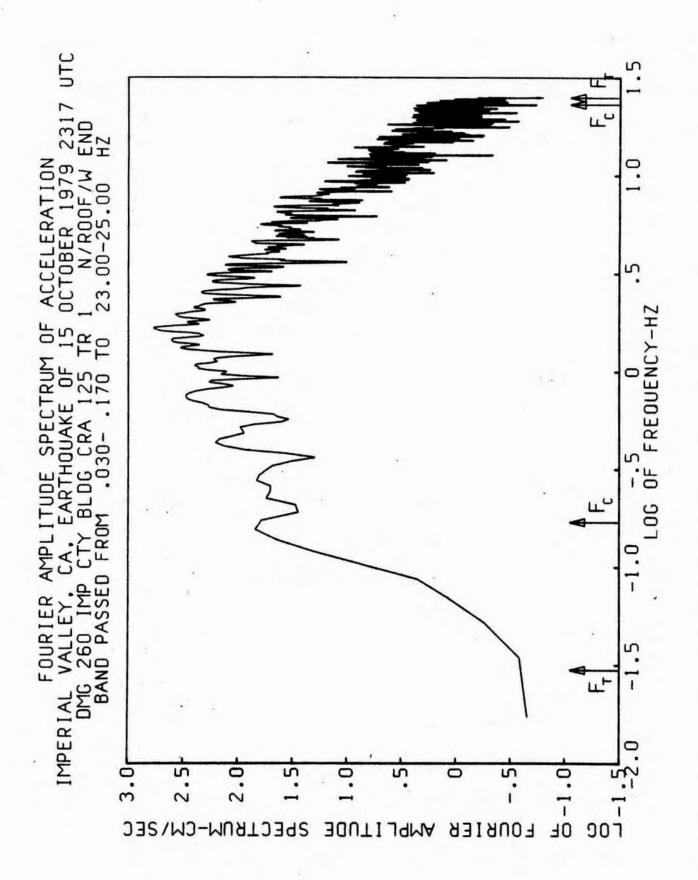


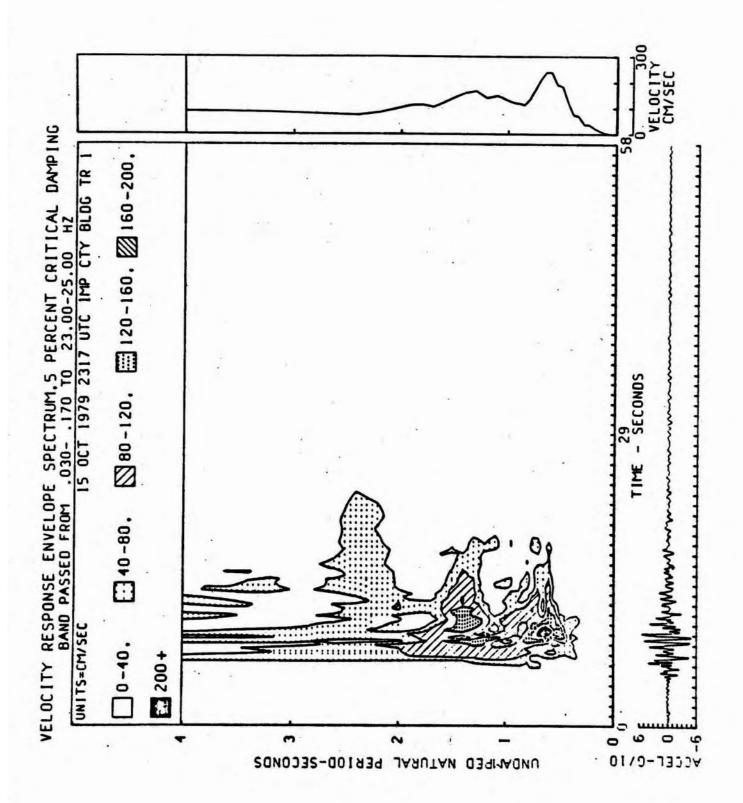


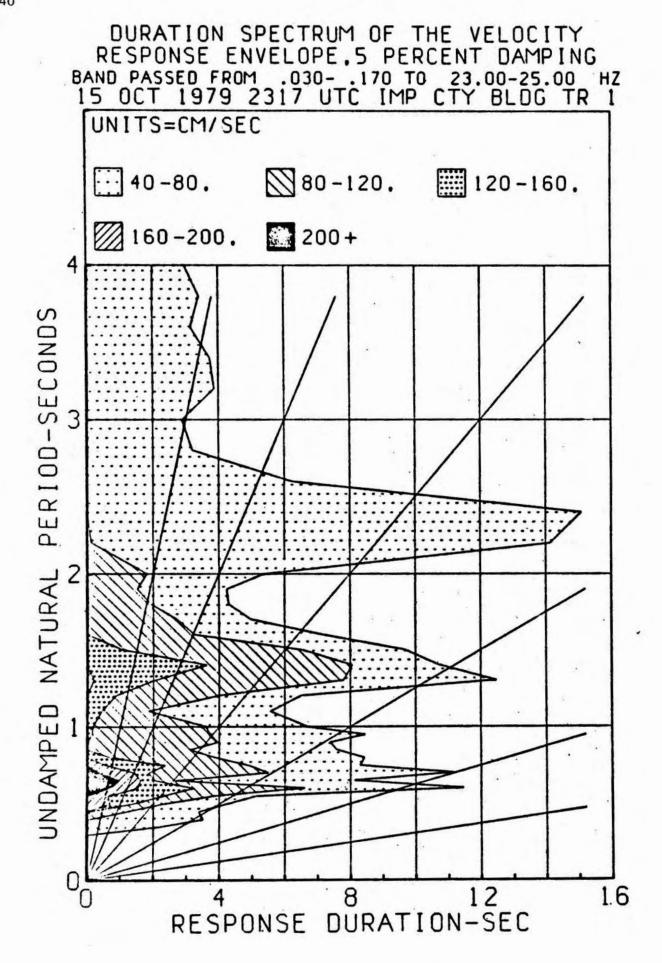
## RESPONSE SPECTRA 15 OCT 1979 2317 UTC IMP CTY BLDG TR 1 0,2,5,10,20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



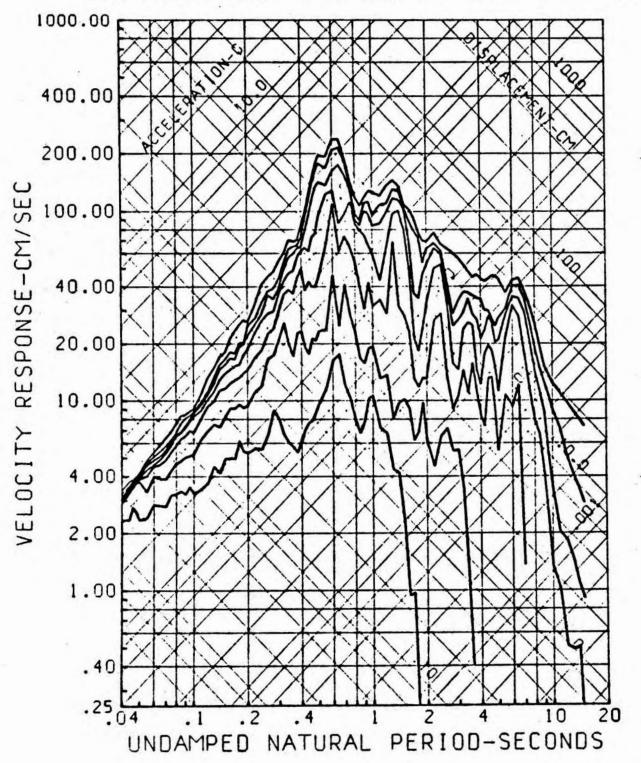


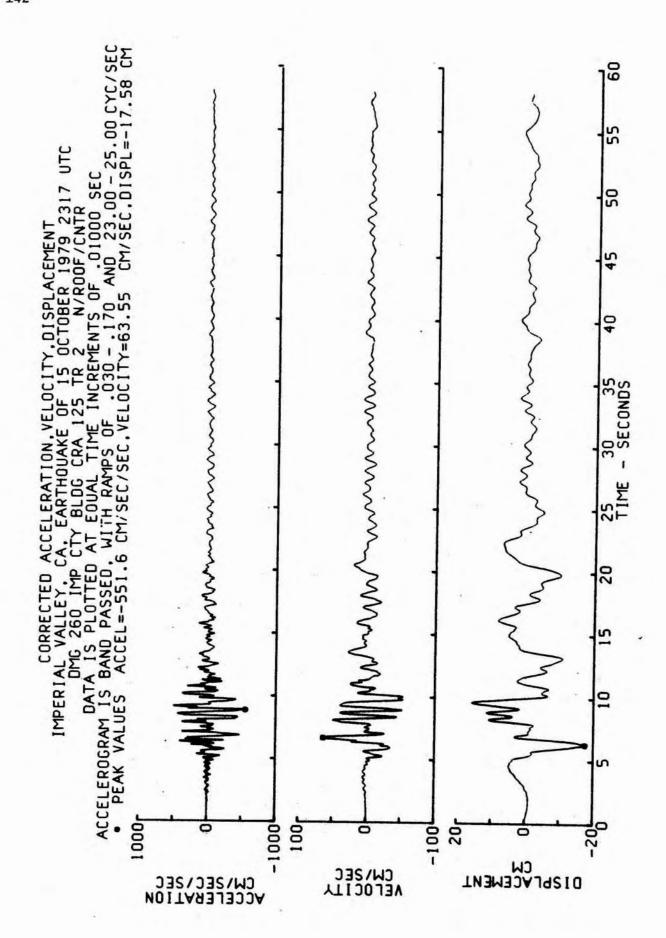






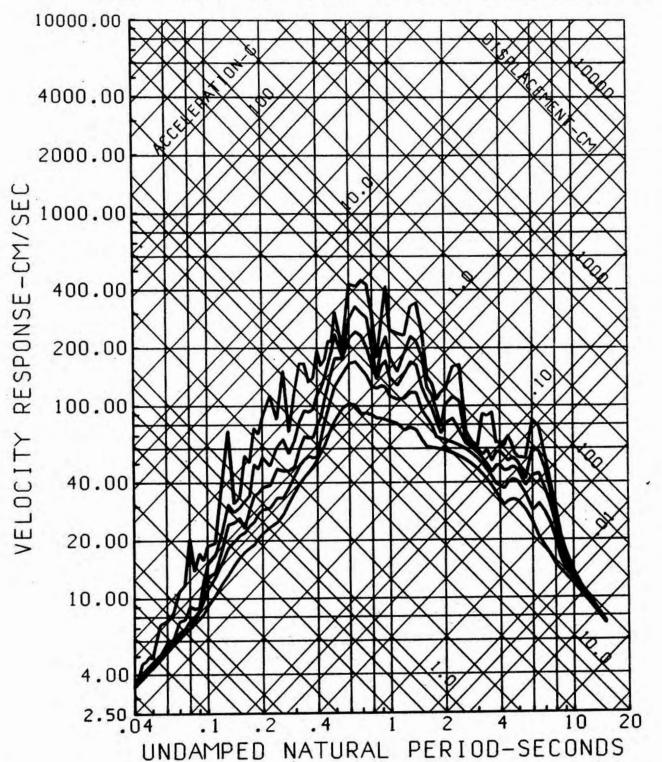
SPECTRA OF AMPLITUDES SUSTAINED .
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 1
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

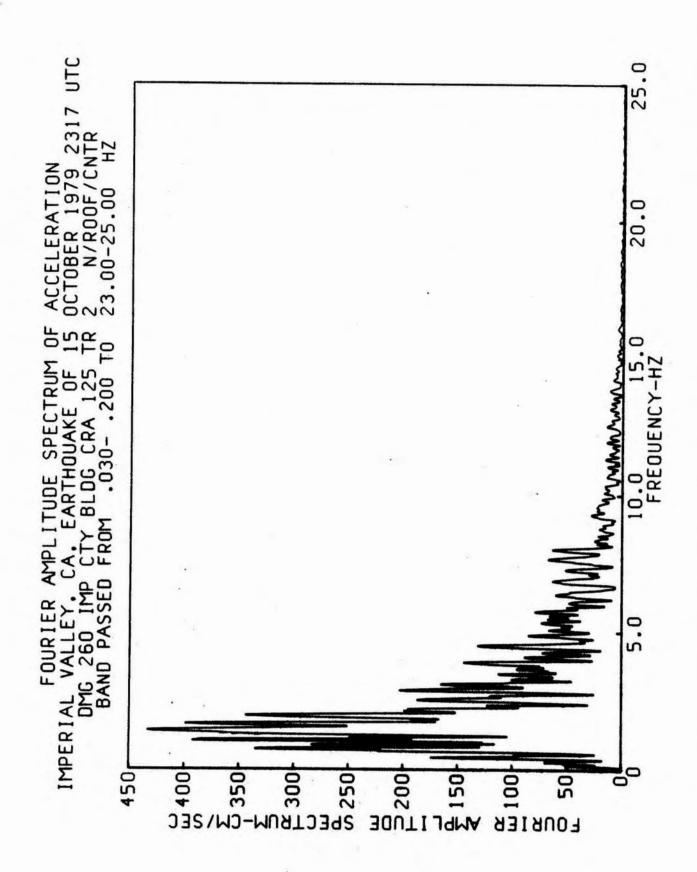


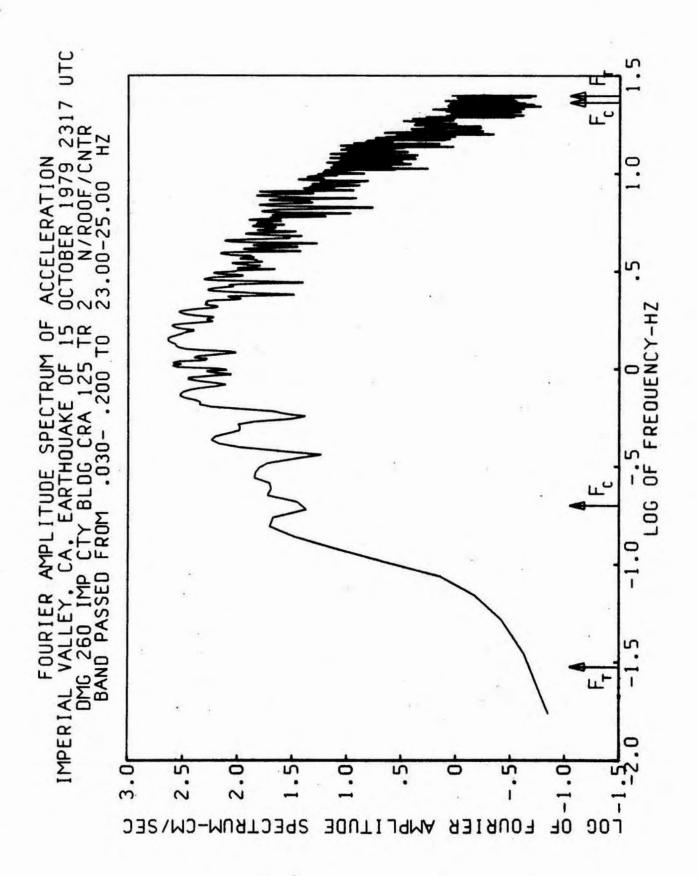


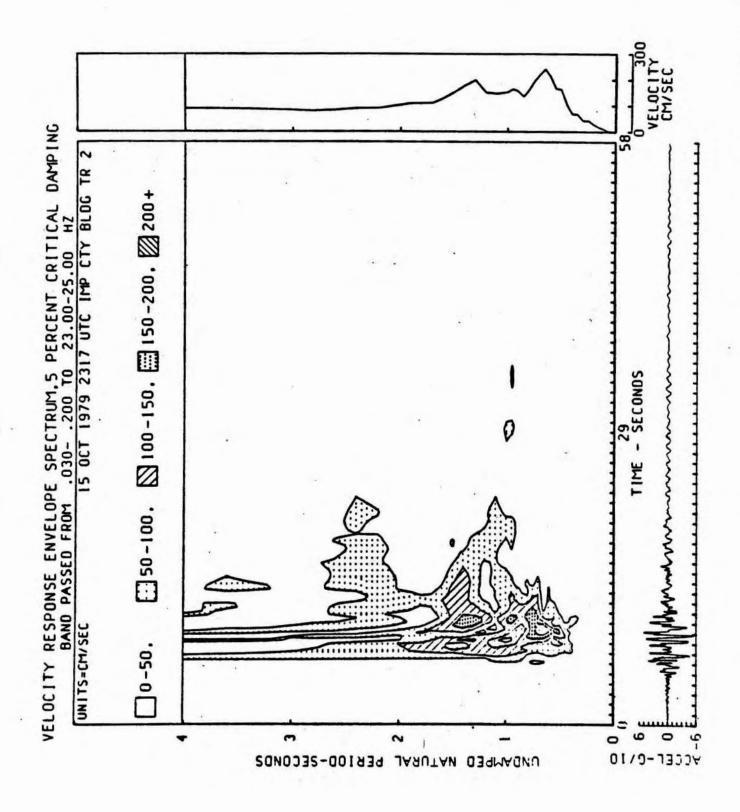
RESPONSE SPECTRA

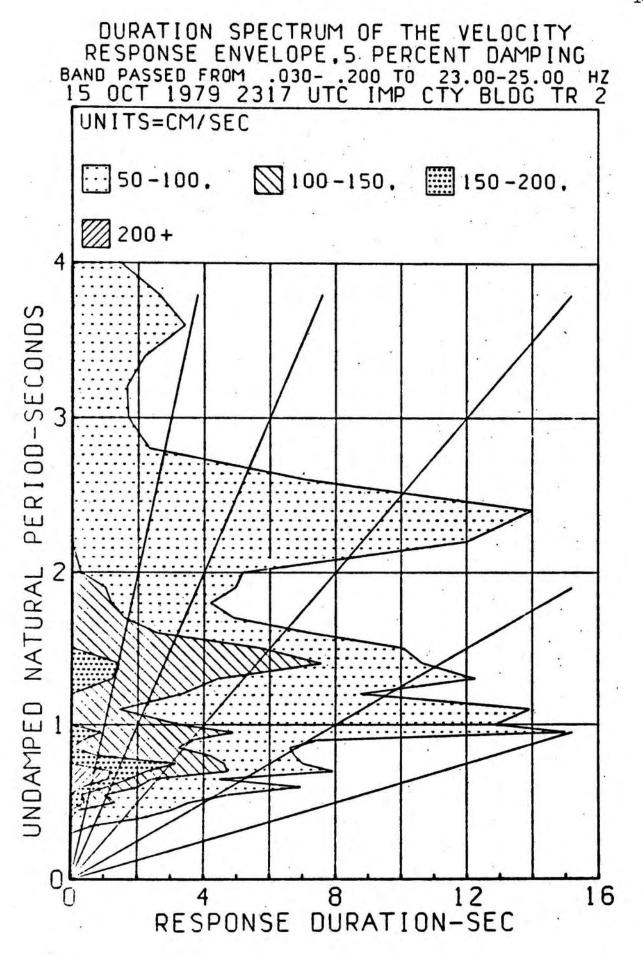
15 OCT 1979 2317 UTC IMP CTY BLDG TR 2
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



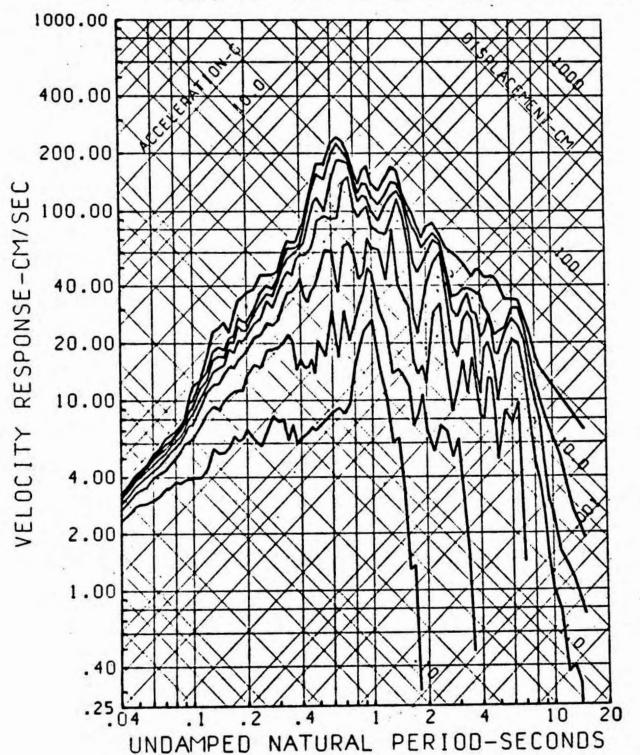


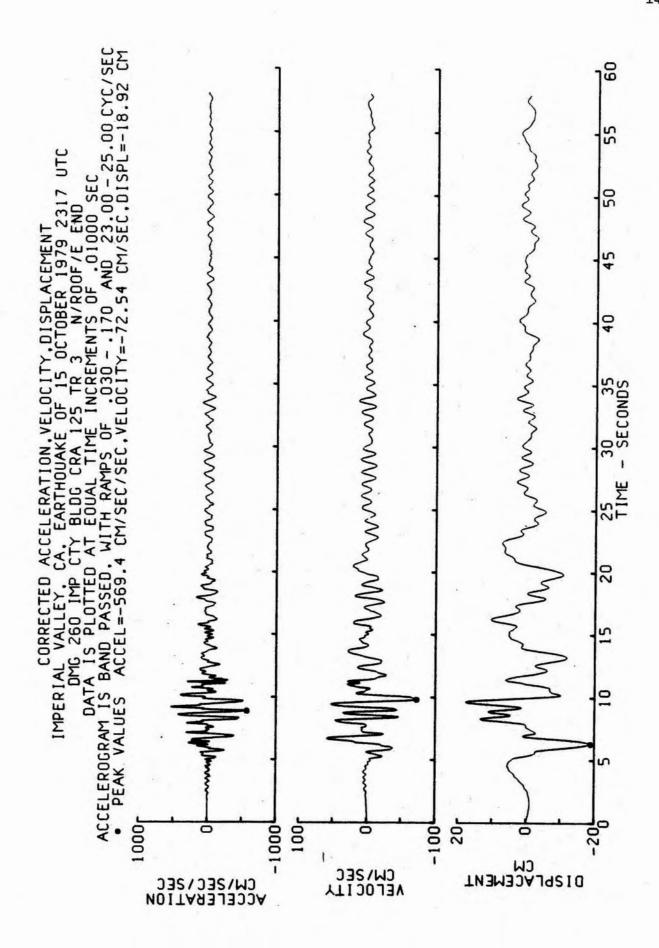






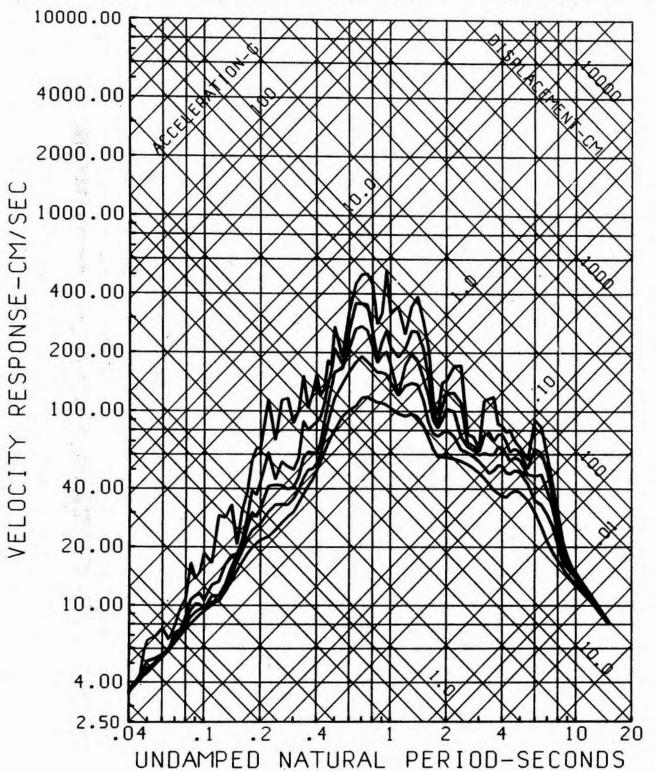
SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 2
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .200 TO 23.00-25.00 HZ

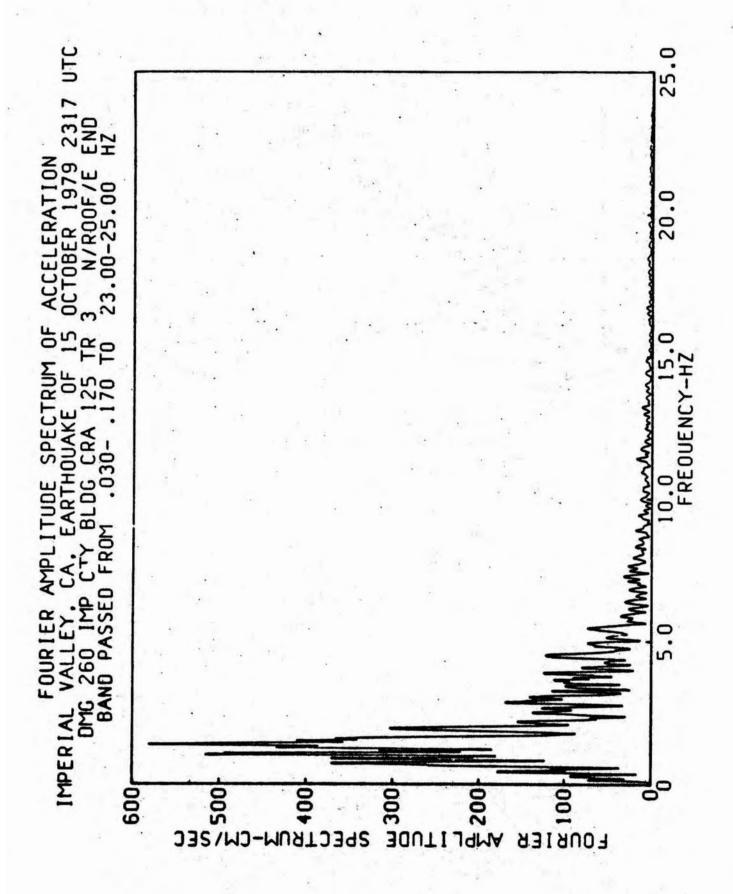


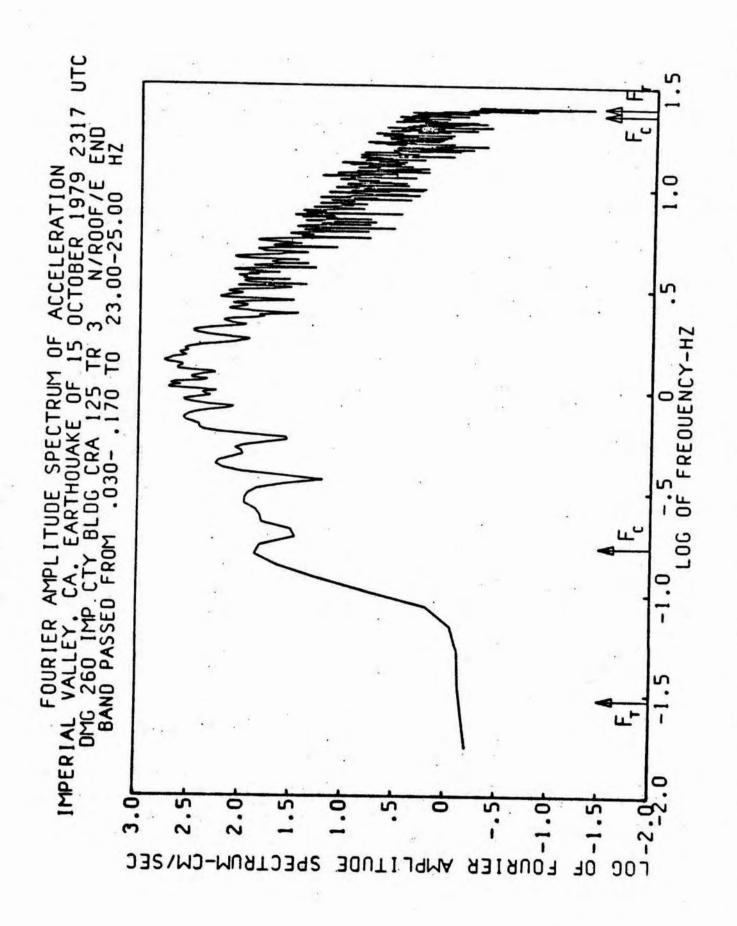


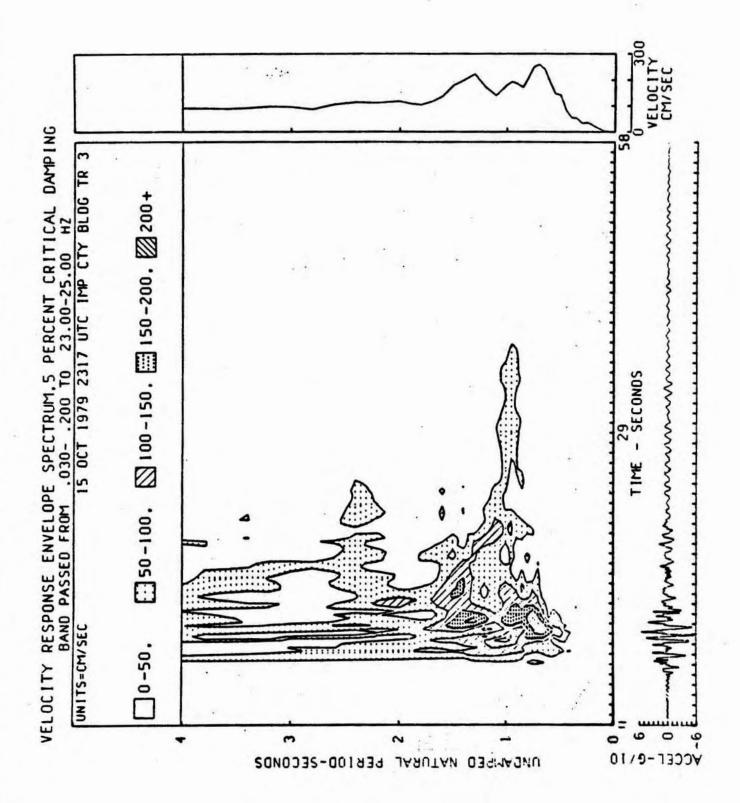
RESPONSE SPECTRA

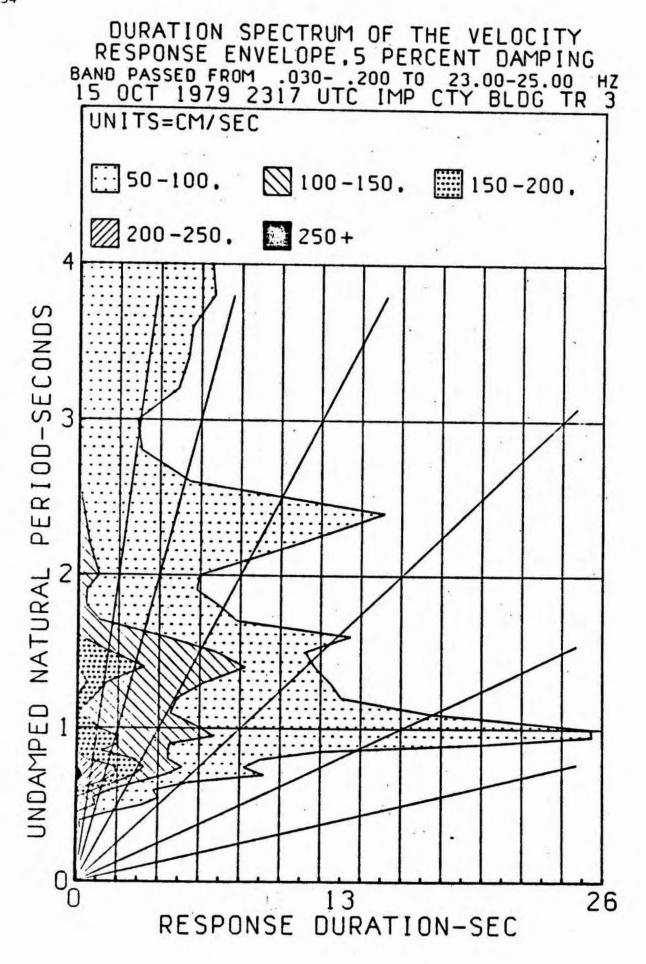
15 OCT 1979 2317 UTC IMP CTY BLDG TR 3
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



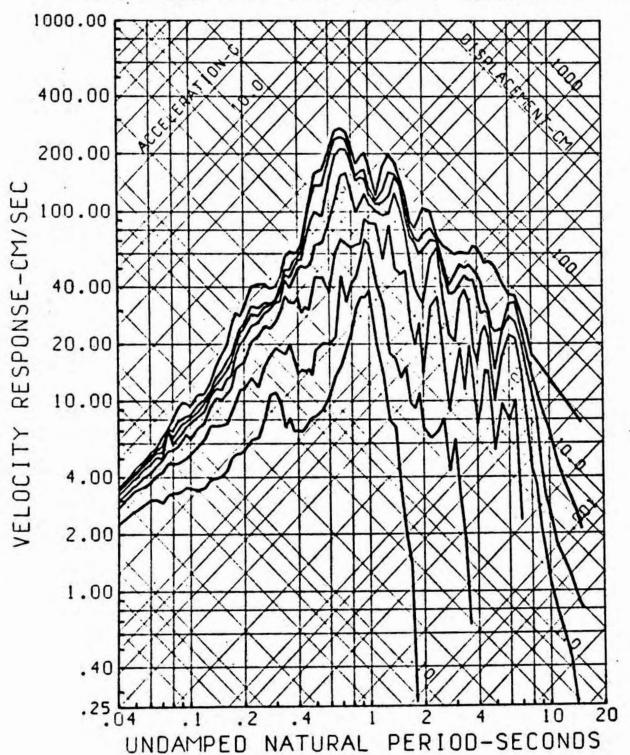


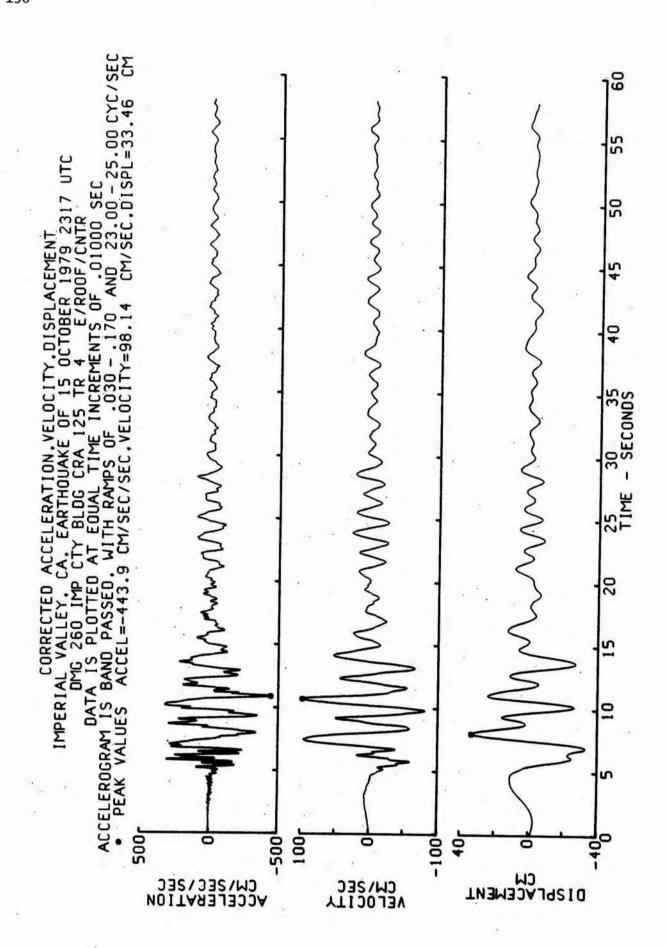






SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 3
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .200 TO 23.00-25.00 HZ

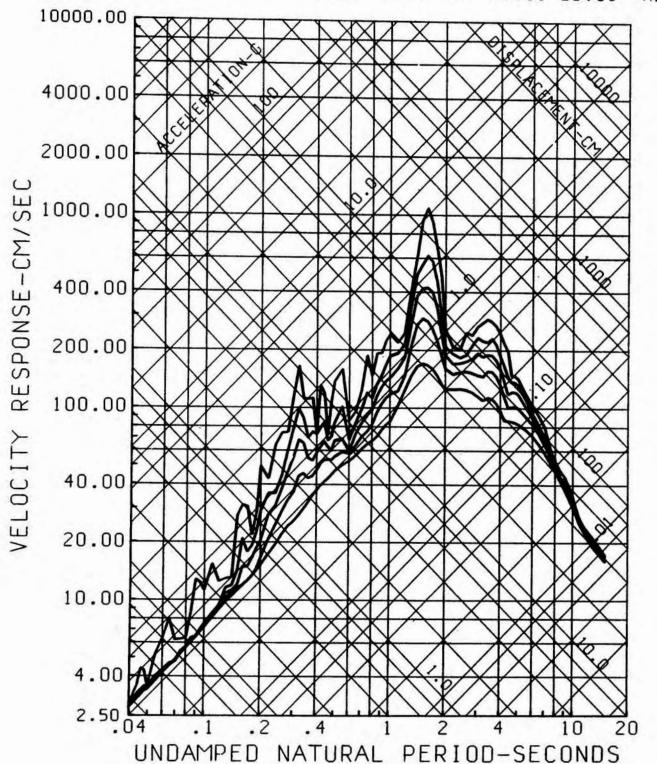


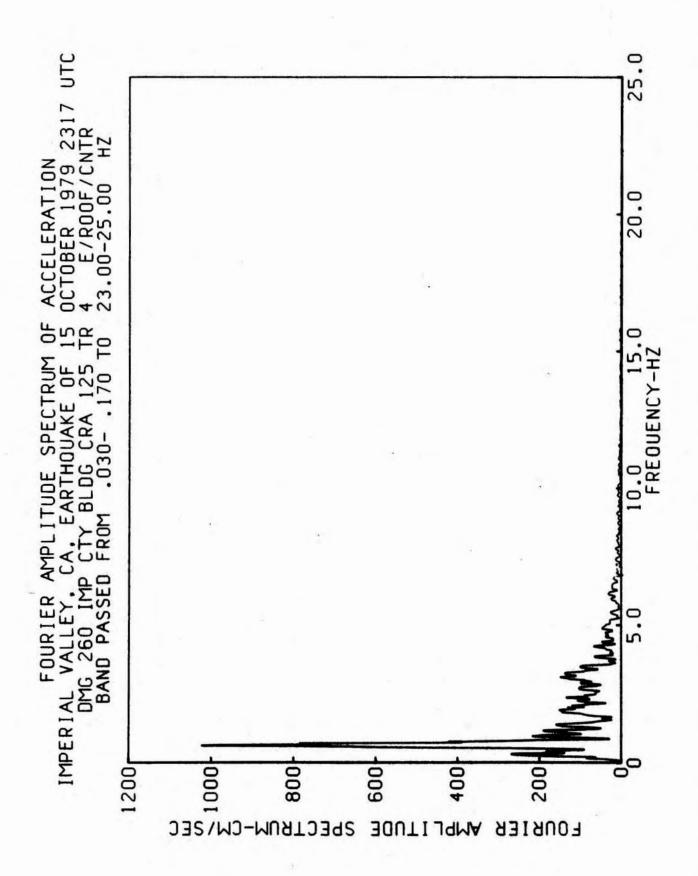


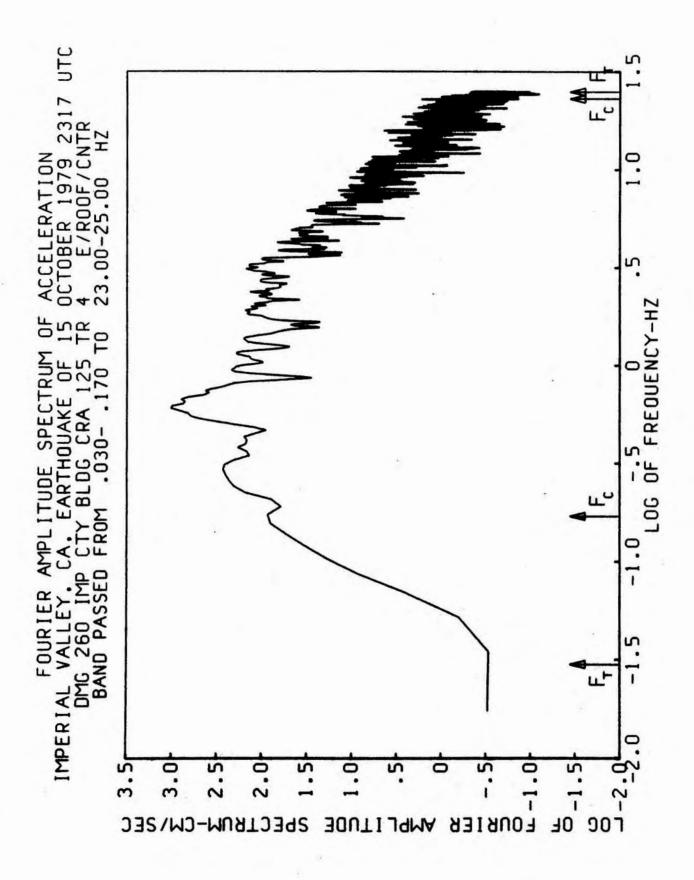
RESPONSE SPECTRA

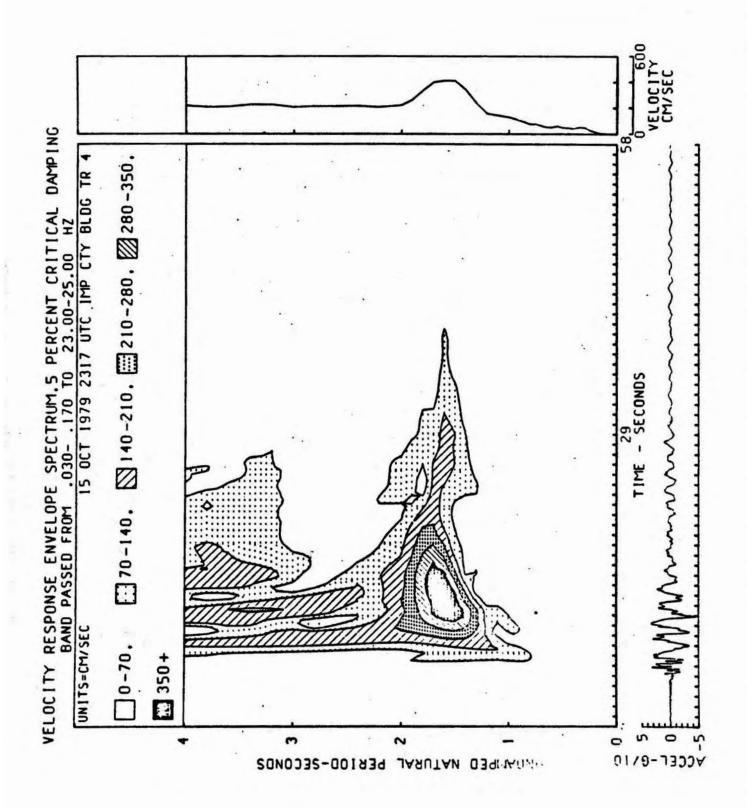
15 OCT 1979 2317 UTC IMP CTY BLDG TR 4

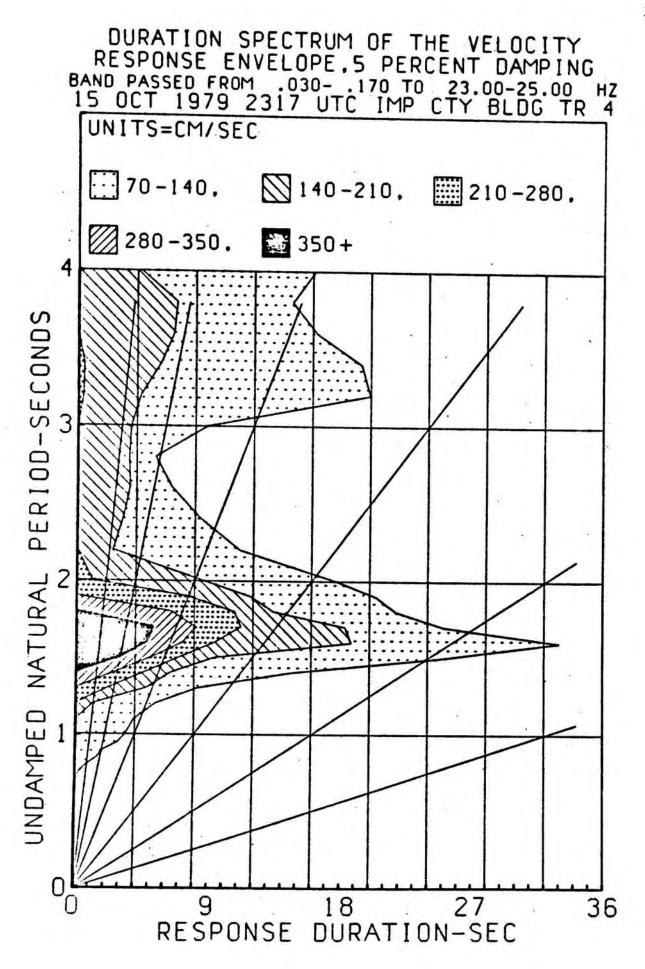
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



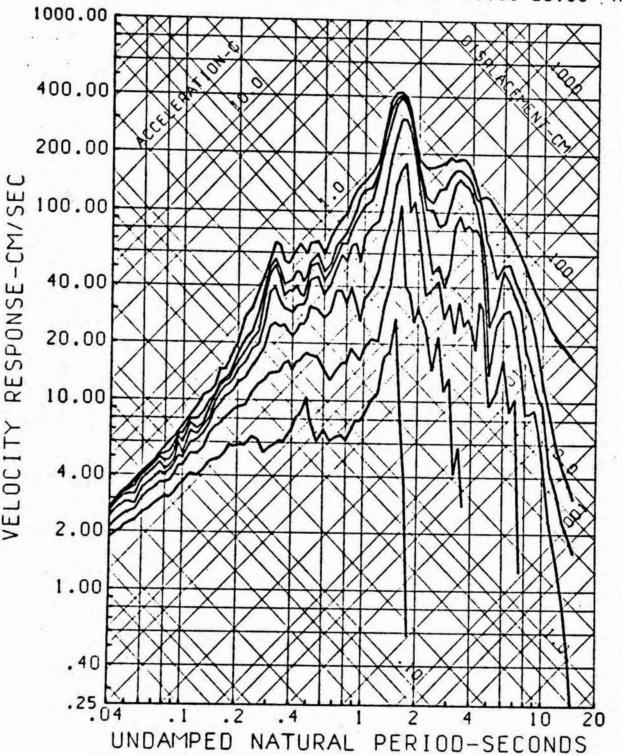


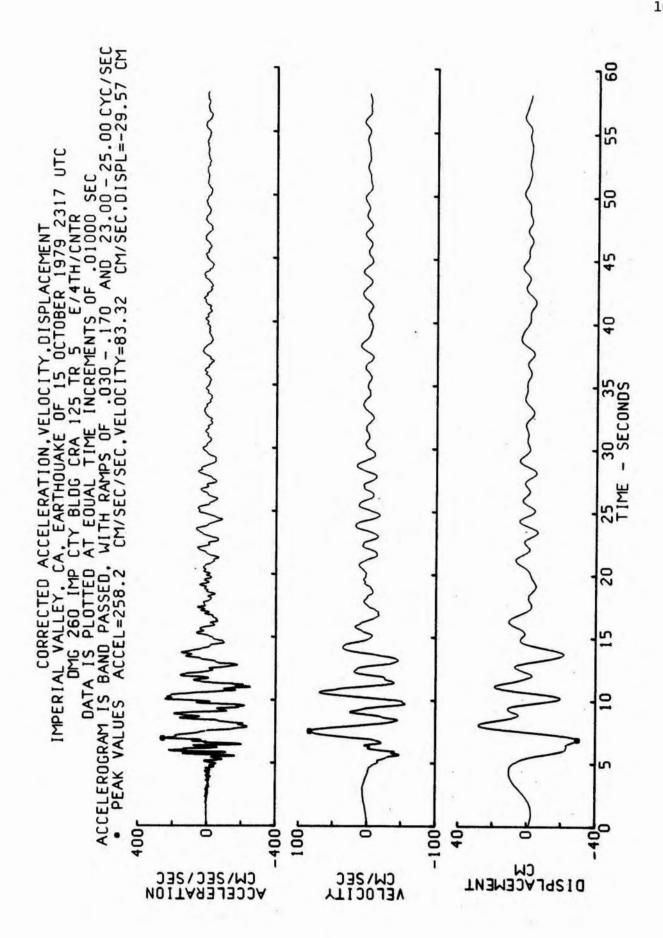






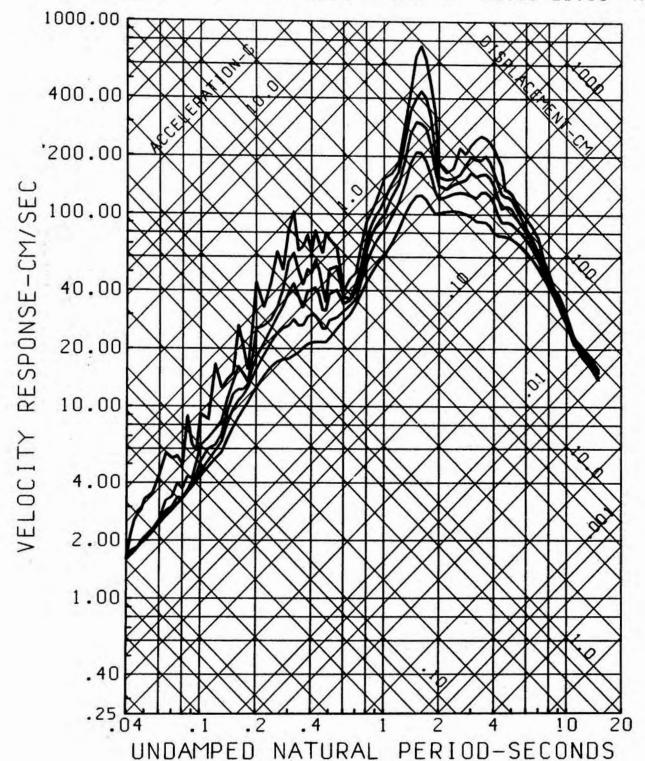
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC IMP CTY BLDG TR 4 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

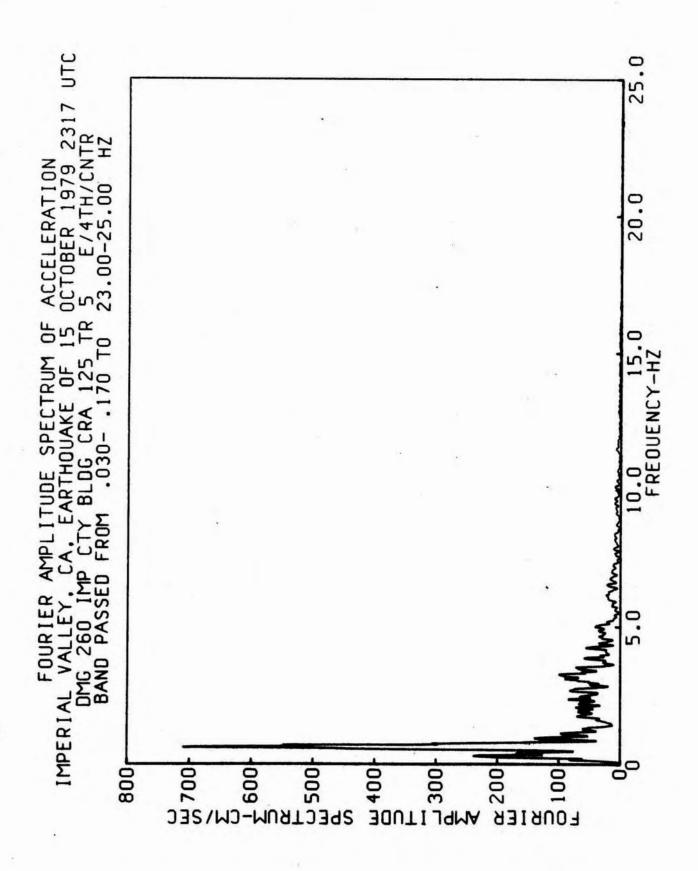


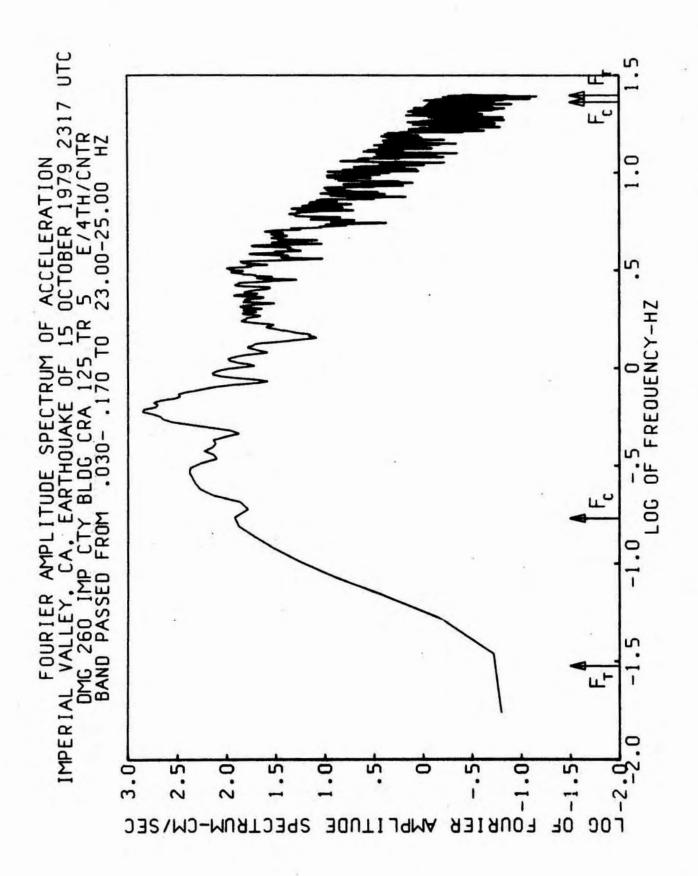


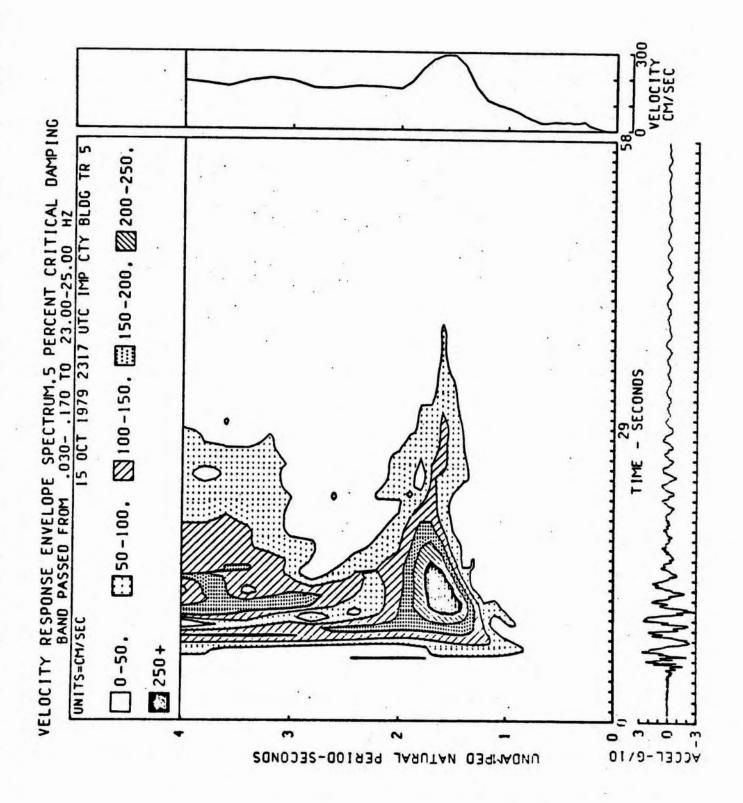
RESPONSE SPECTRA

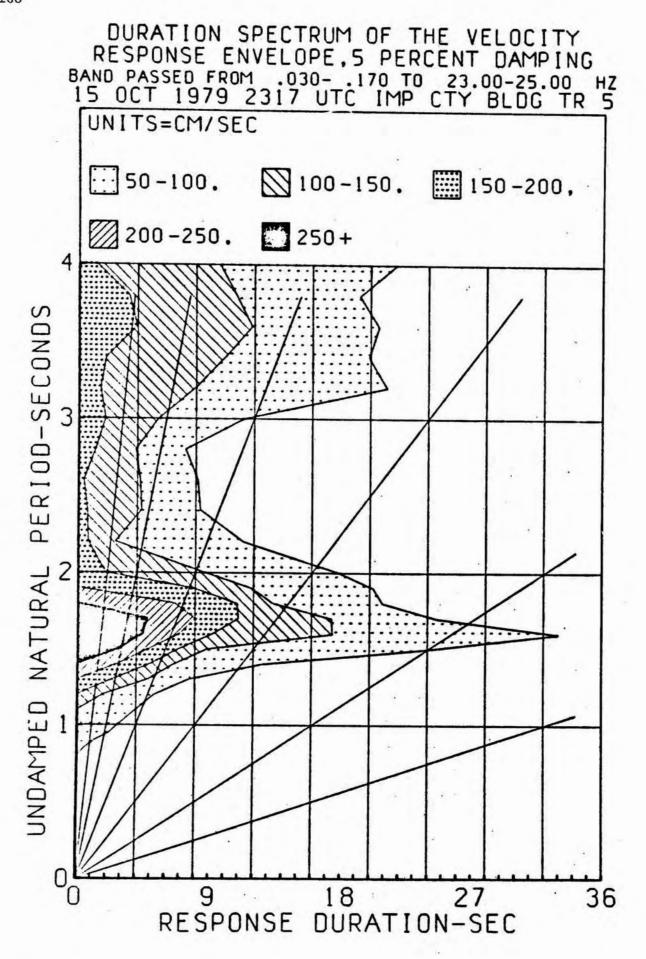
15 OCT 1979 2317 UTC IMP CTY BLDG TR 5
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



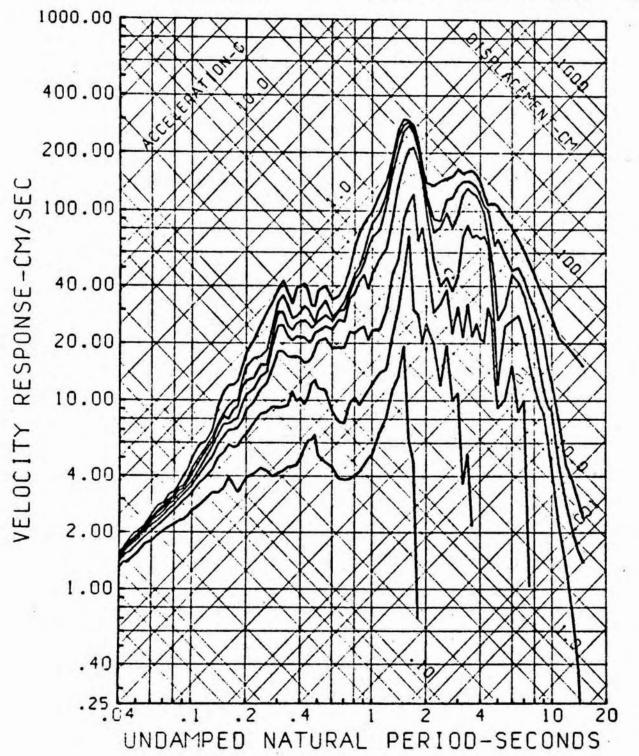


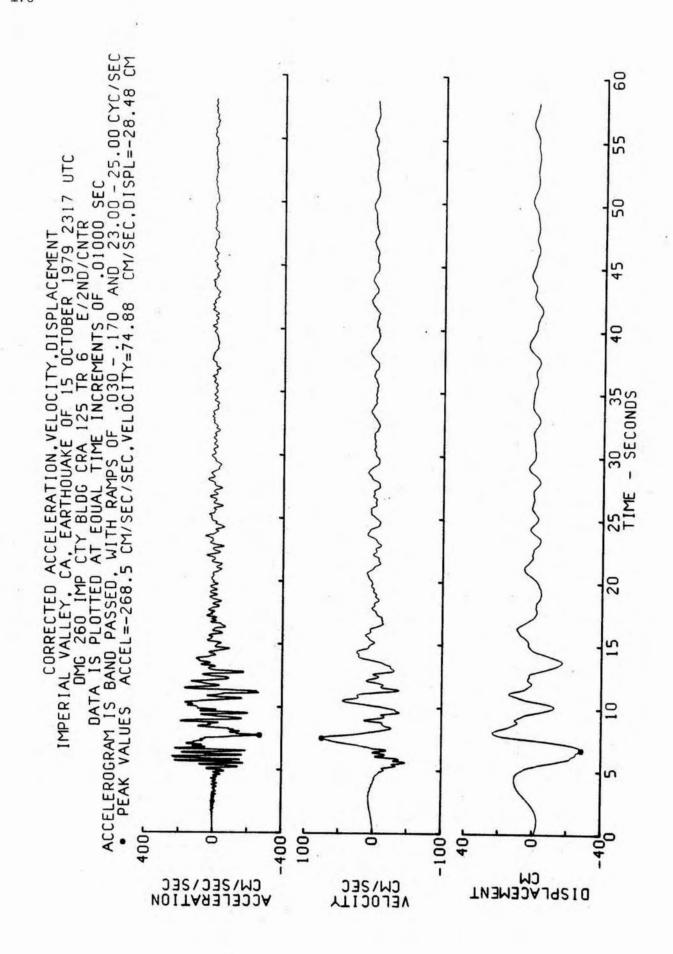






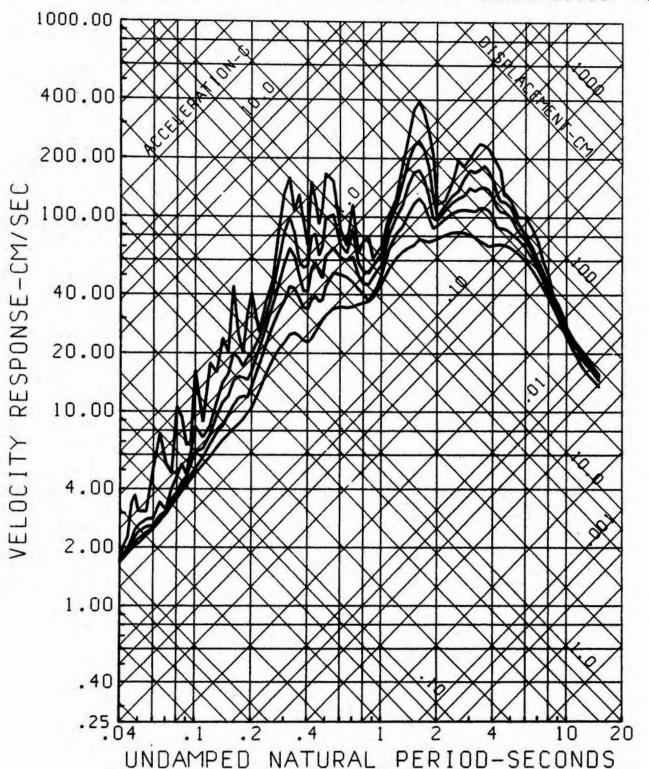
SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 5
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

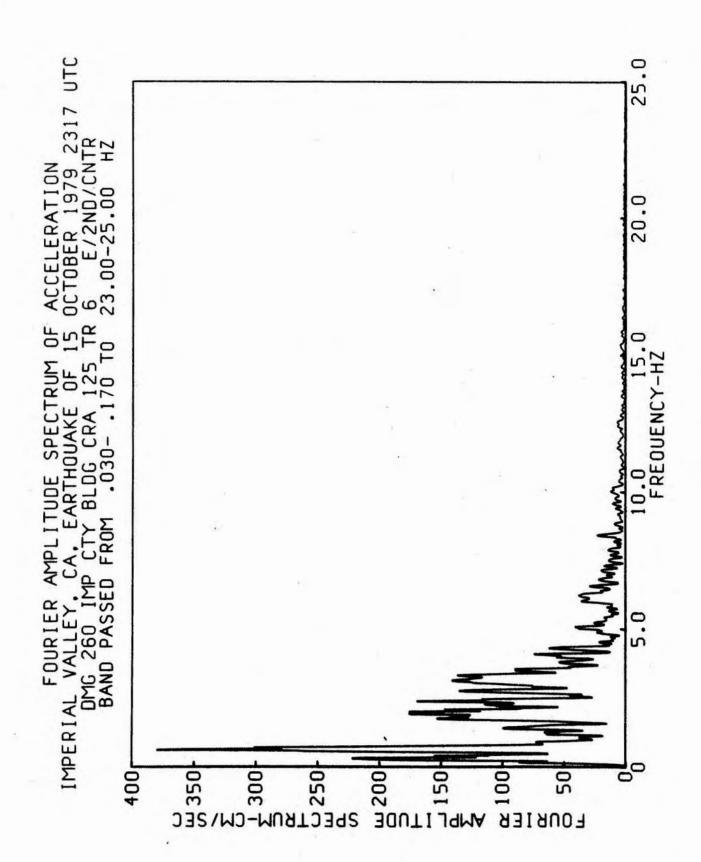


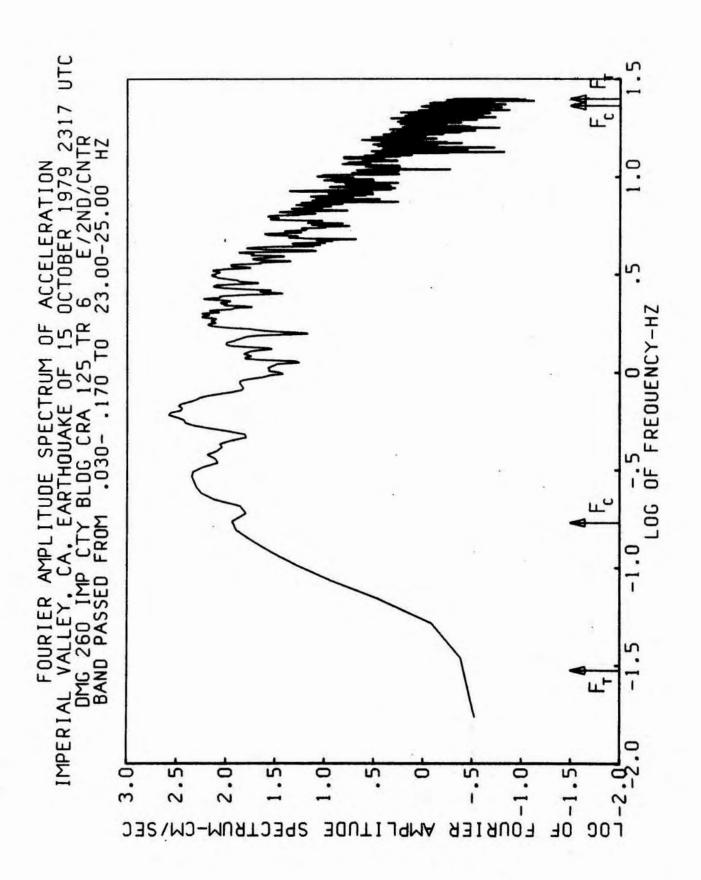


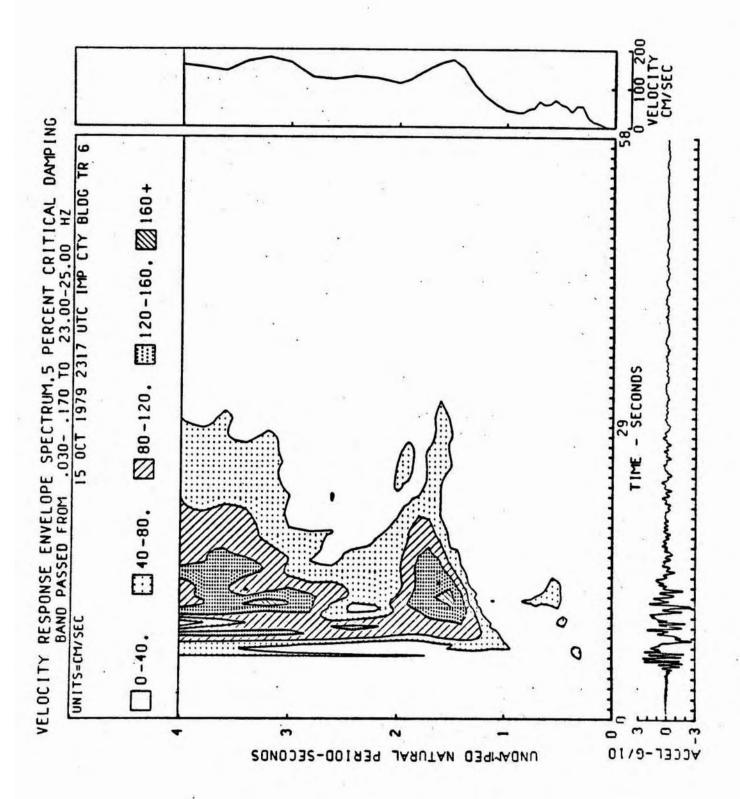
RESPONSE SPECTRA

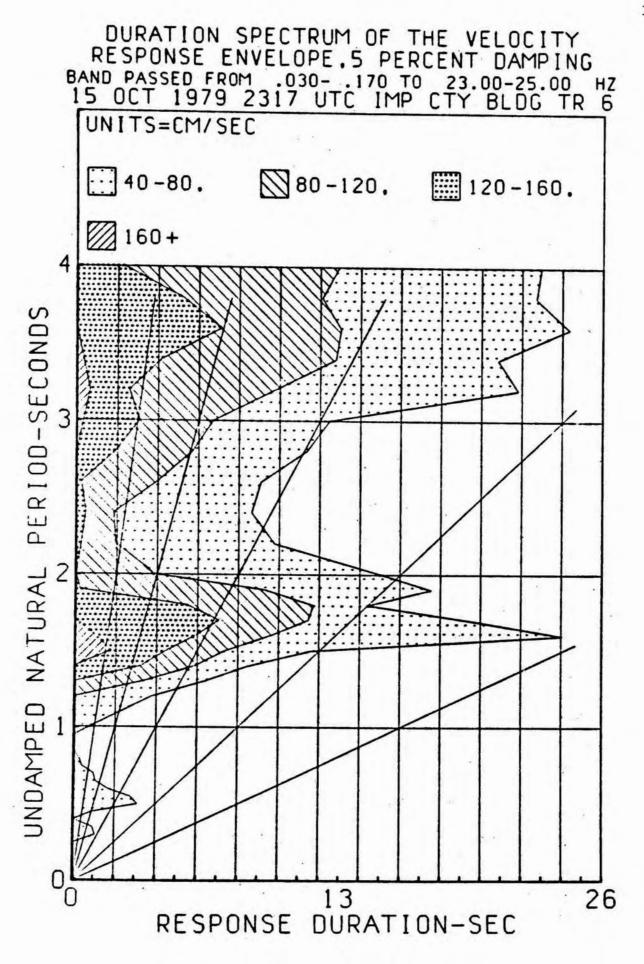
15 OCT 1979 2317 UTC IMP CTY BLDG TR 6
0.2.5.10.20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



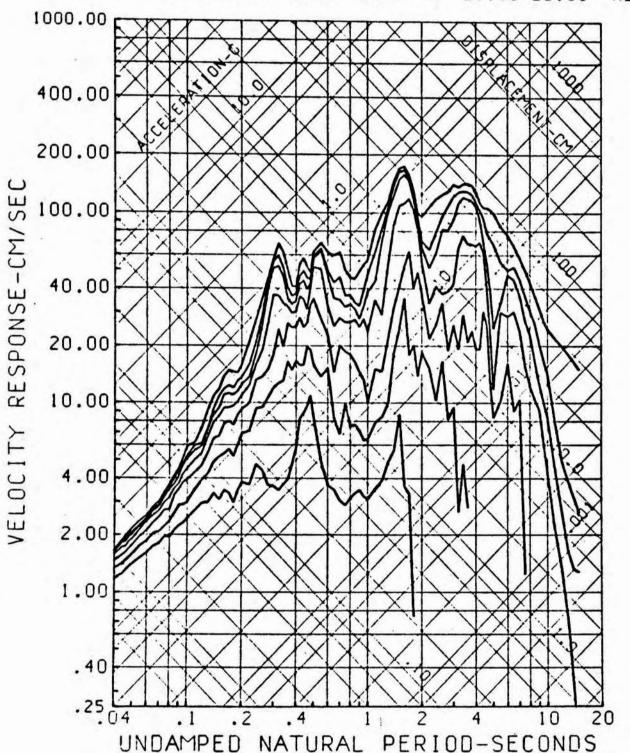


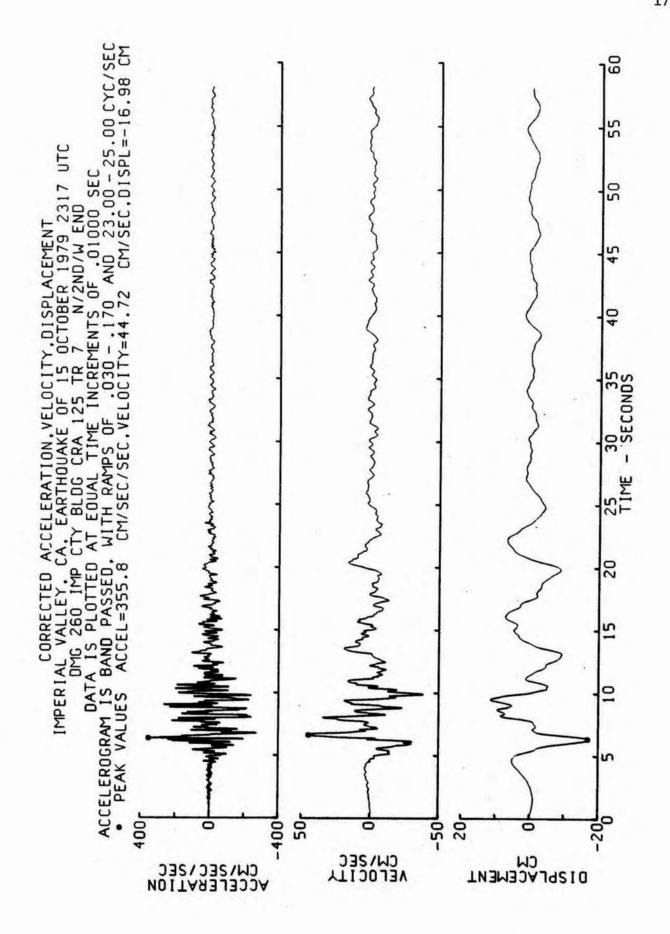






SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 6
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

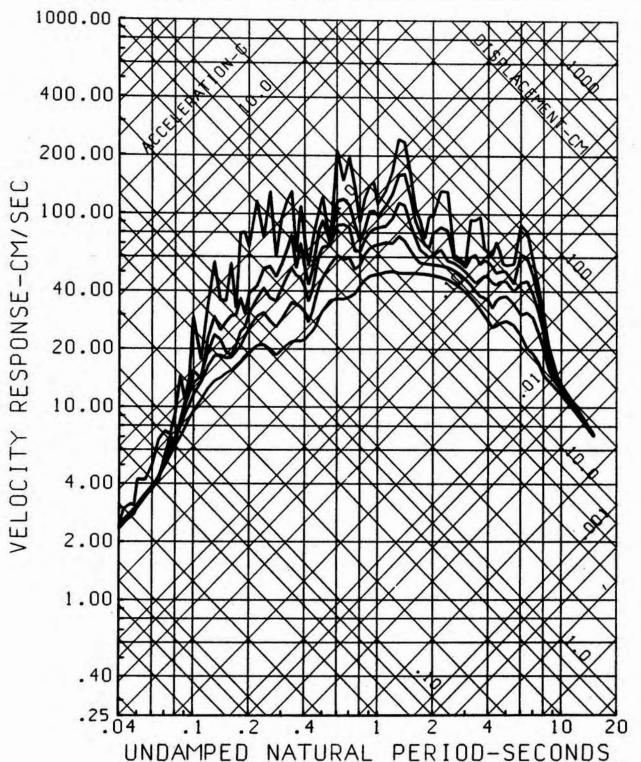


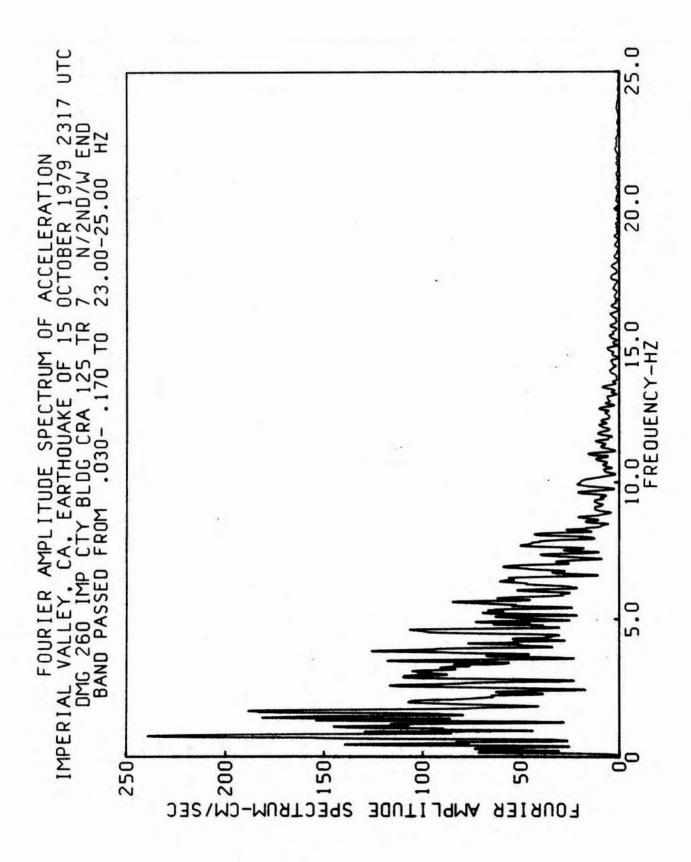


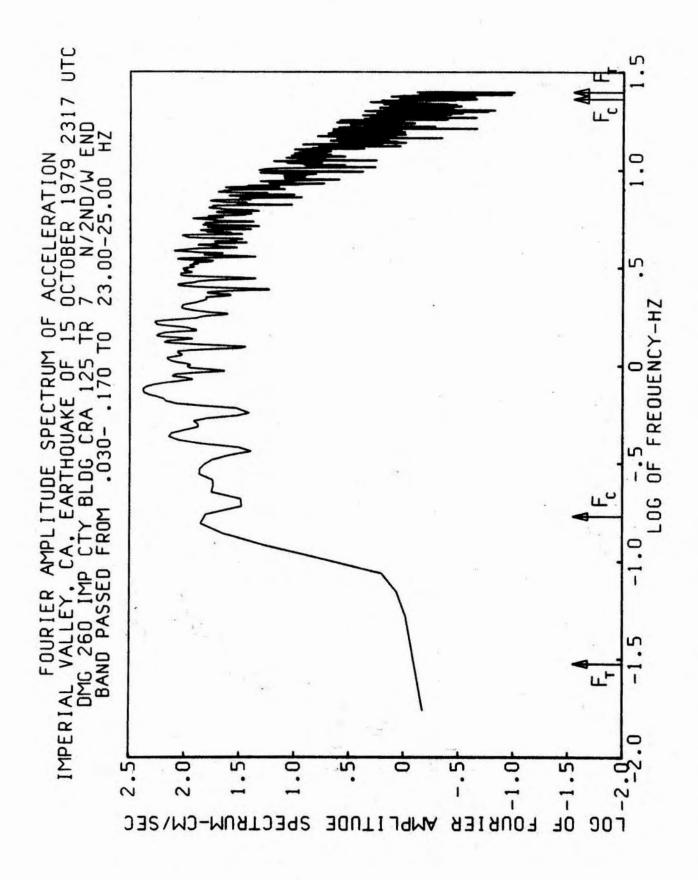
RESPONSE SPECTRA

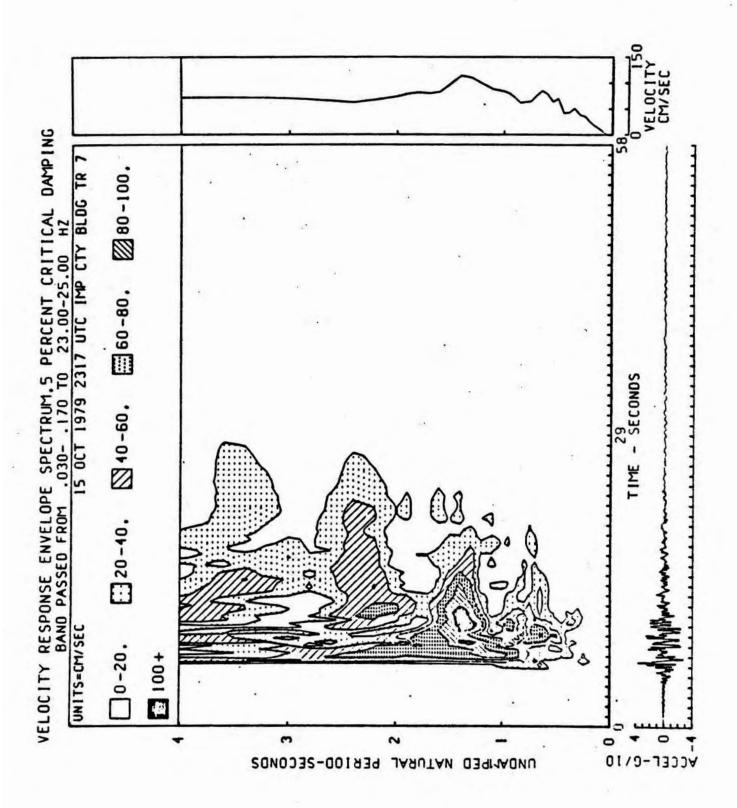
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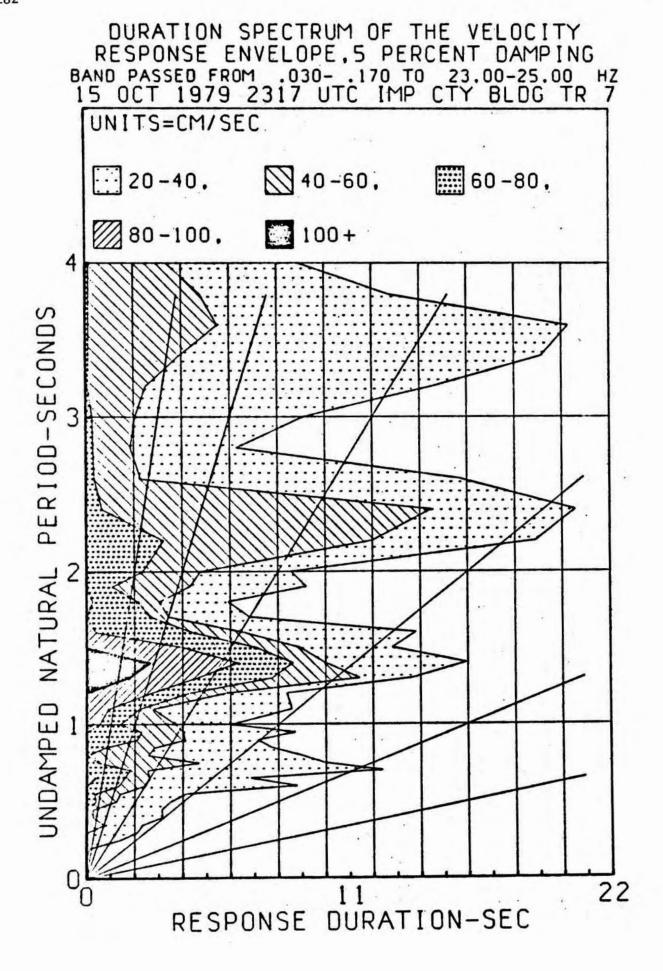
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



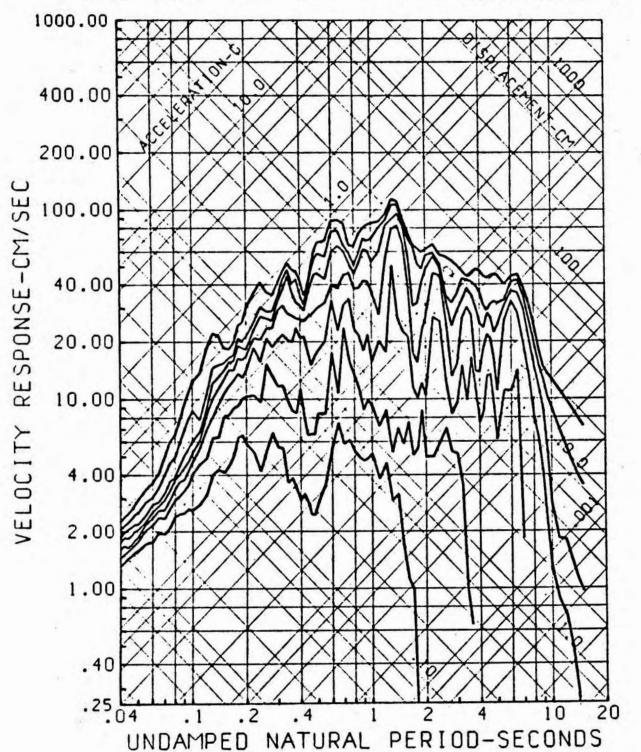


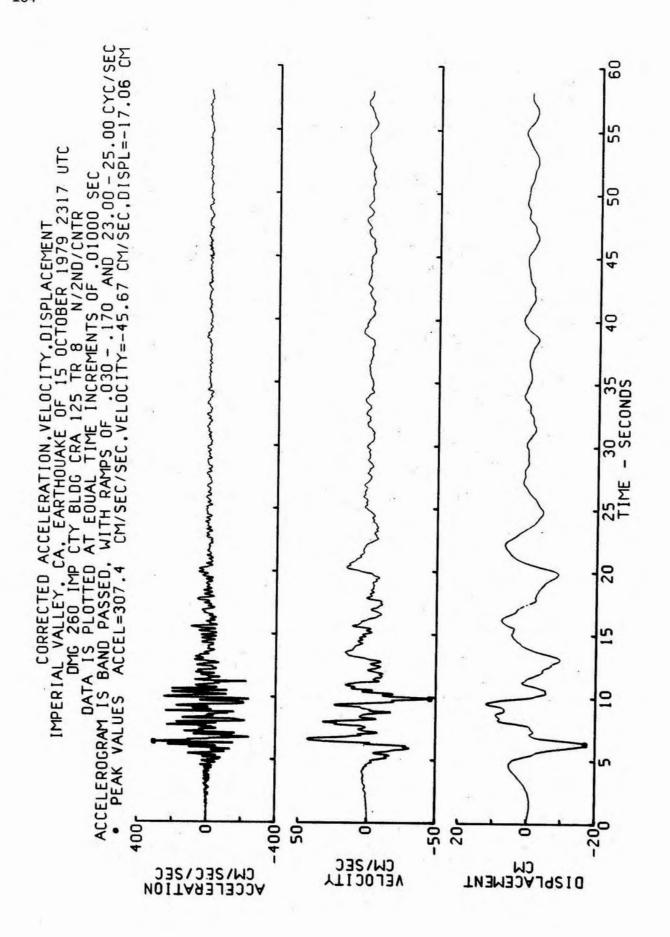






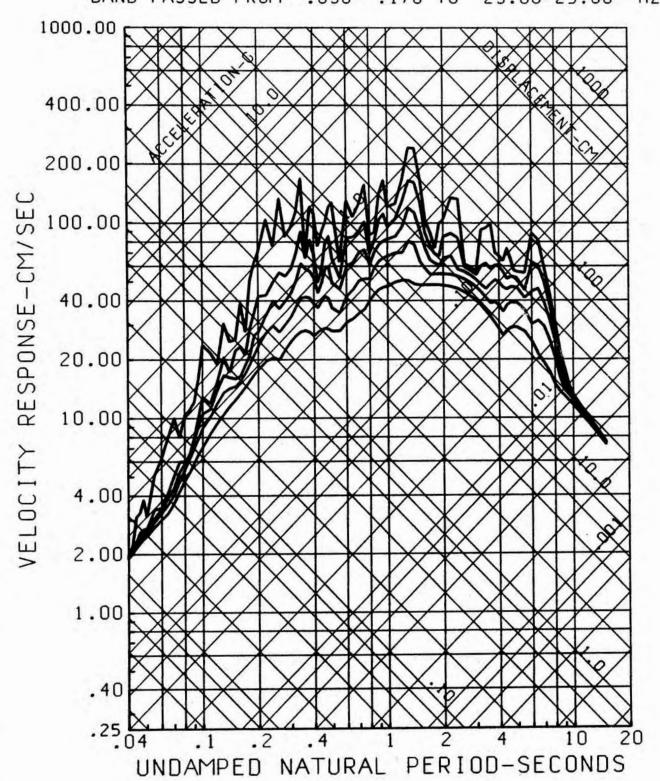
SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 7
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

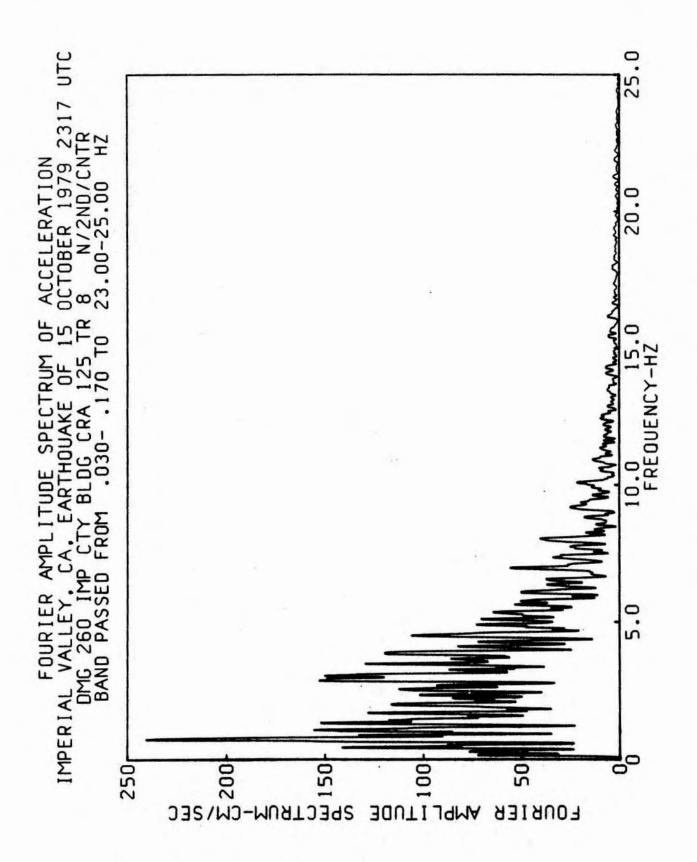


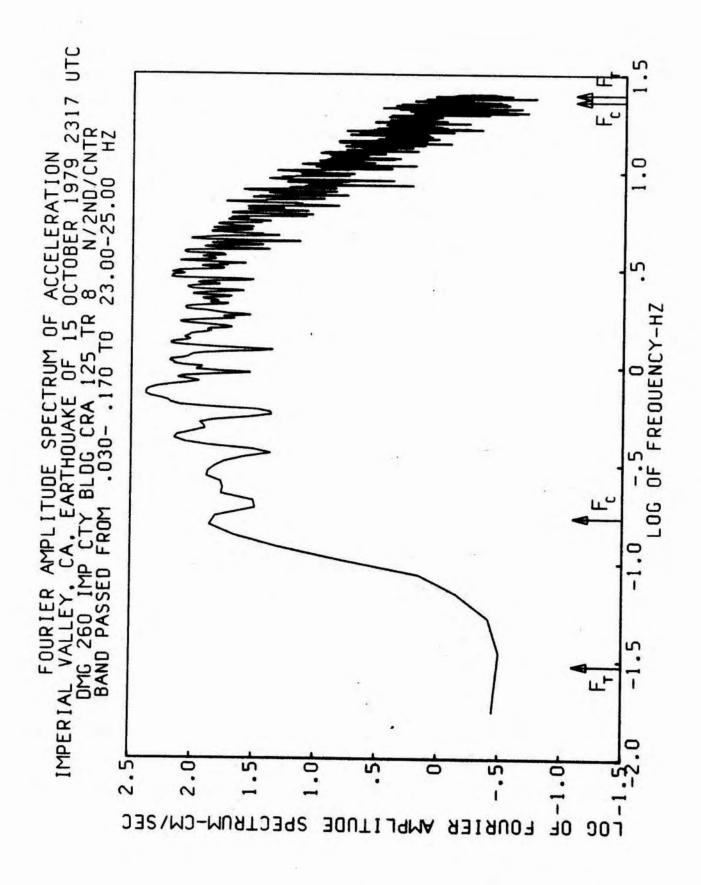


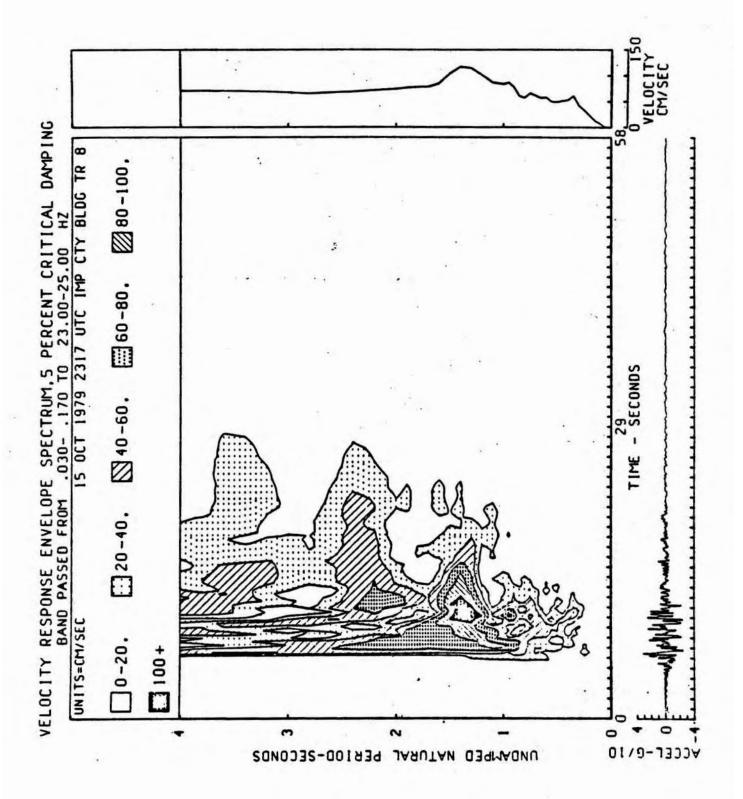
RESPONSE SPECTRA

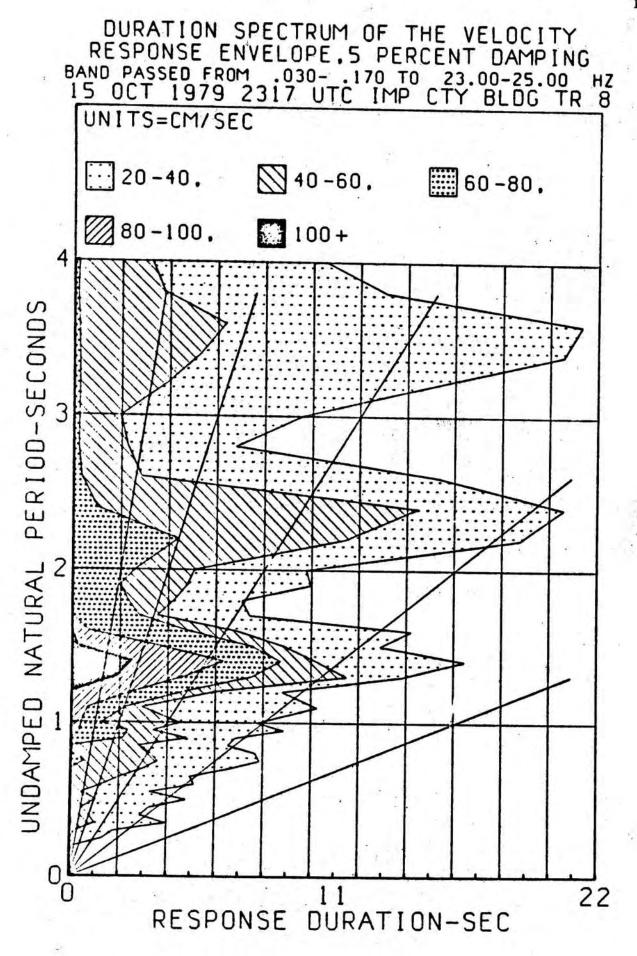
15 OCT 1979 2317 UTC IMP CTY BLDG TR 8
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



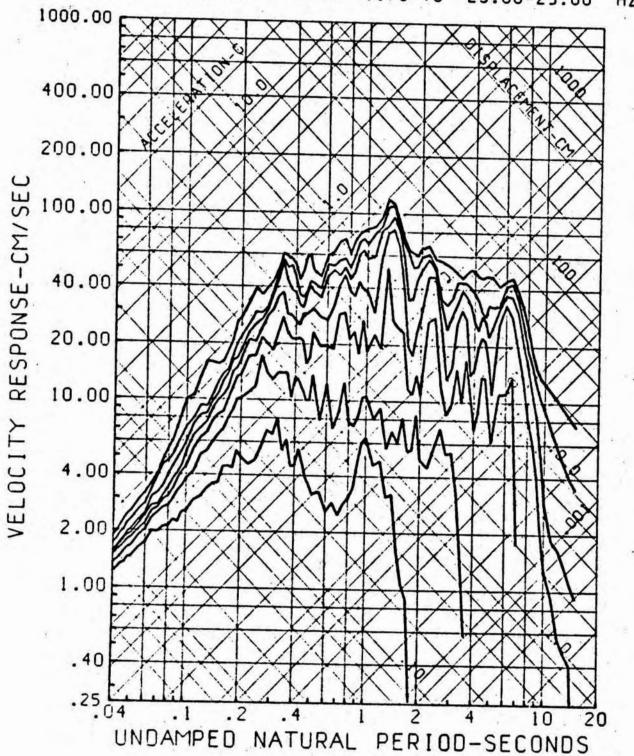


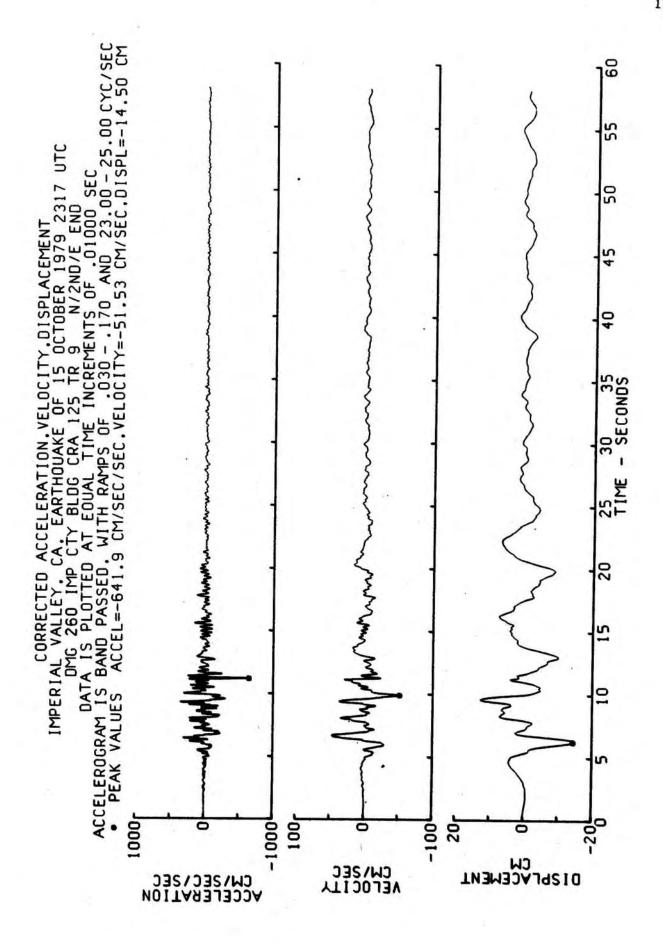






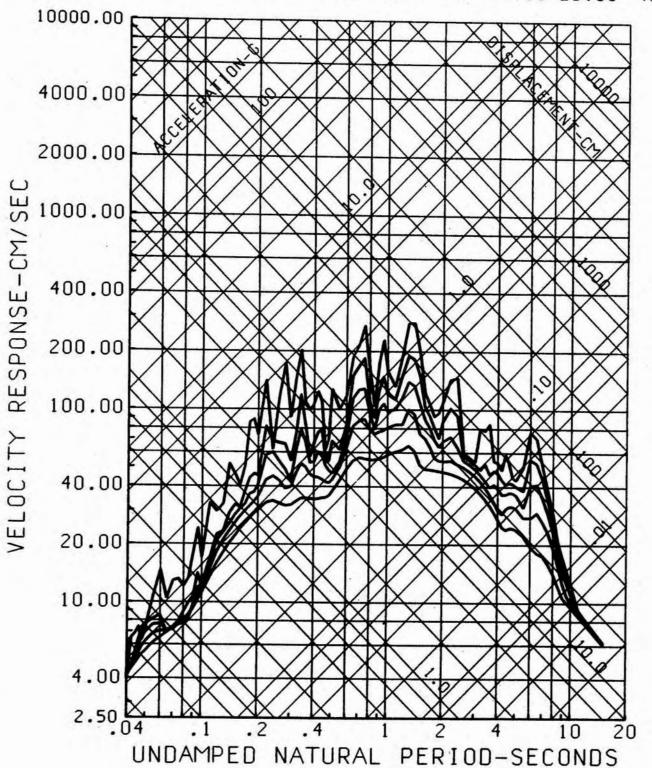
SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 8
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

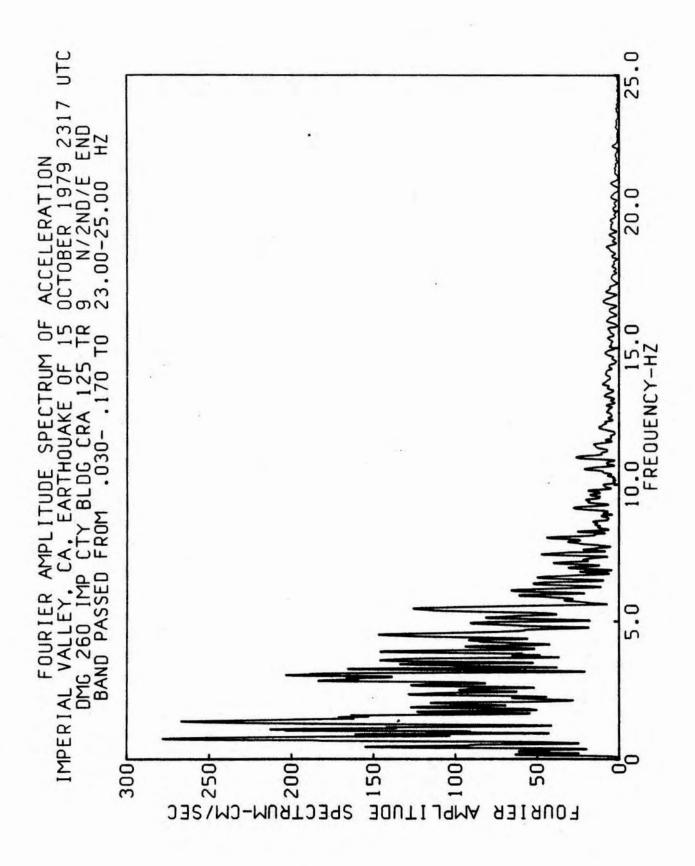


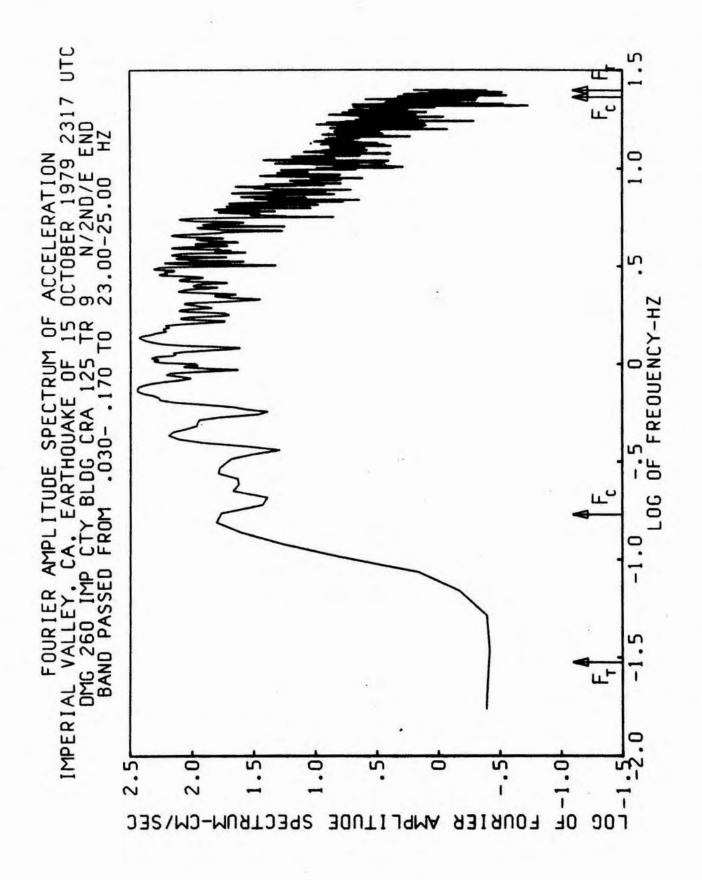


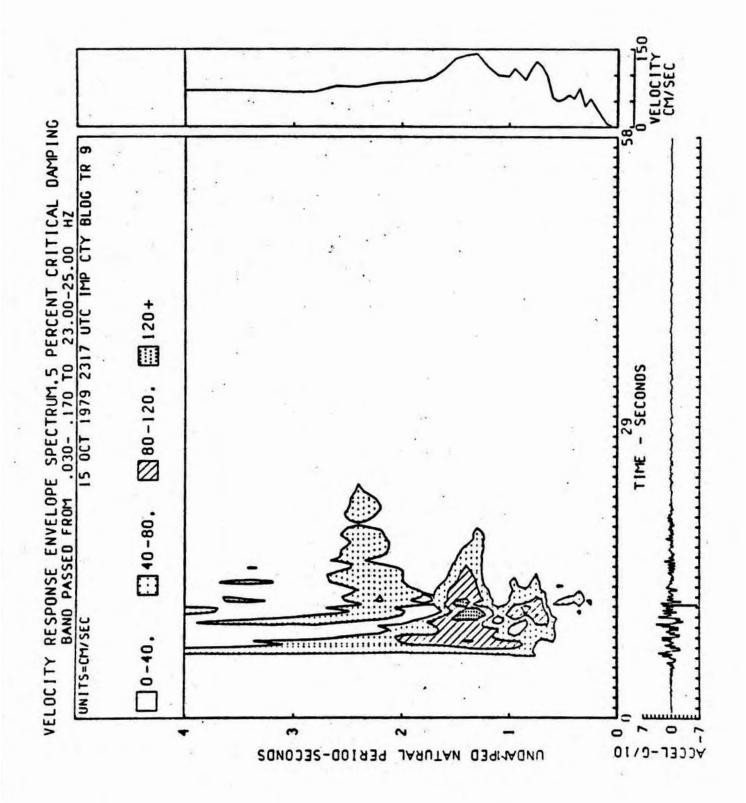
RESPONSE SPECTRA

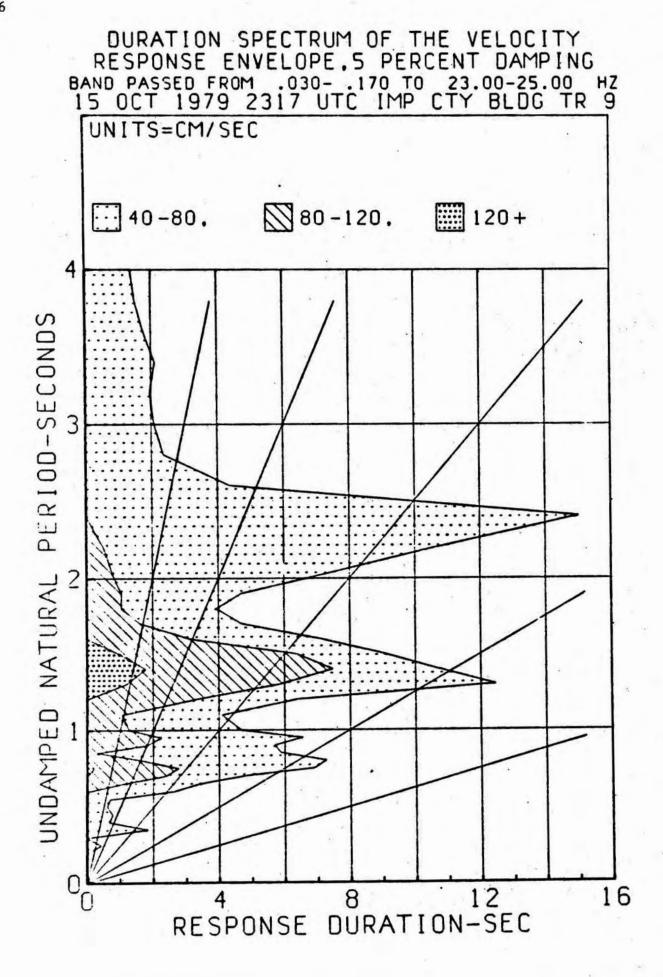
15 OCT 1979 2317 UTC IMP CTY BLDG TR 9
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



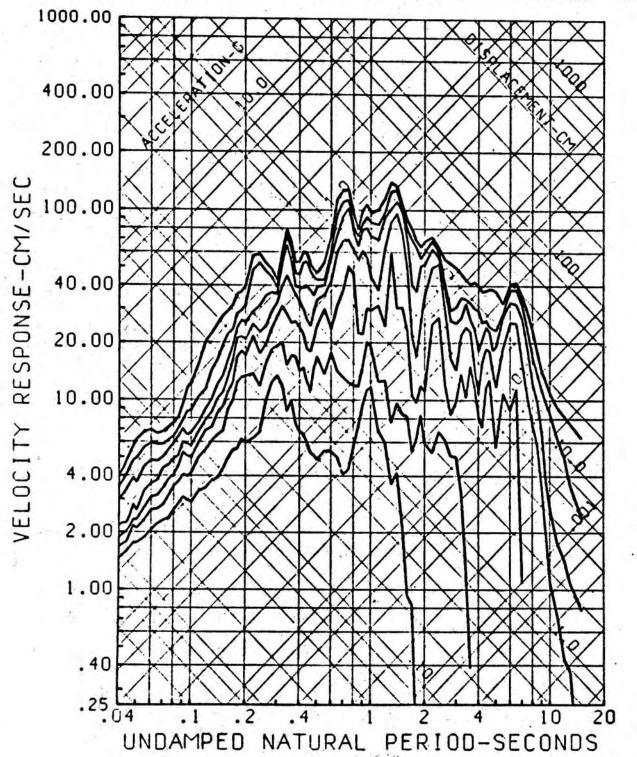


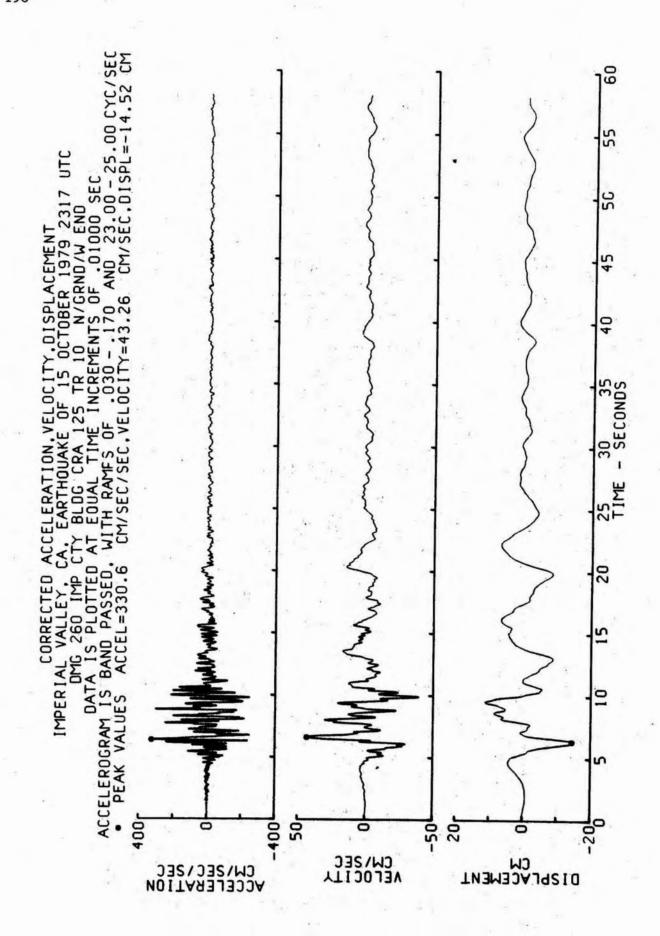






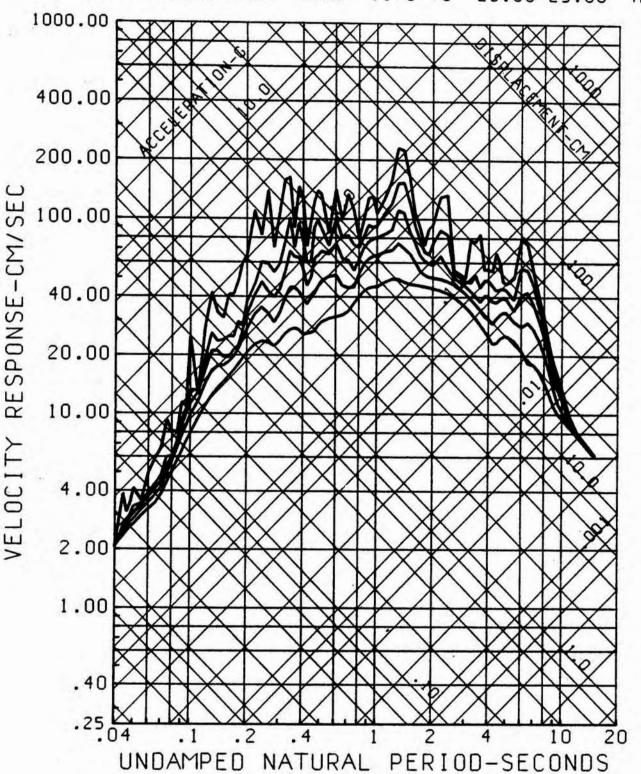
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC IMP CTY BLDG TR 9 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

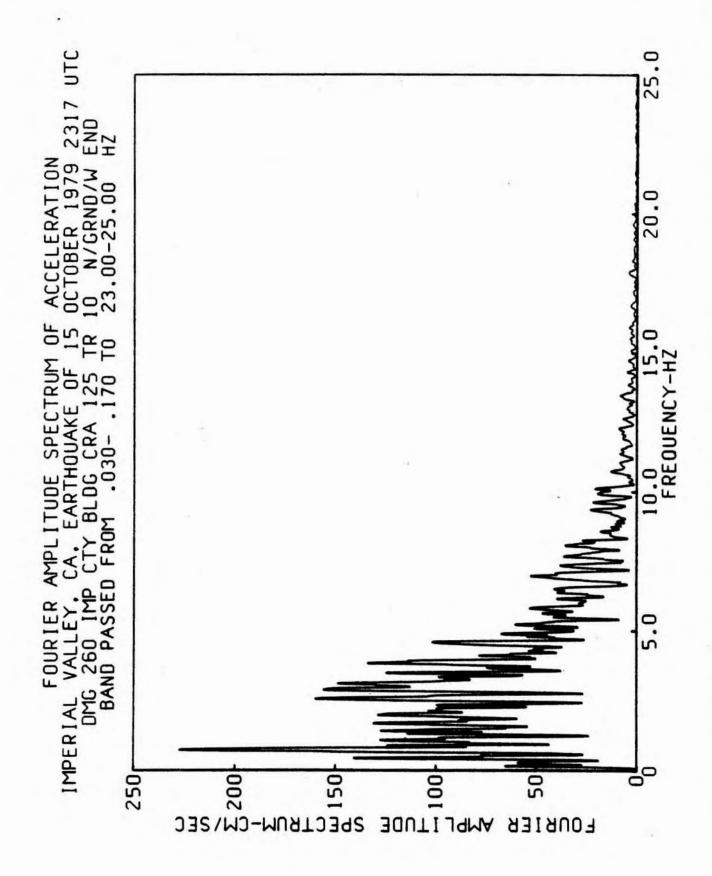


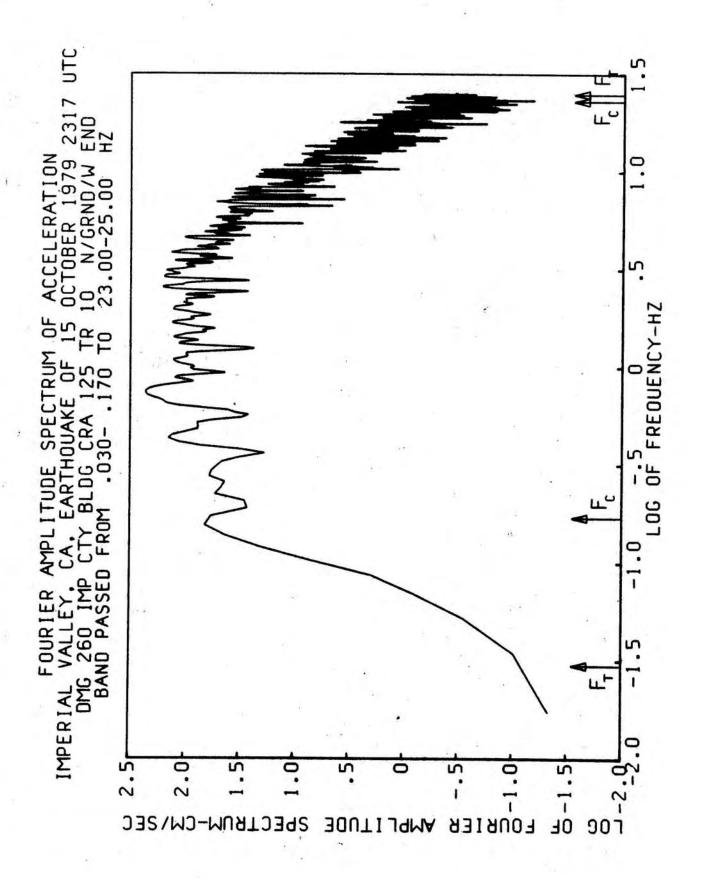


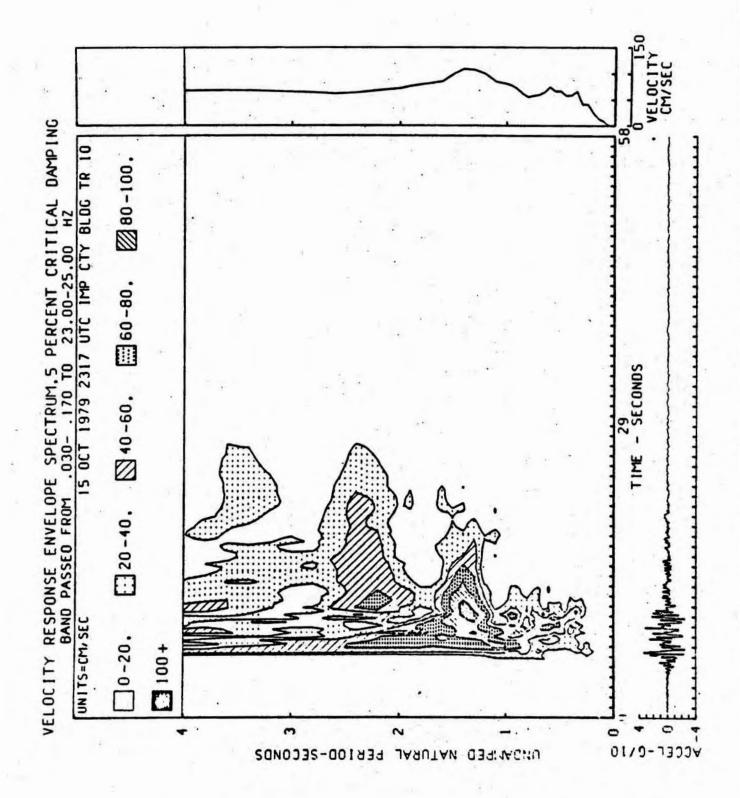
RESPONSE SPECTRA

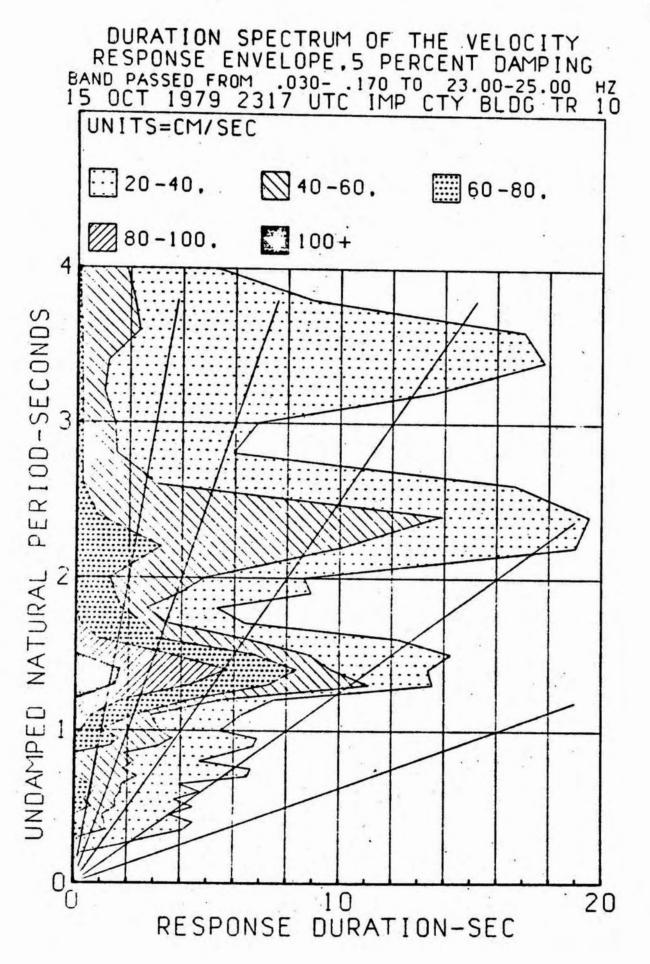
15 OCT 1979 2317 UTC IMP CTY BLDG TR 10
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



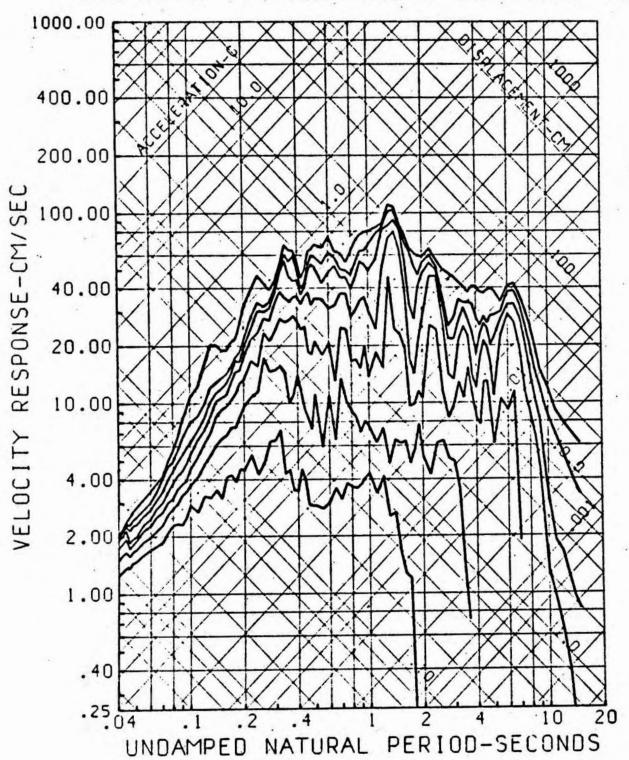


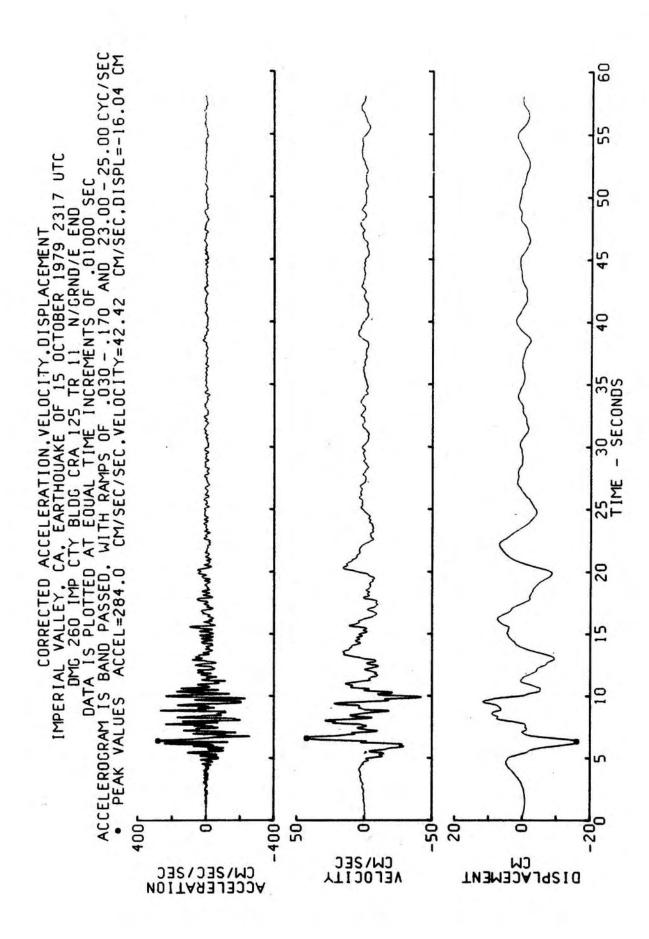






SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 10
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

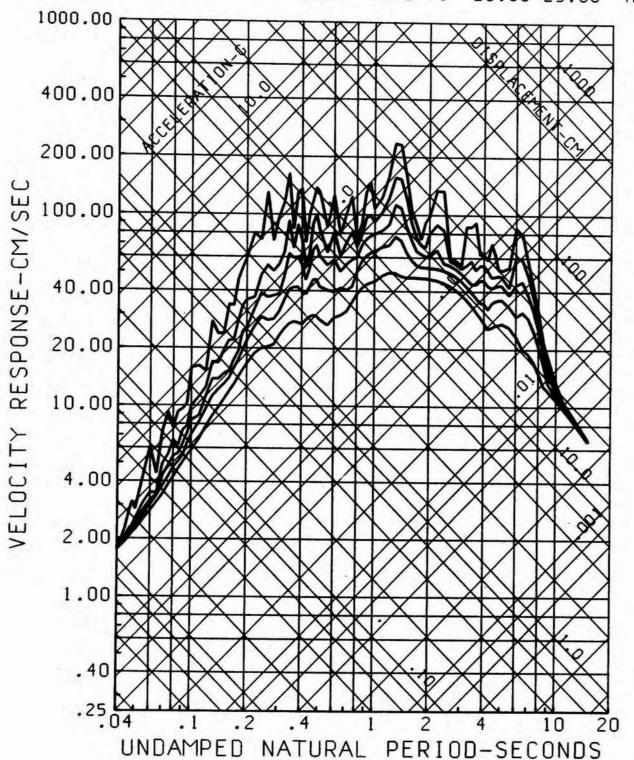


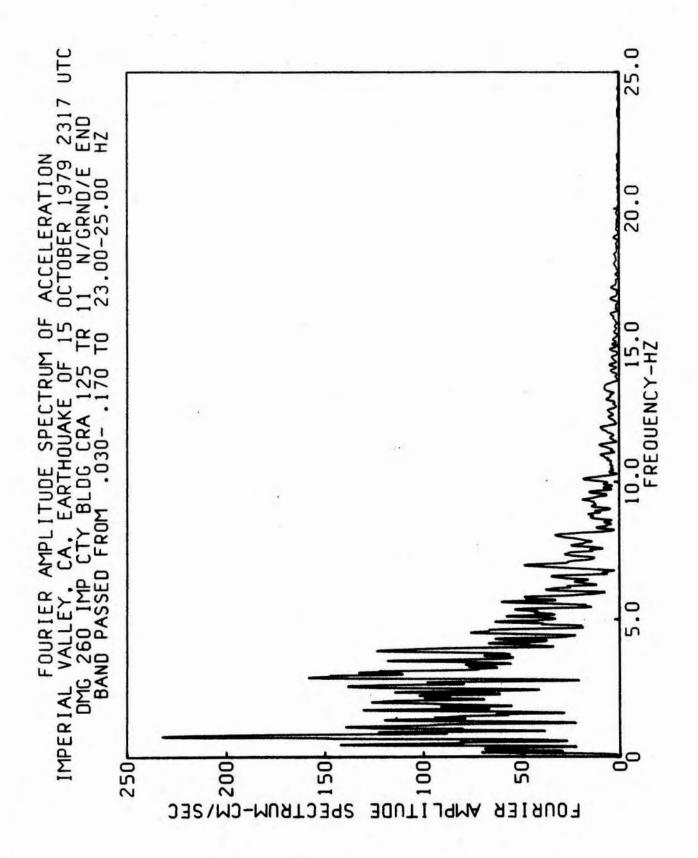


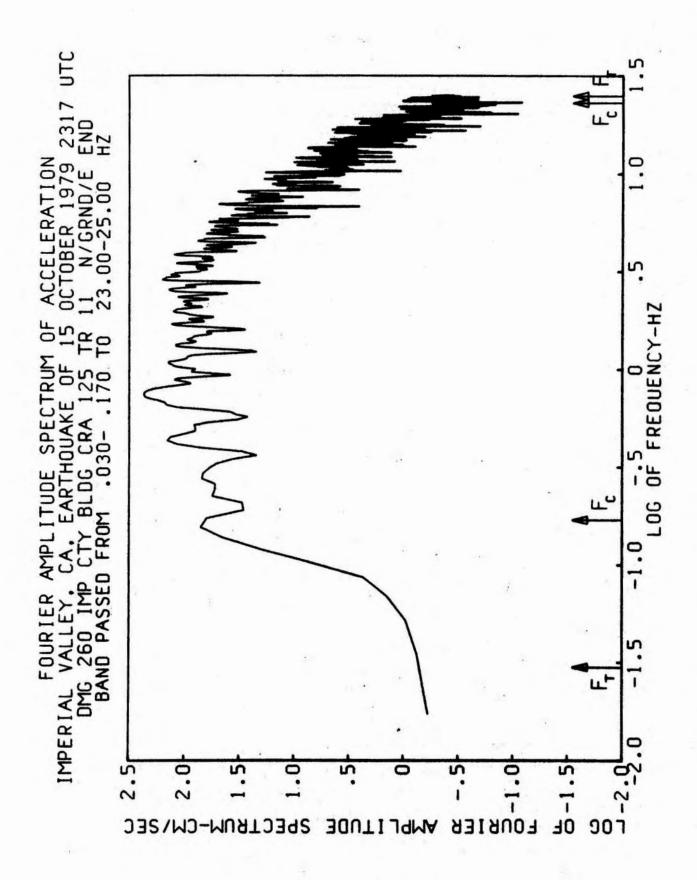
RESPONSE SPECTRA

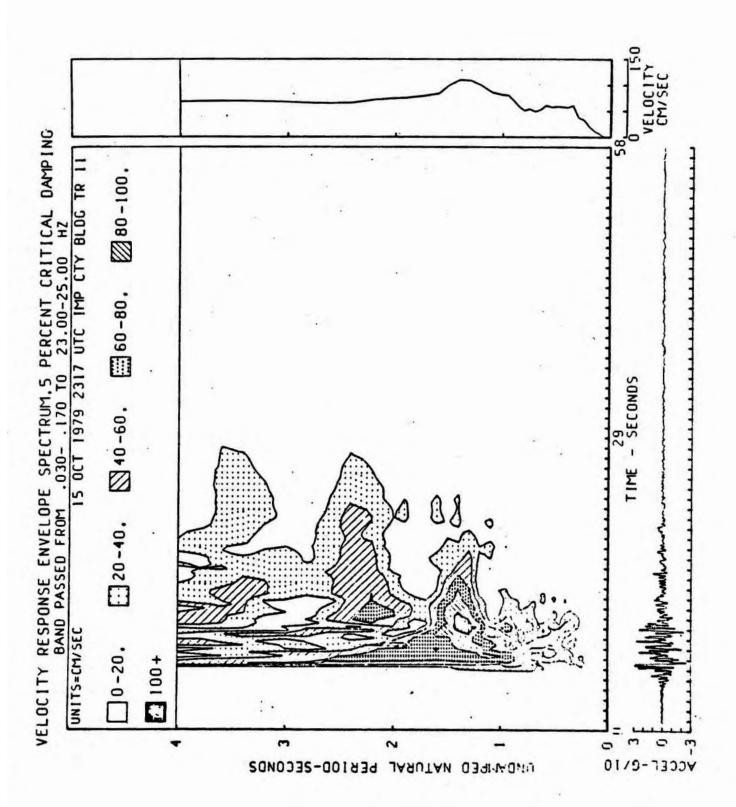
15 OCT 1979 2317 UTC IMP CTY BLDG TR 11

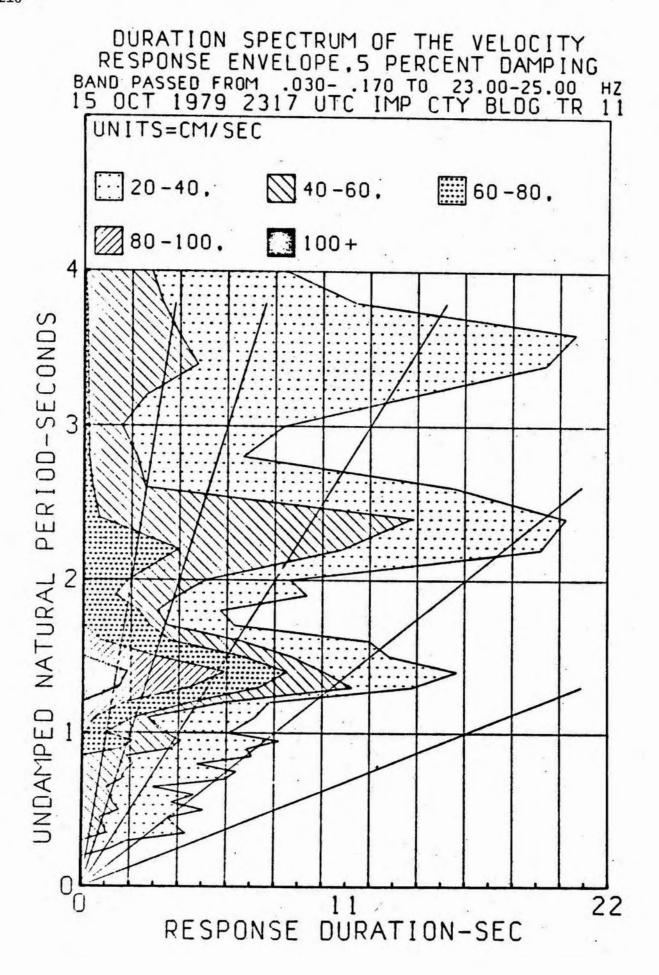
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



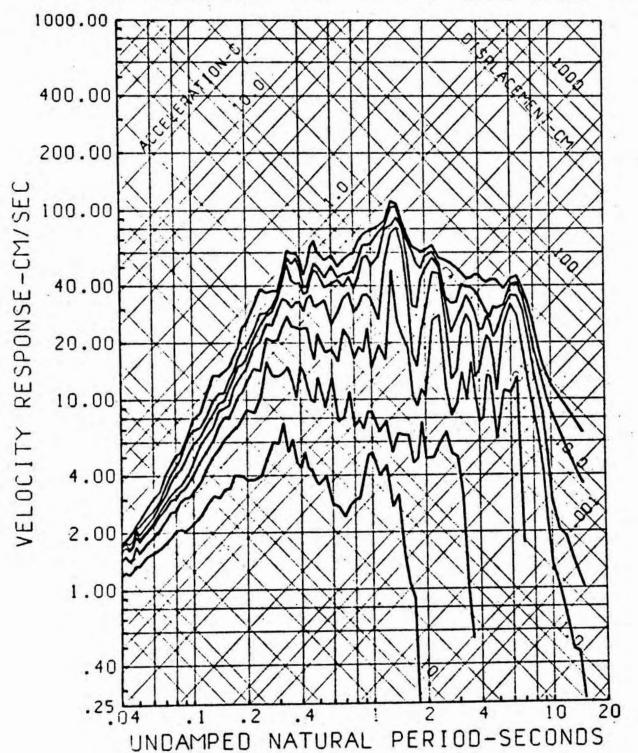


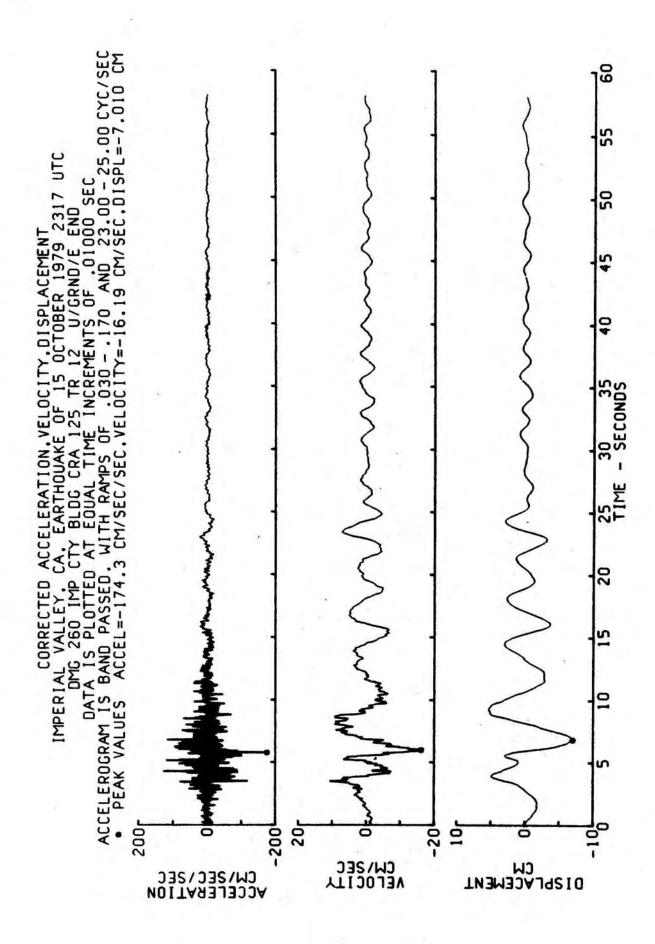






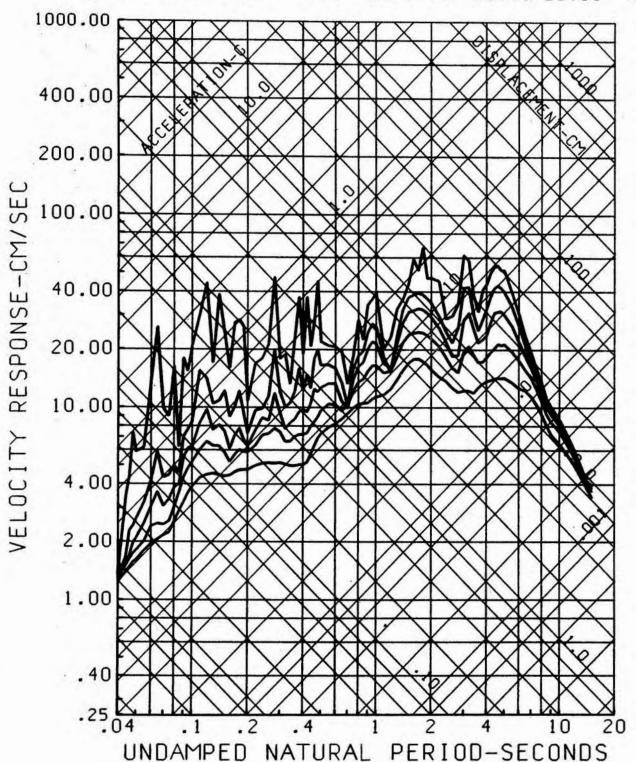
SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 11
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

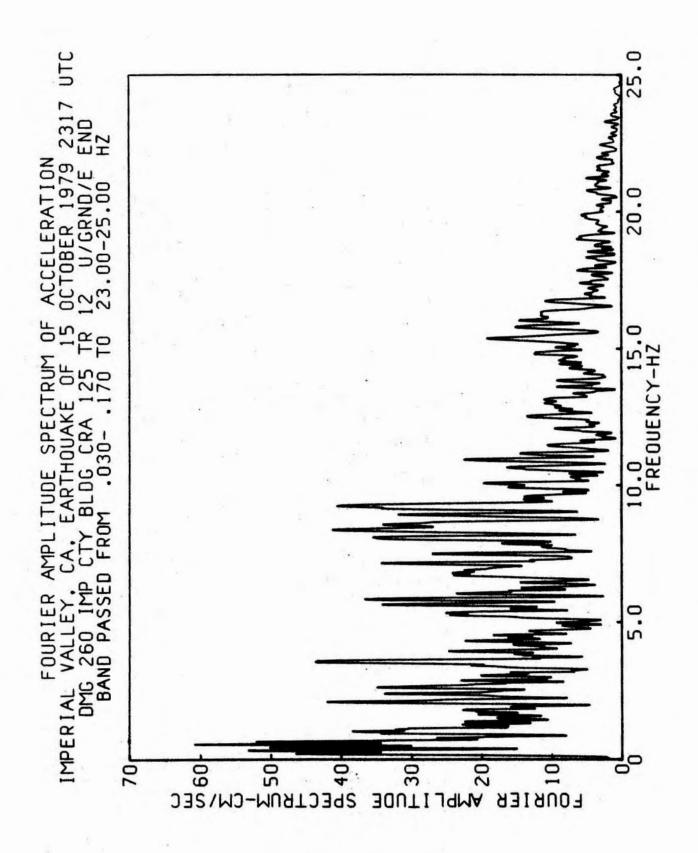


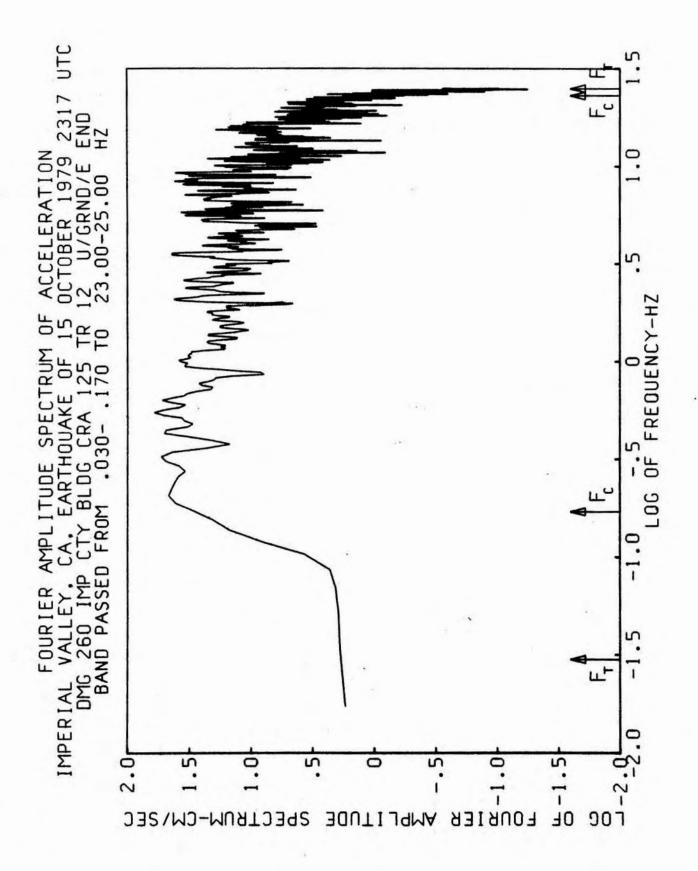


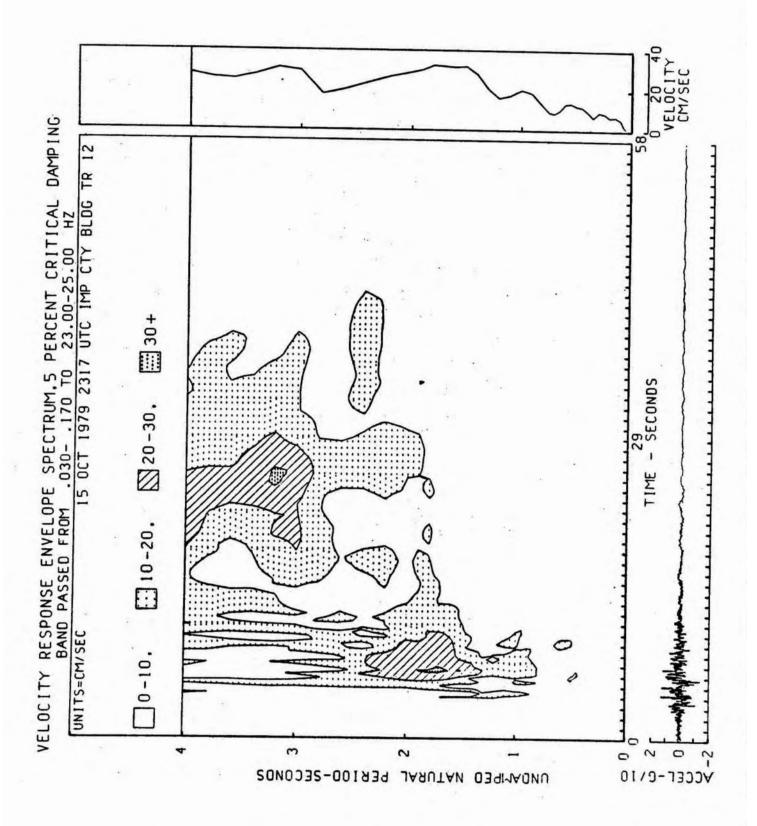
RESPONSE SPECTRA

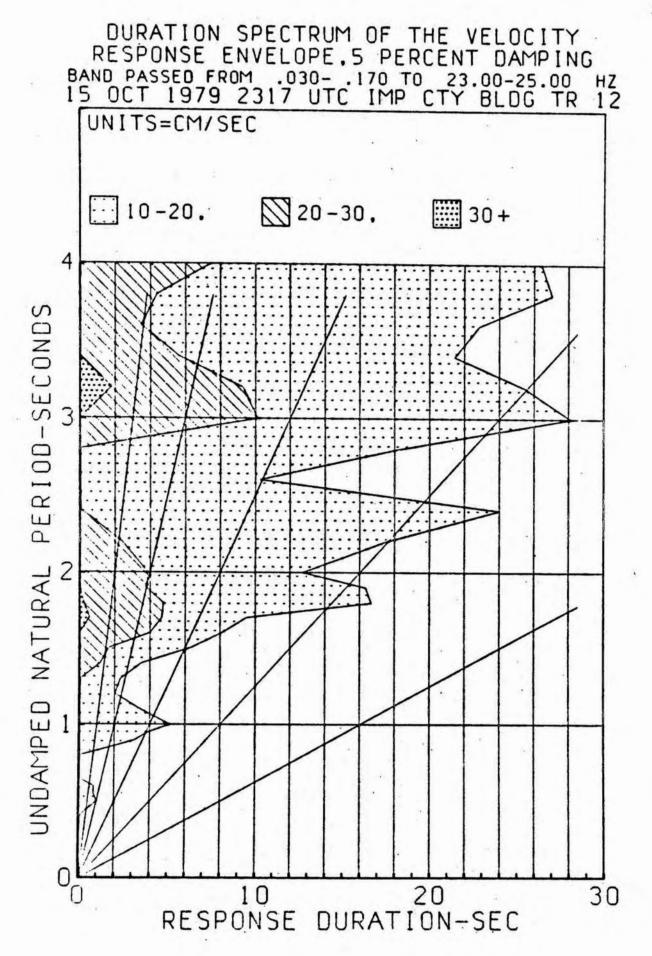
15 OCT 1979 2317 UTC IMP CTY BLDG TR 12
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



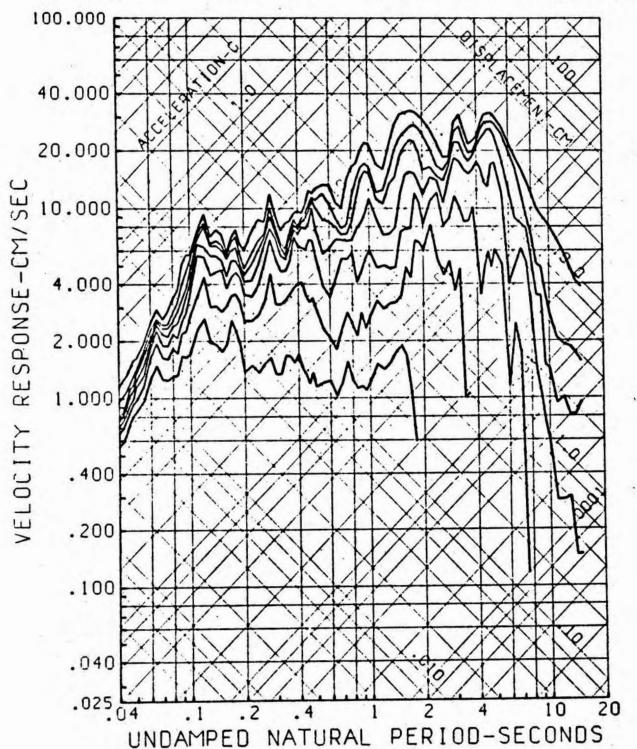


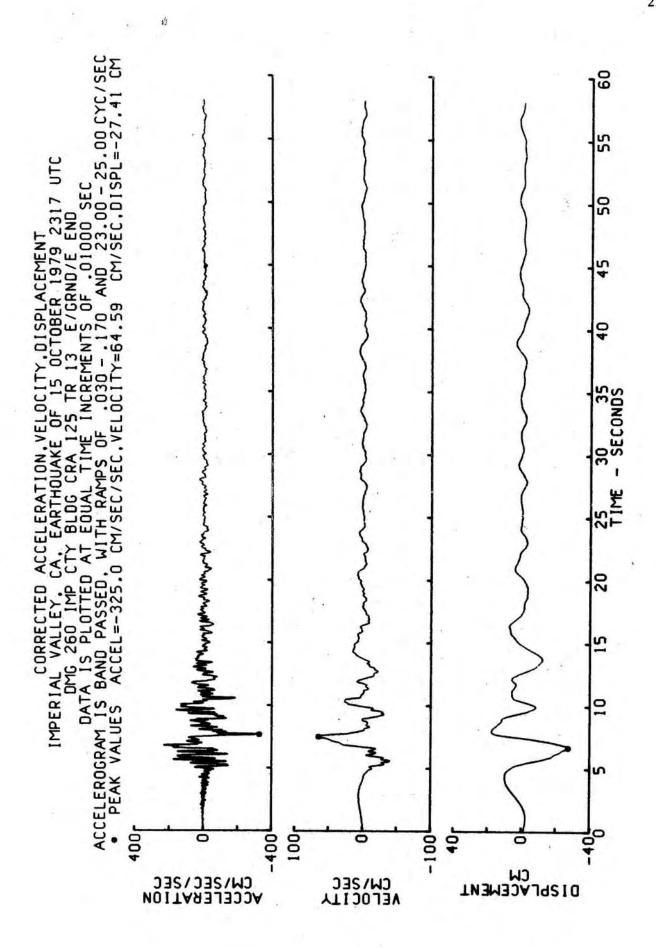






SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 12
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

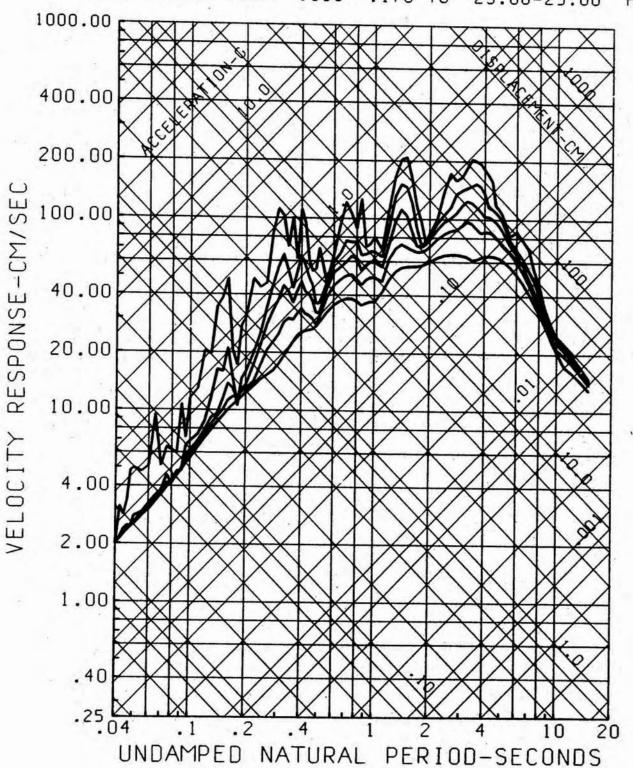


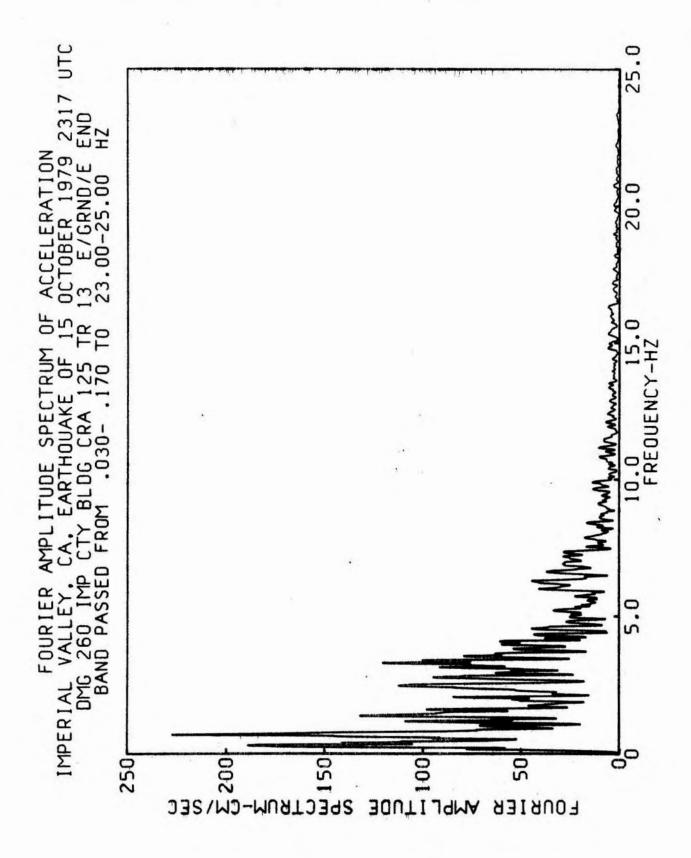


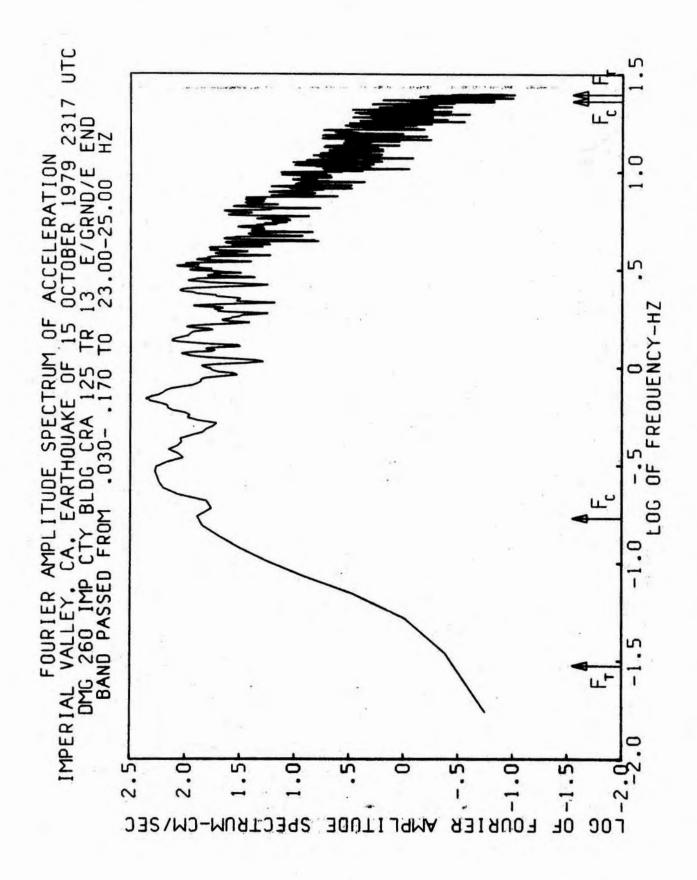
RESPONSE SPECTRA

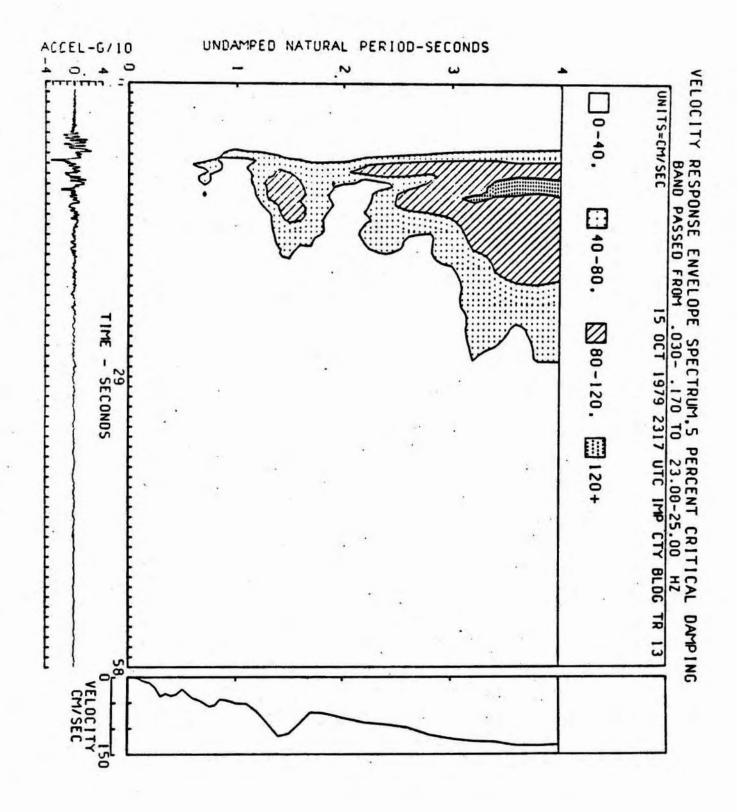
15 OCT 1979 2317 UTC IMP CTY BLDG TR 13

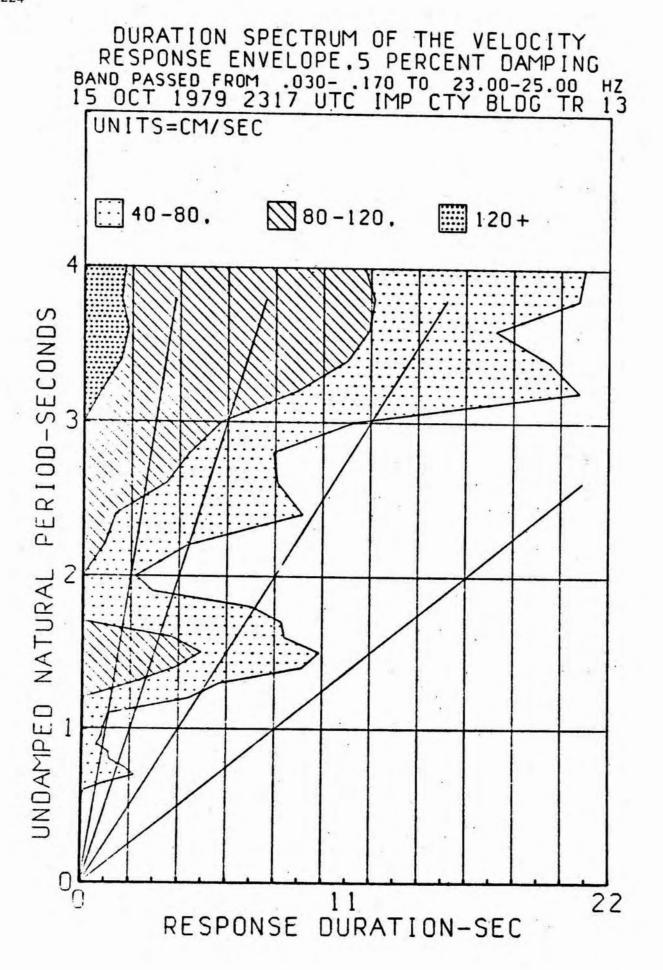
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



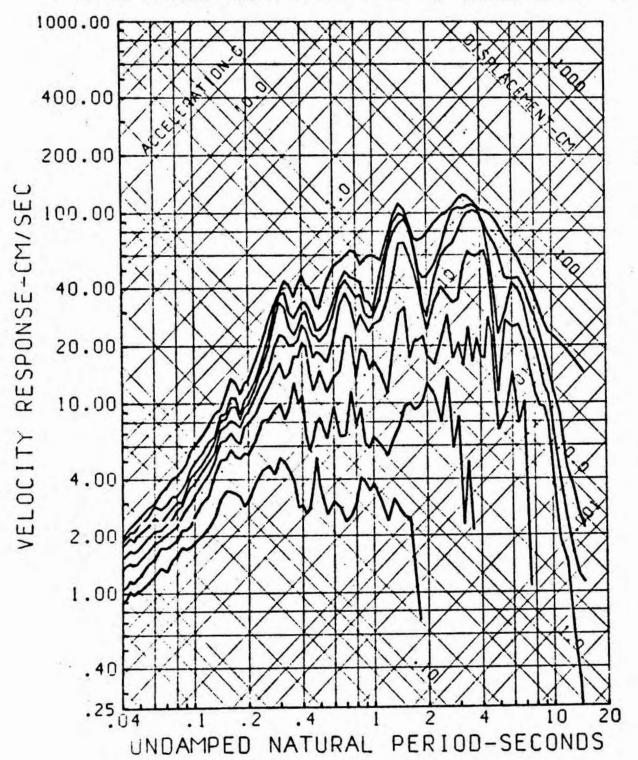


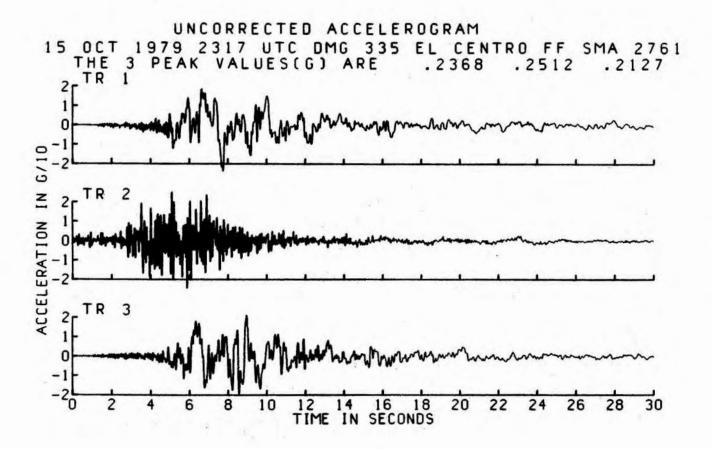


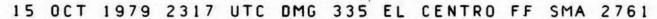


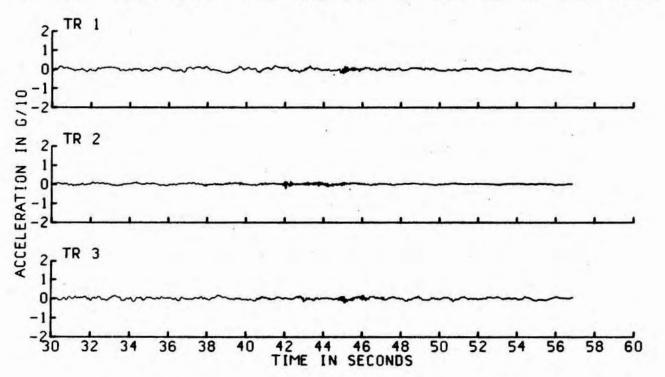


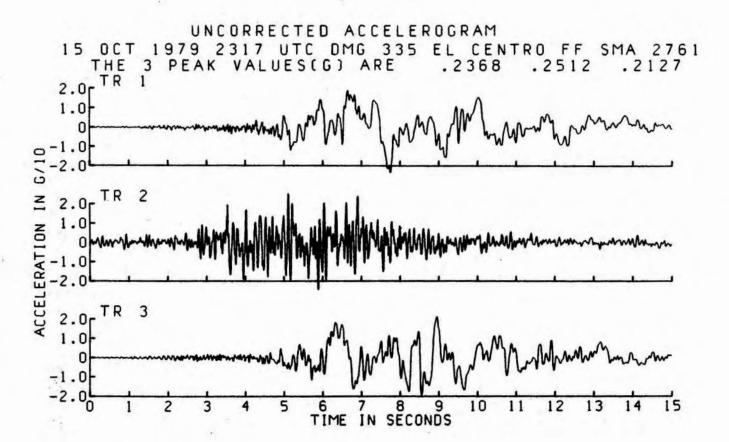
SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC IMP CTY BLDG TR 13
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

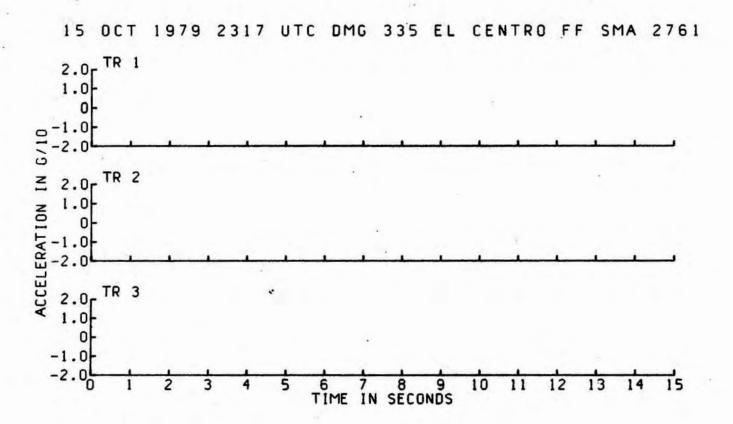


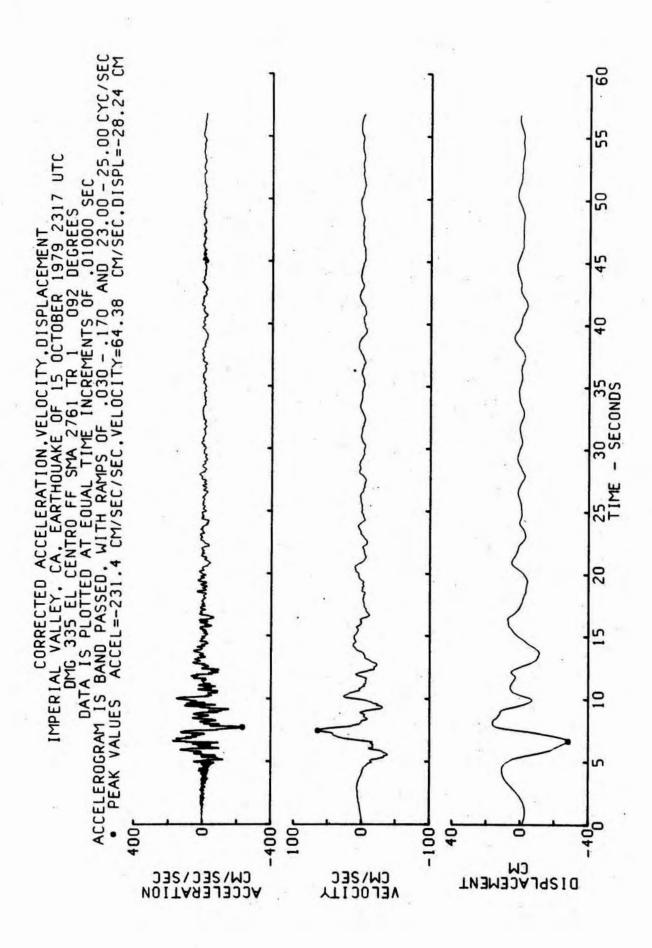






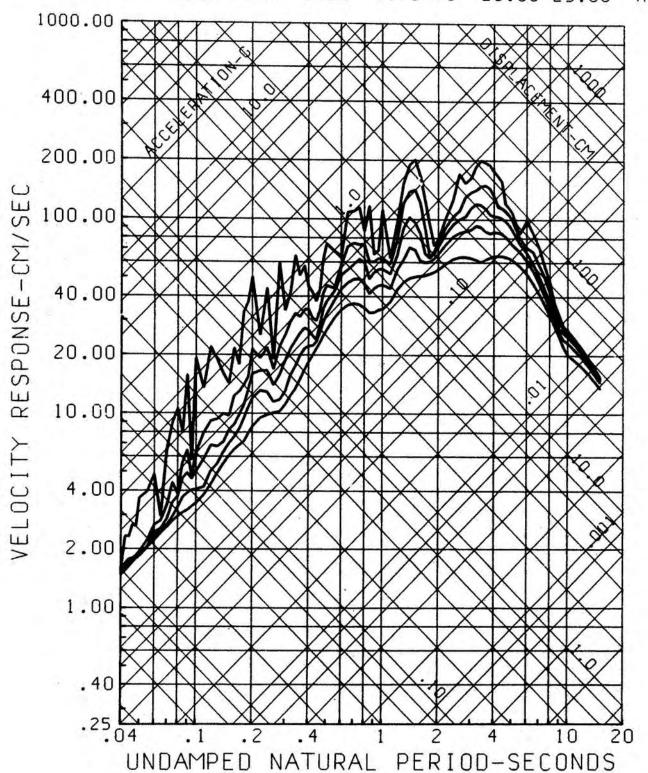


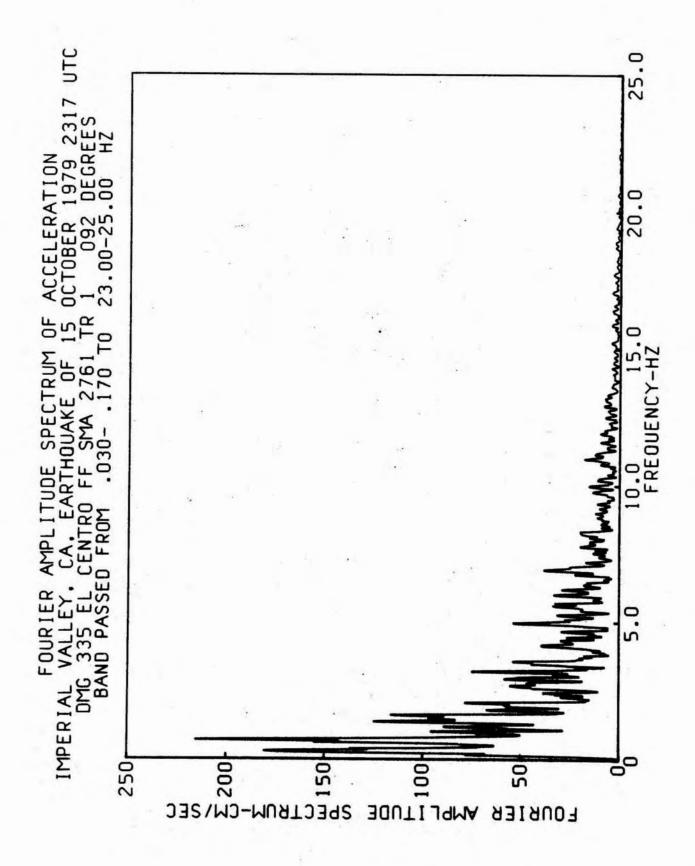


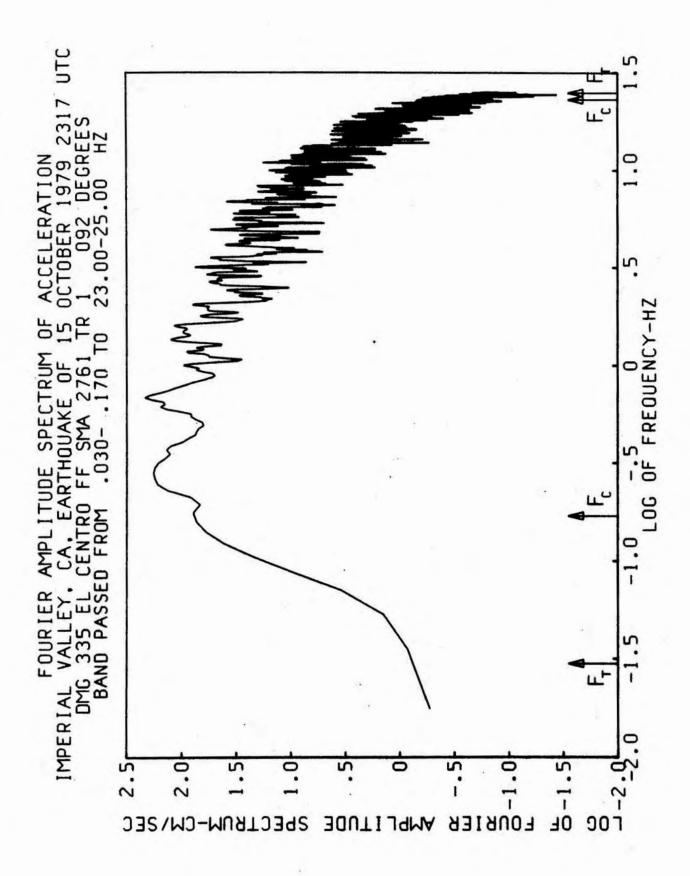


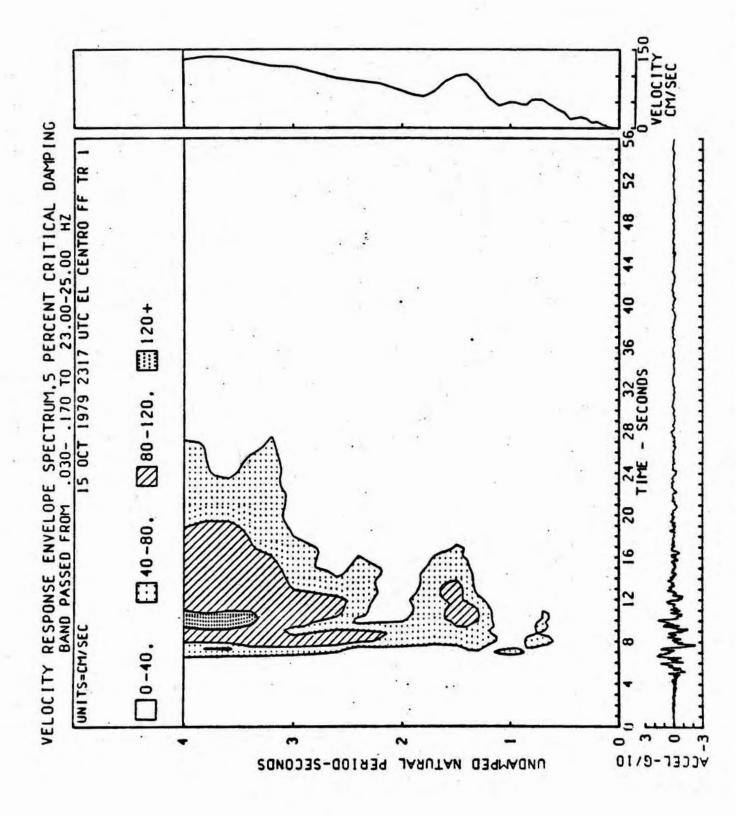
## RESPONSE SPECTRA

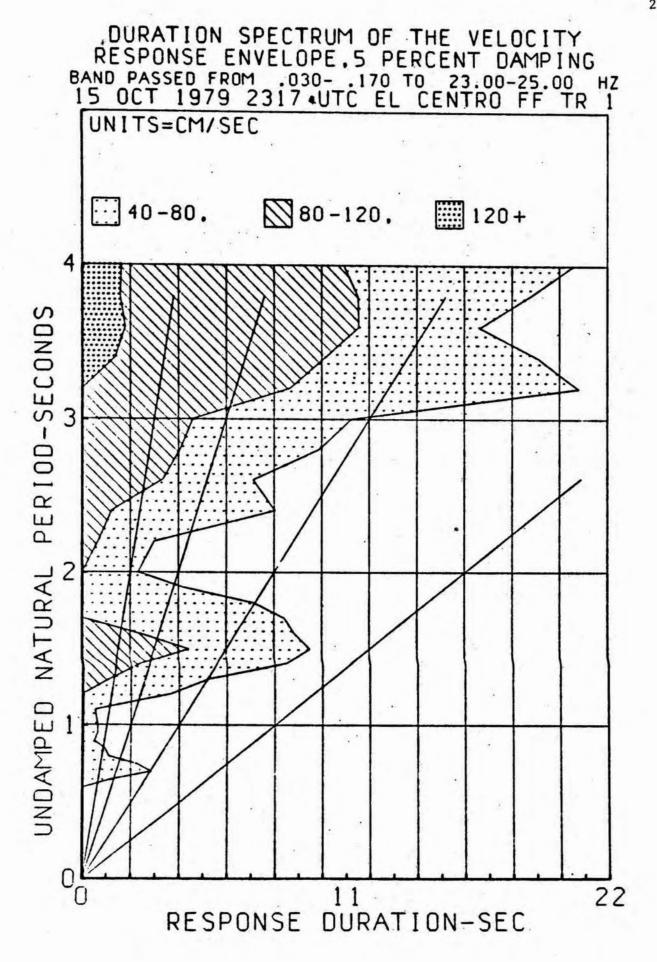
15 OCT 1979 2317 UTC EL CENTRO FF TR 1 0,2,5,10,20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



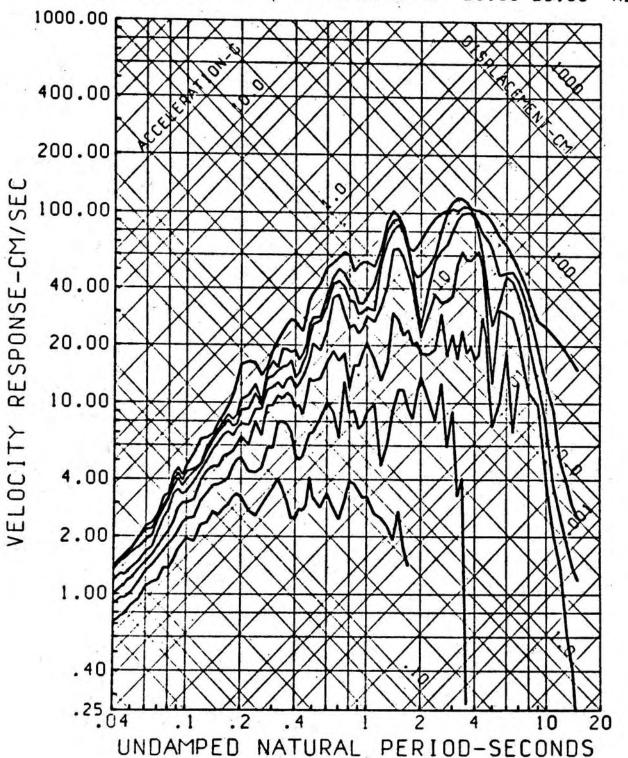


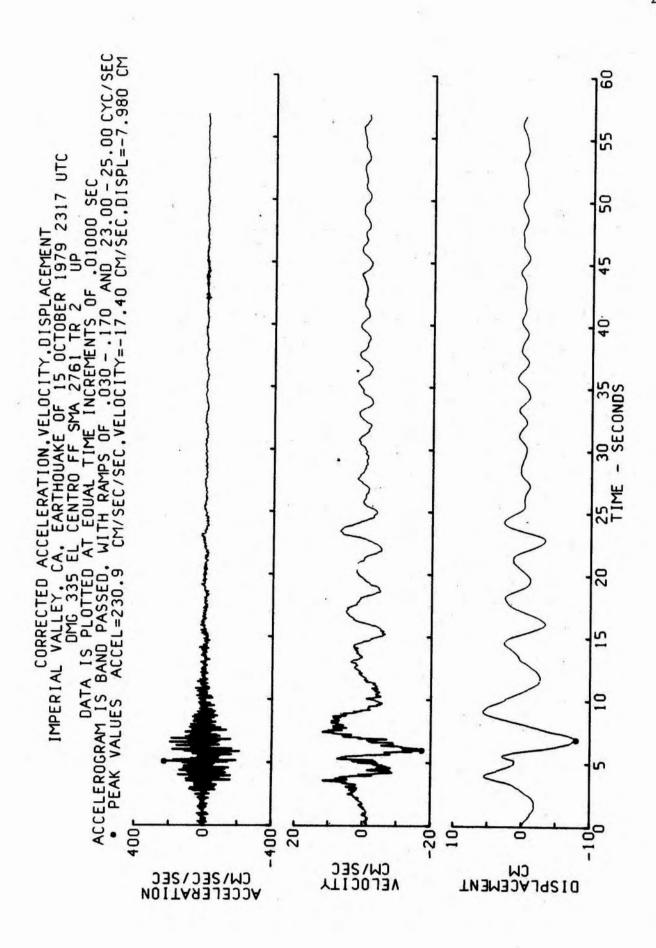






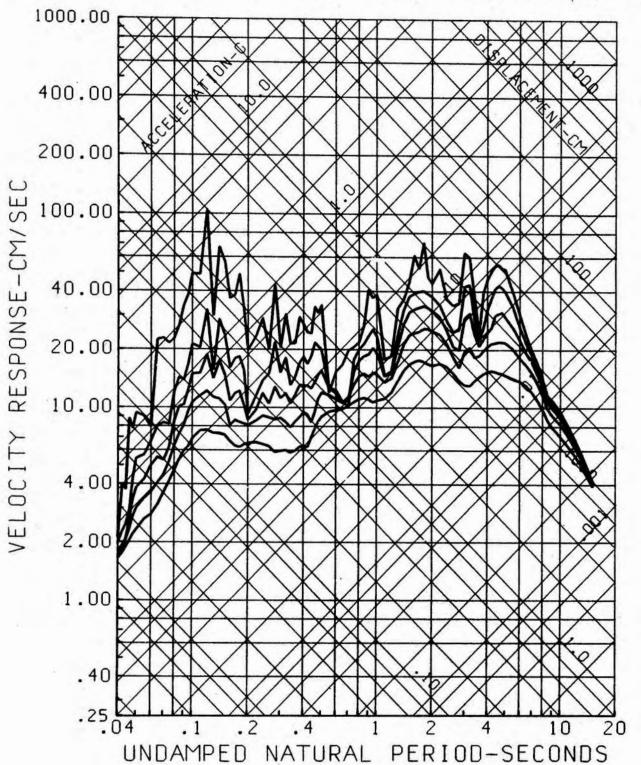
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC EL CENTRO FF TR 1 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

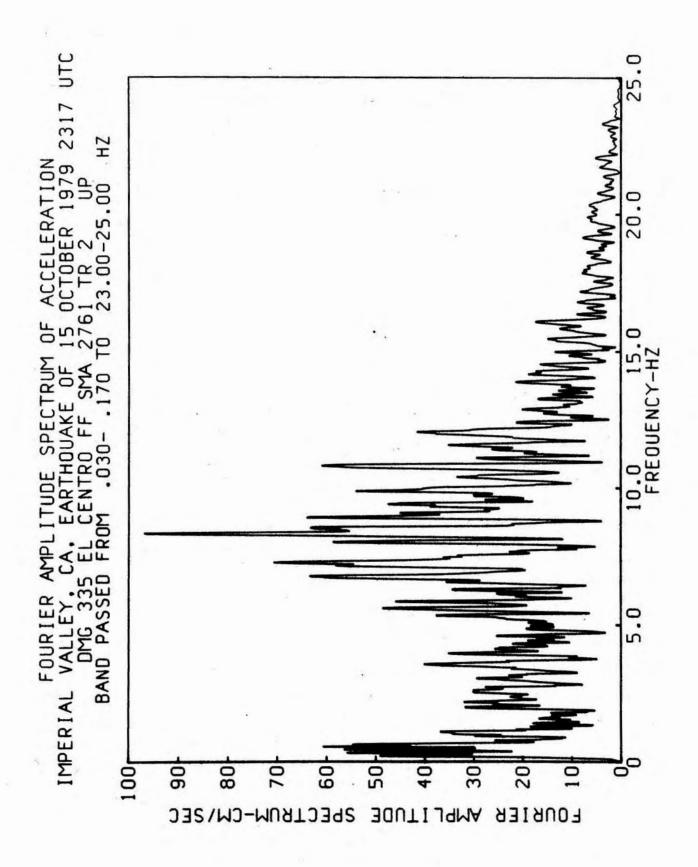


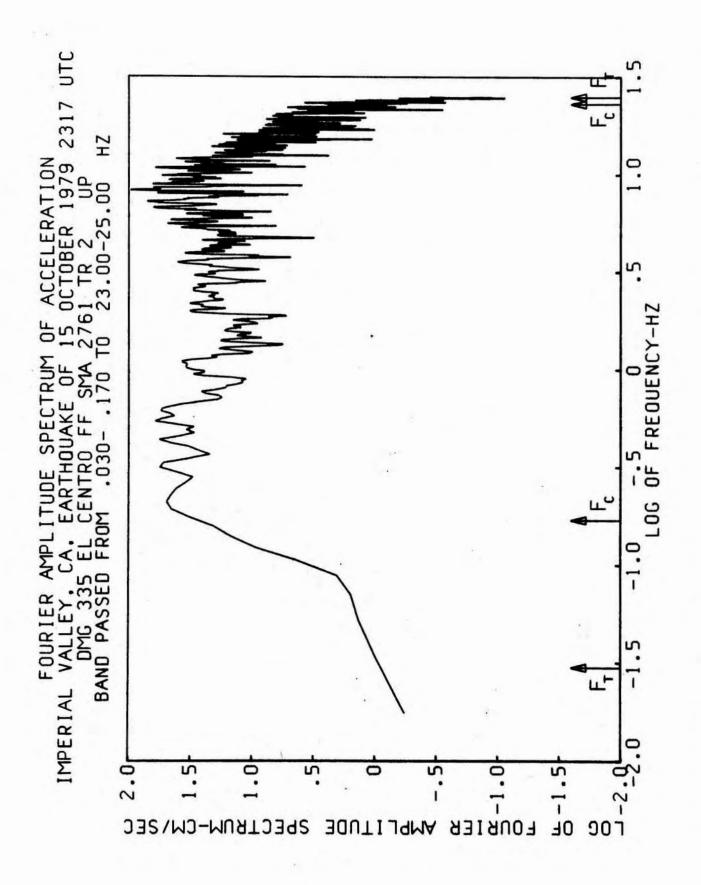


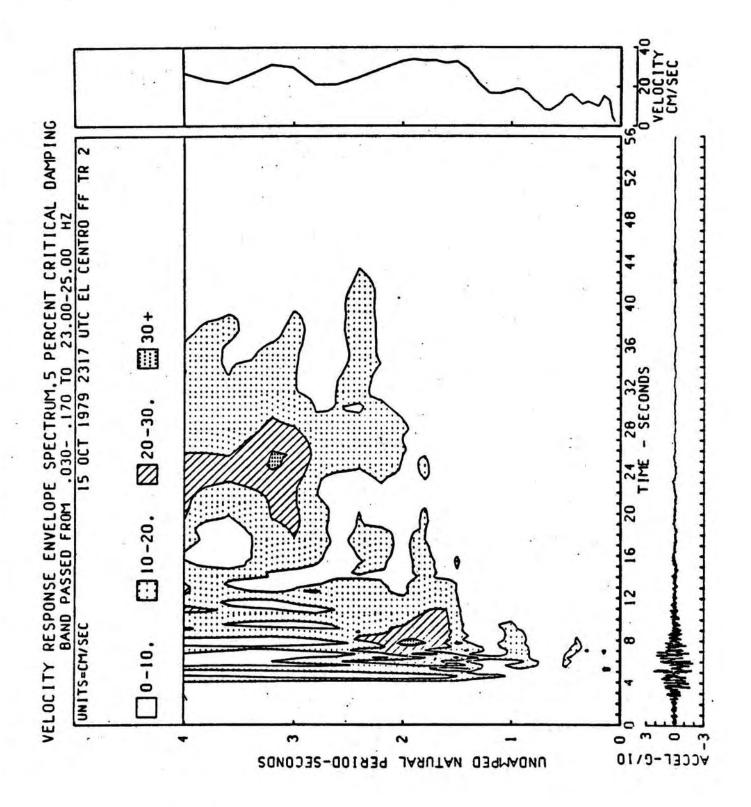
RESPONSE SPECTRA

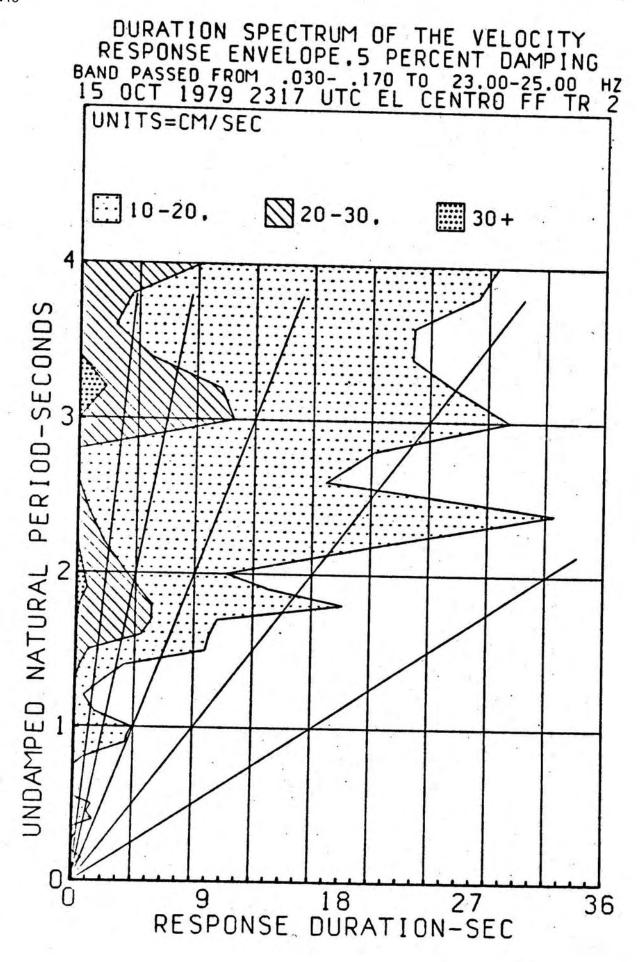
15 OCT 1979 2317 UTC EL CENTRO FF TR 2
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



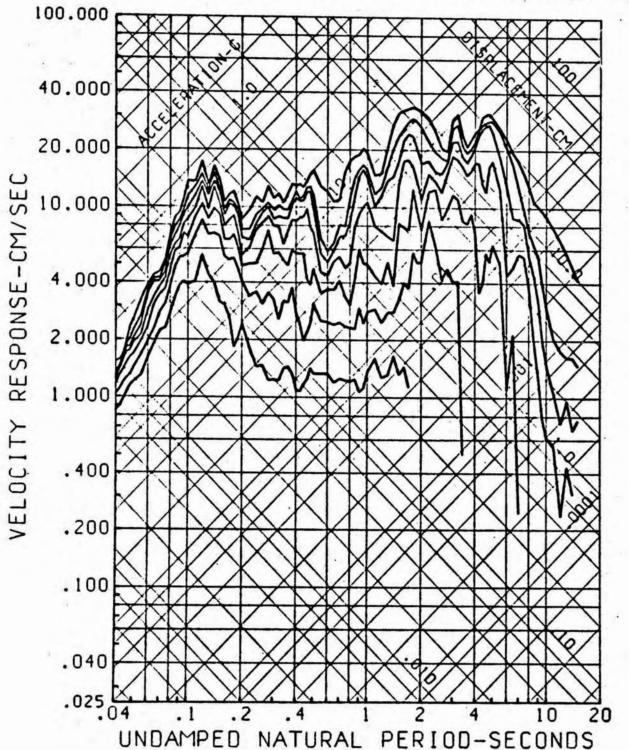


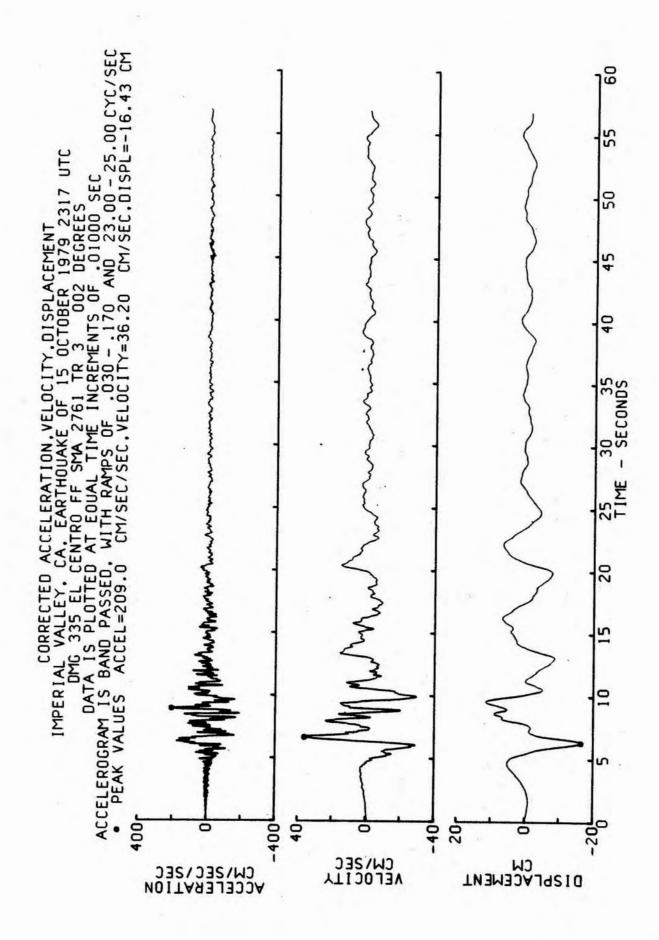






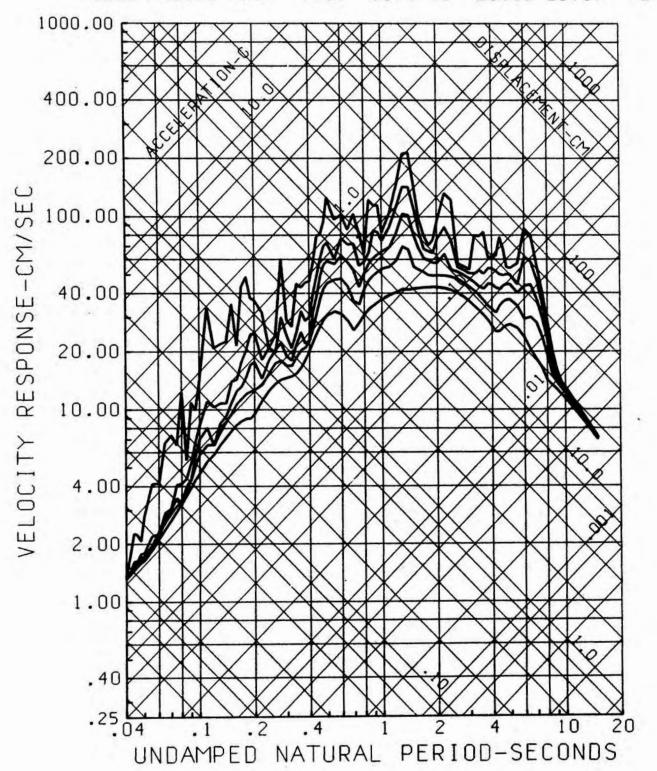
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC EL CENTRO FF TR 2 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

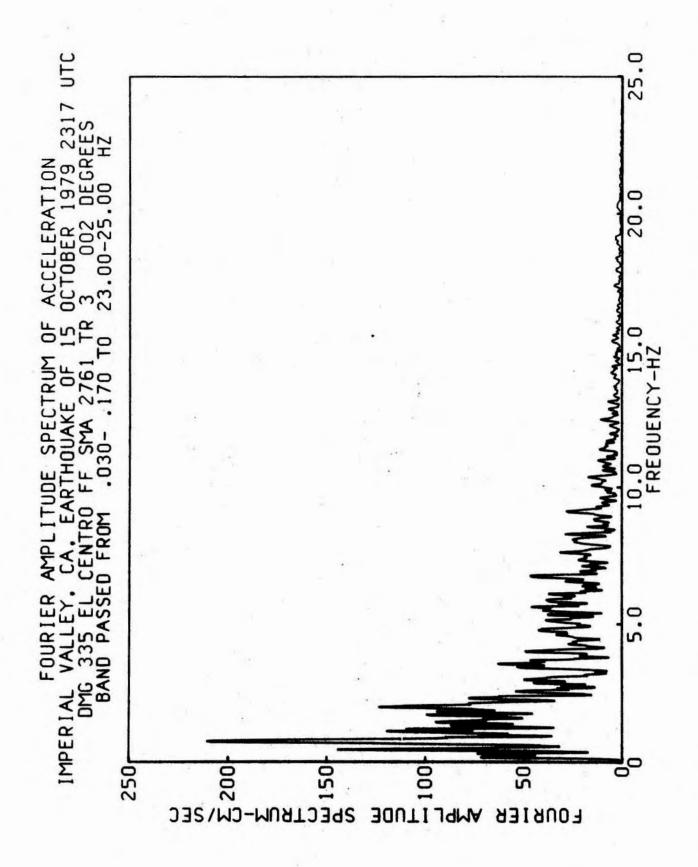


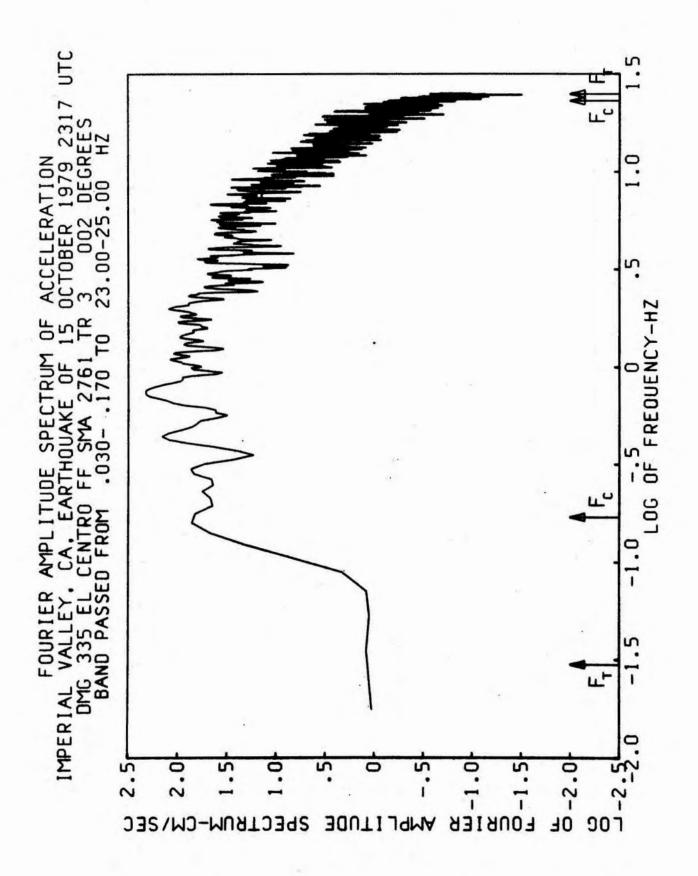


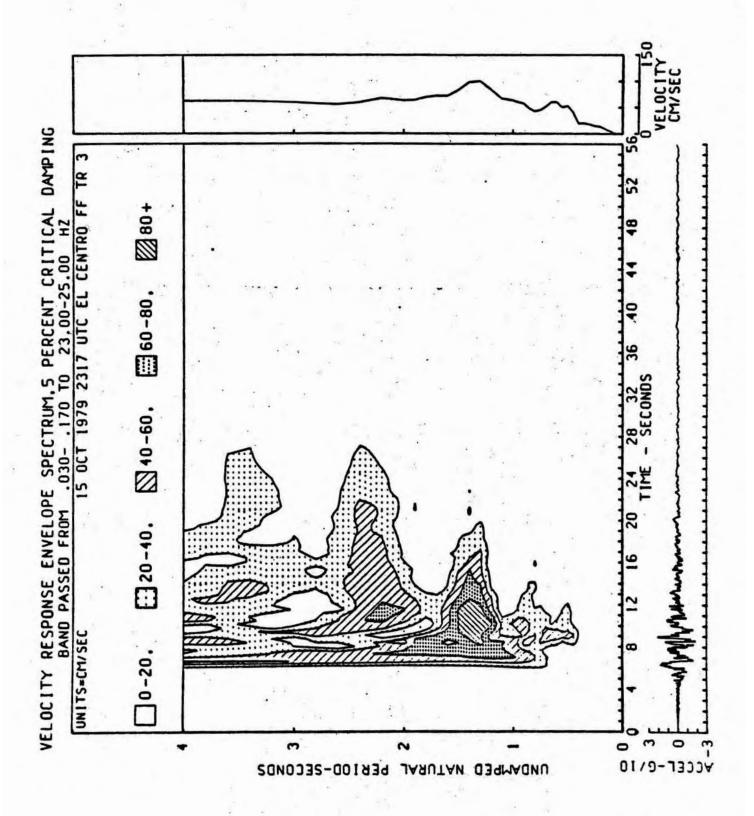
RESPONSE SPECTRA

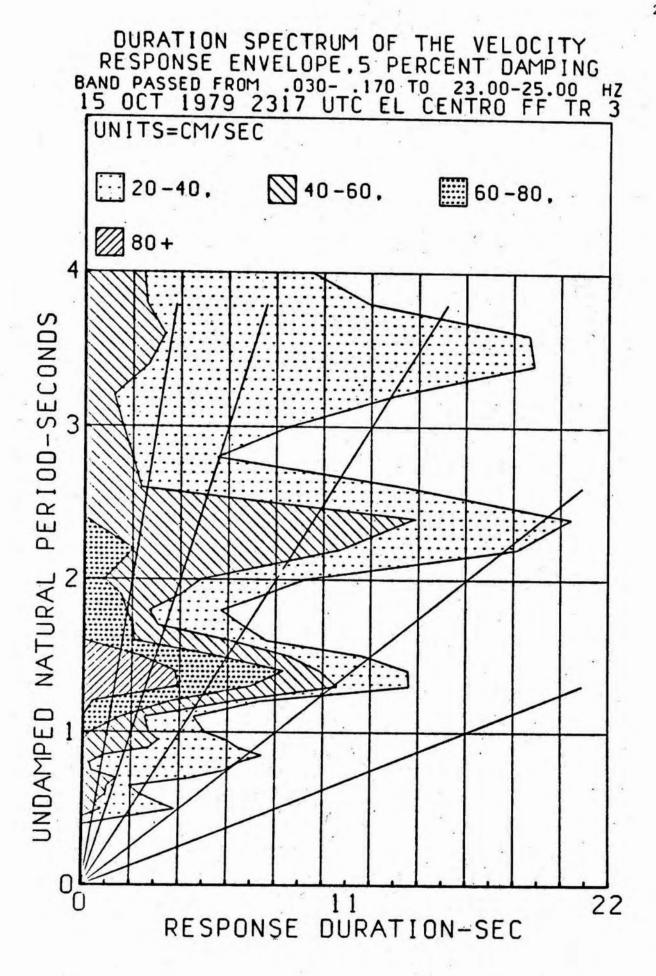
15 OCT 1979 2317 UTC EL CENTRO FF TR 3 0.2.5.10.20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



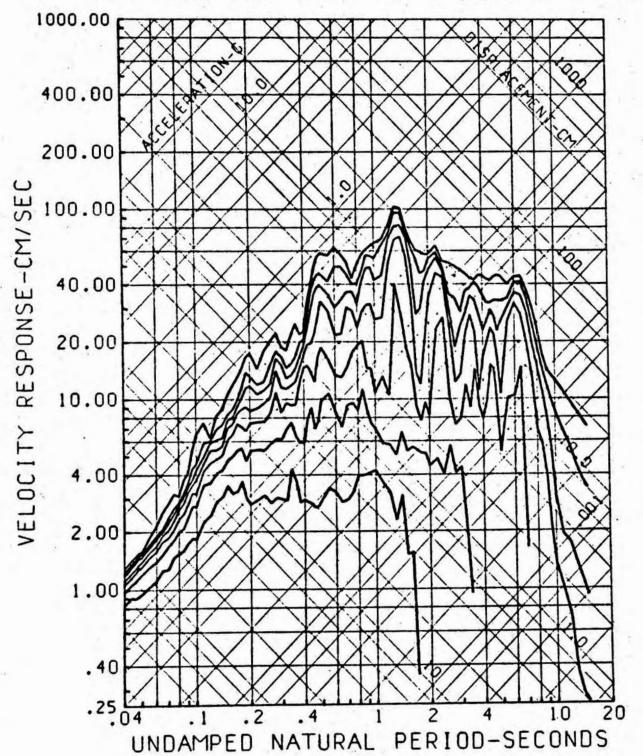


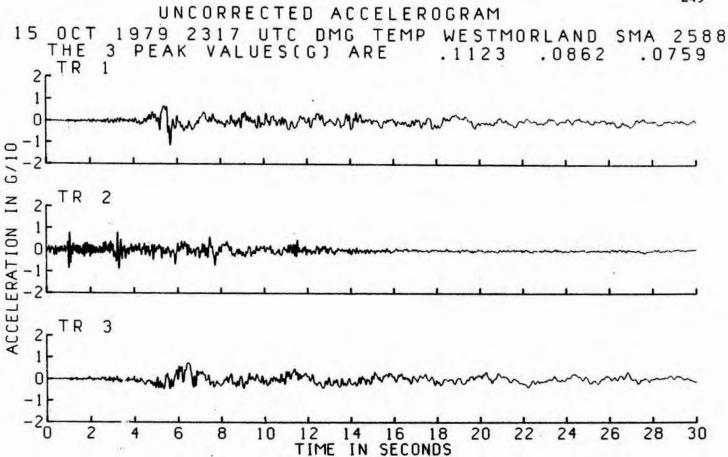


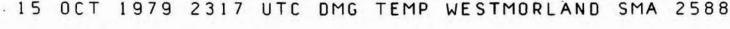


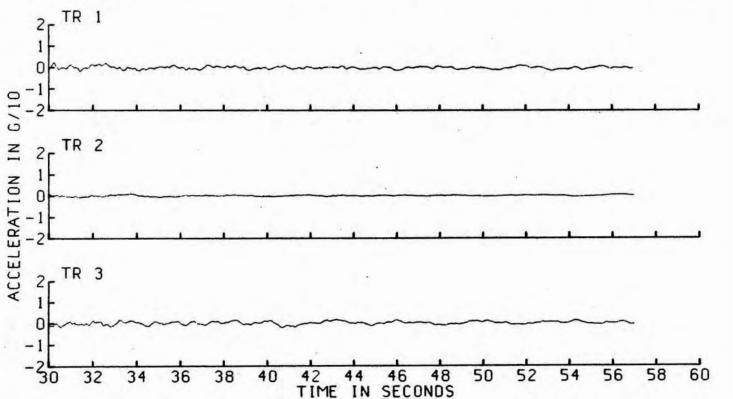


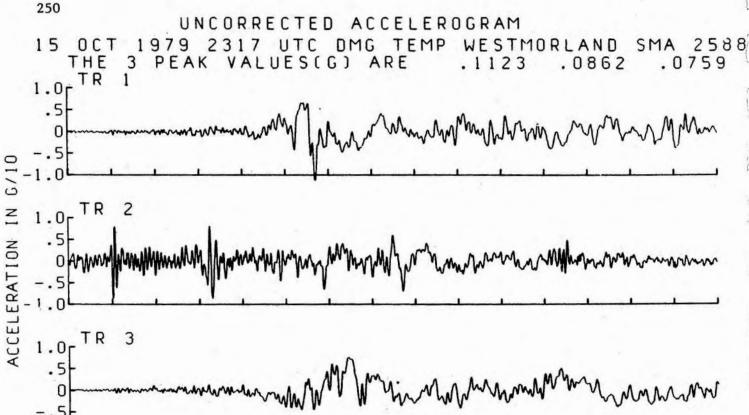
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC EL CENTRO FF TR 3 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

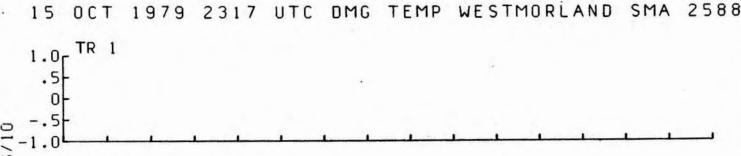




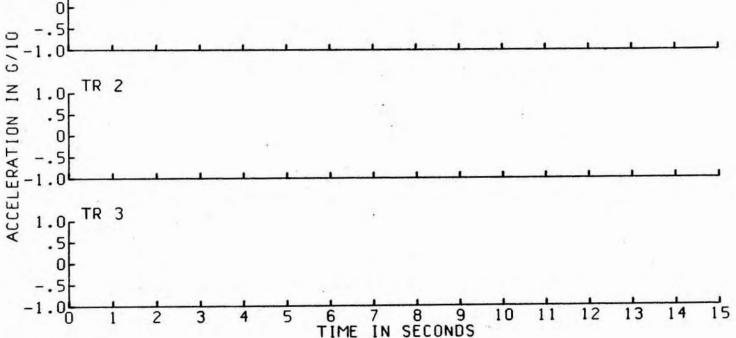


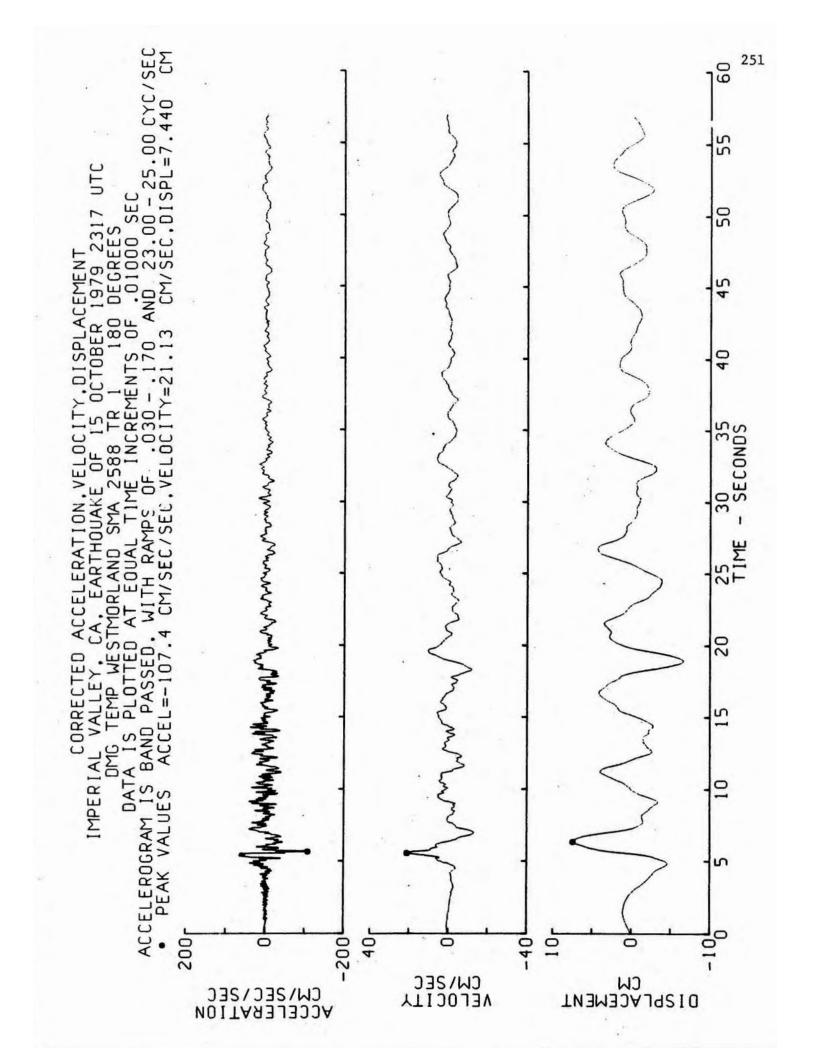




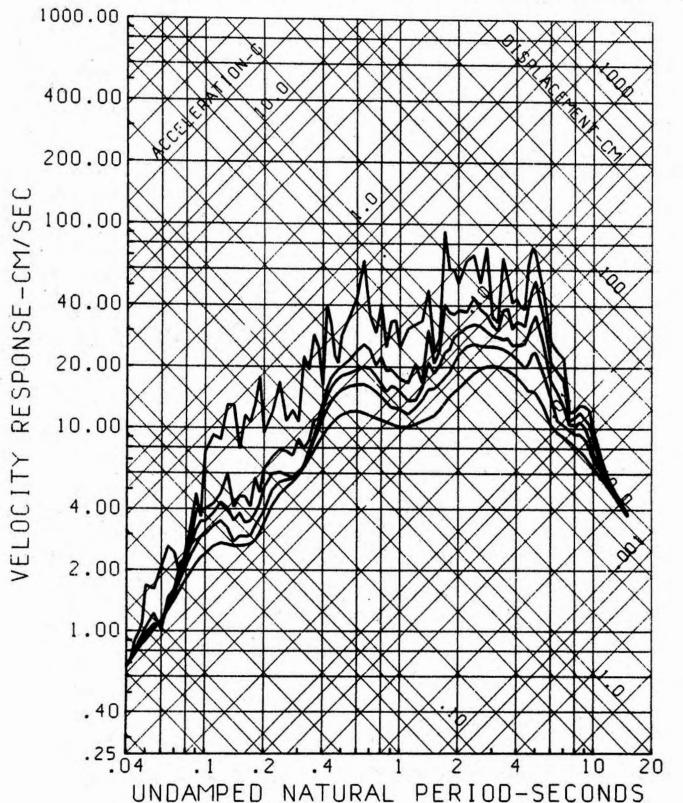


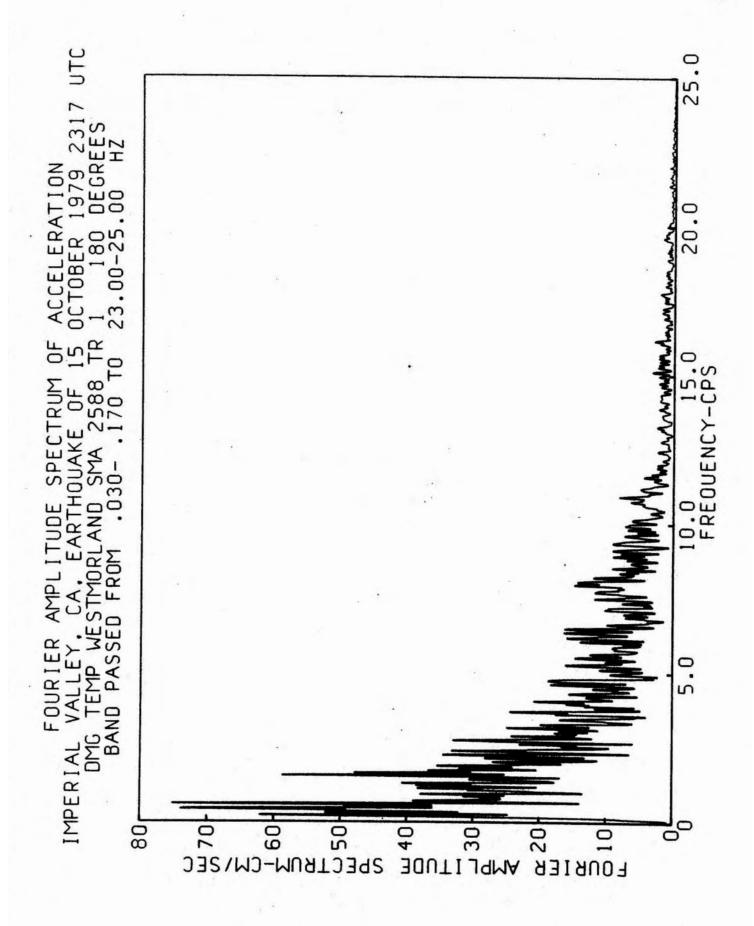
6 7 8 9 TIME IN SECONDS

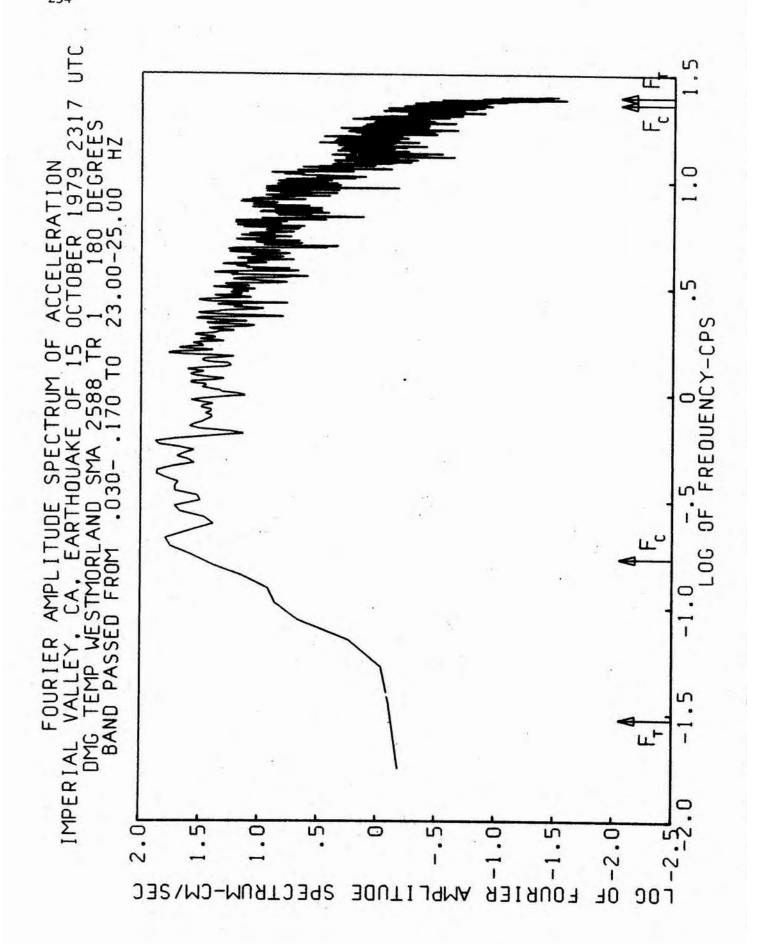


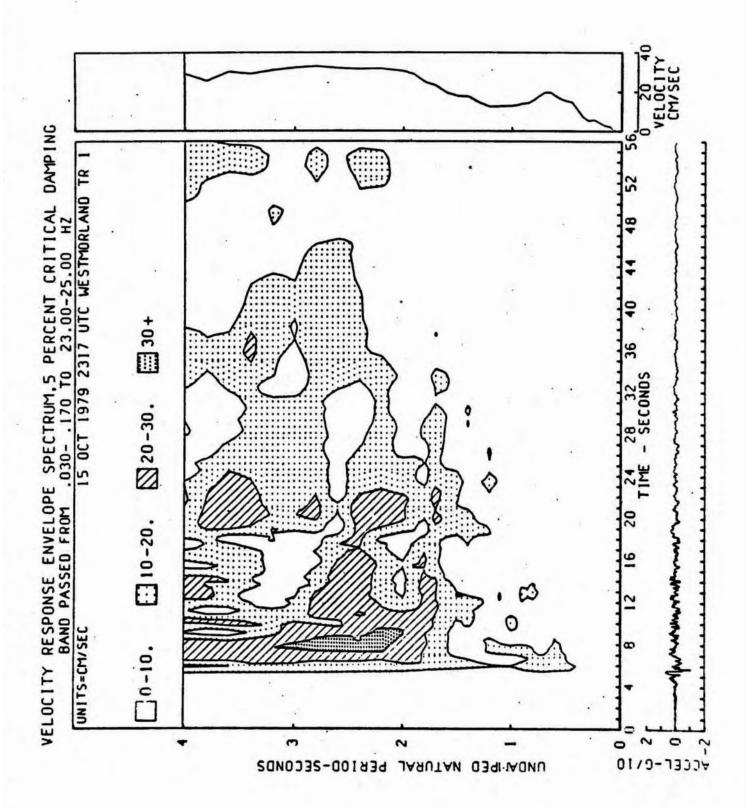


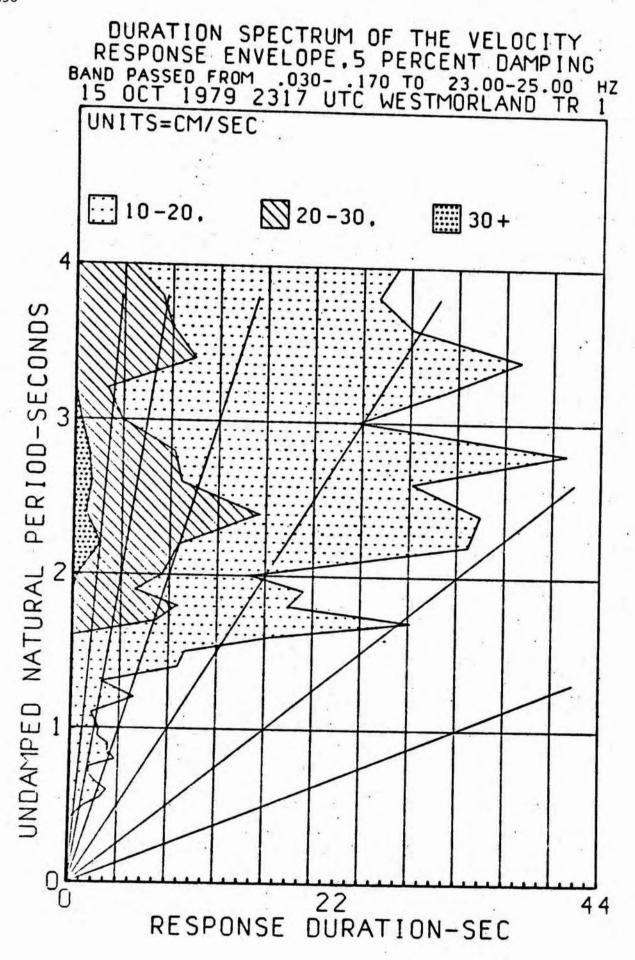
RESPONSE SPECTRA
15 OCT 1979 2317 UTC WESTMORLAND TR 1
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ







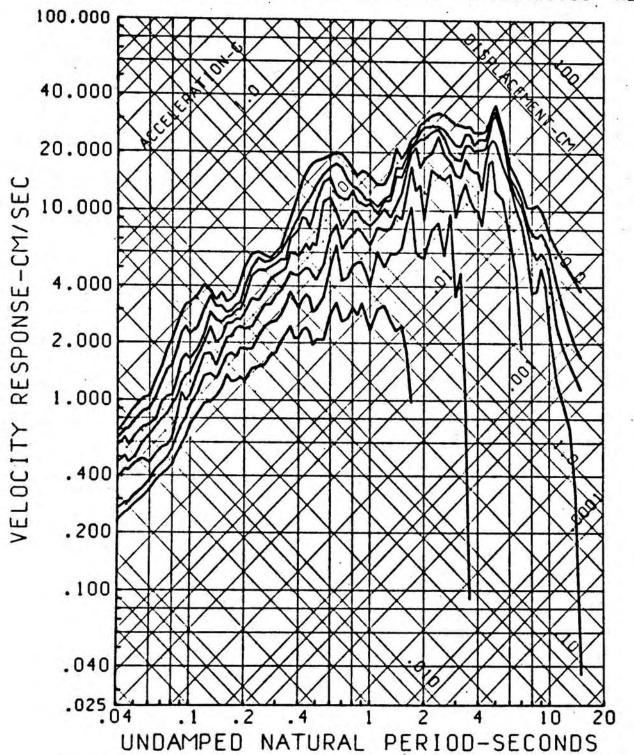


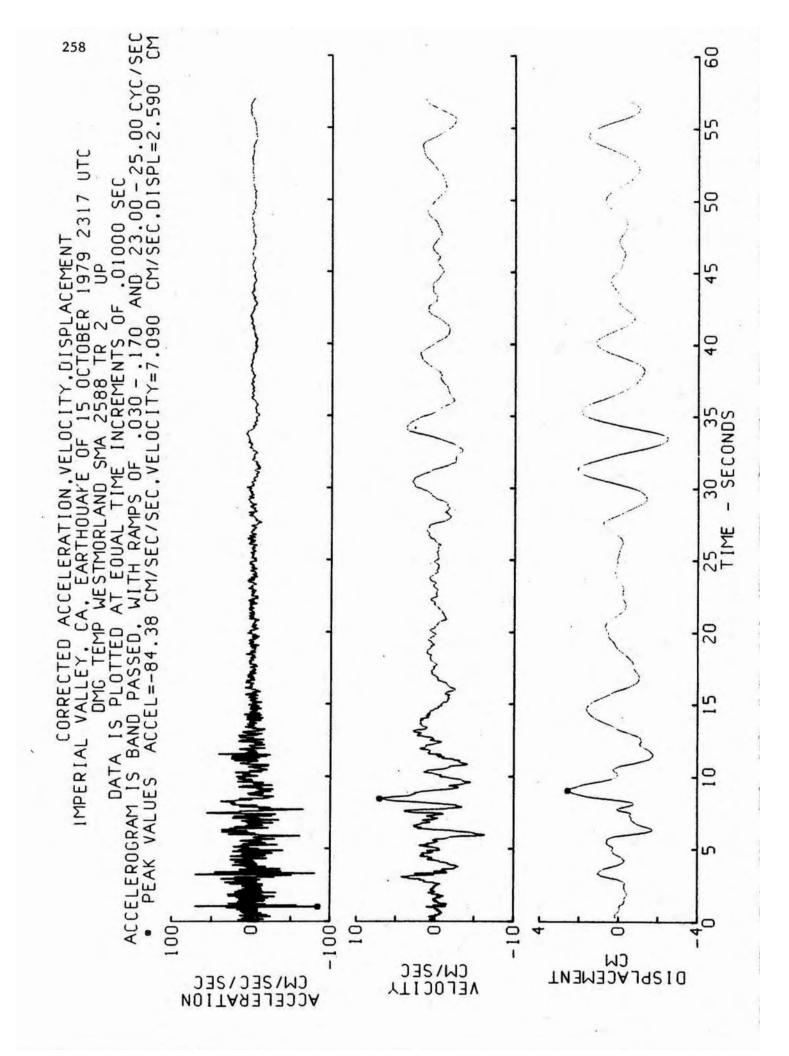


SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES.

15 OCT 1979 2317 UTC WESTMORLAND TR 1

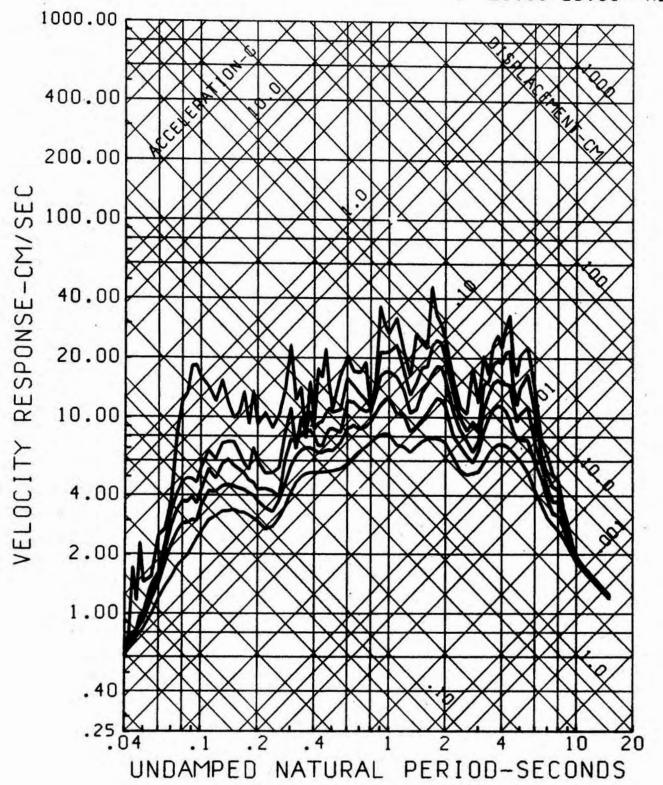
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

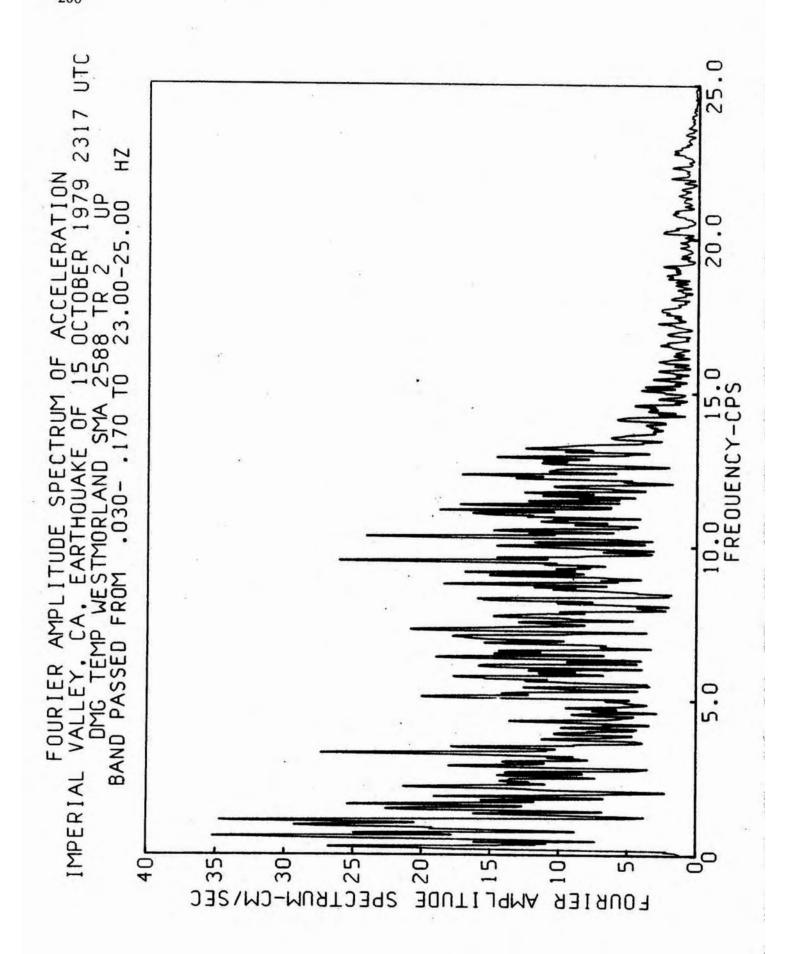


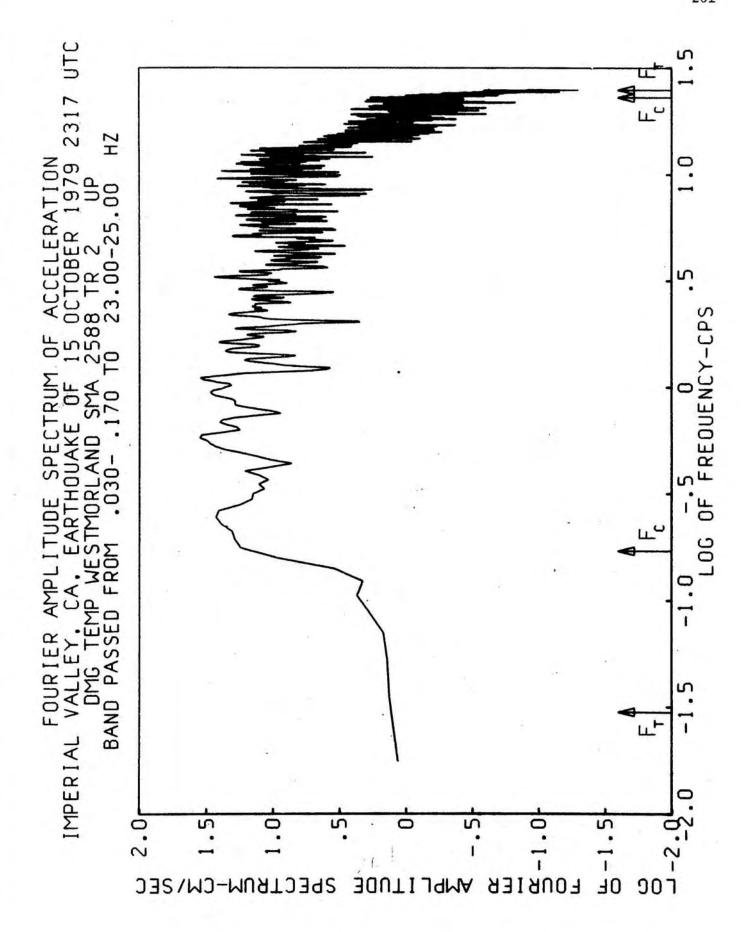


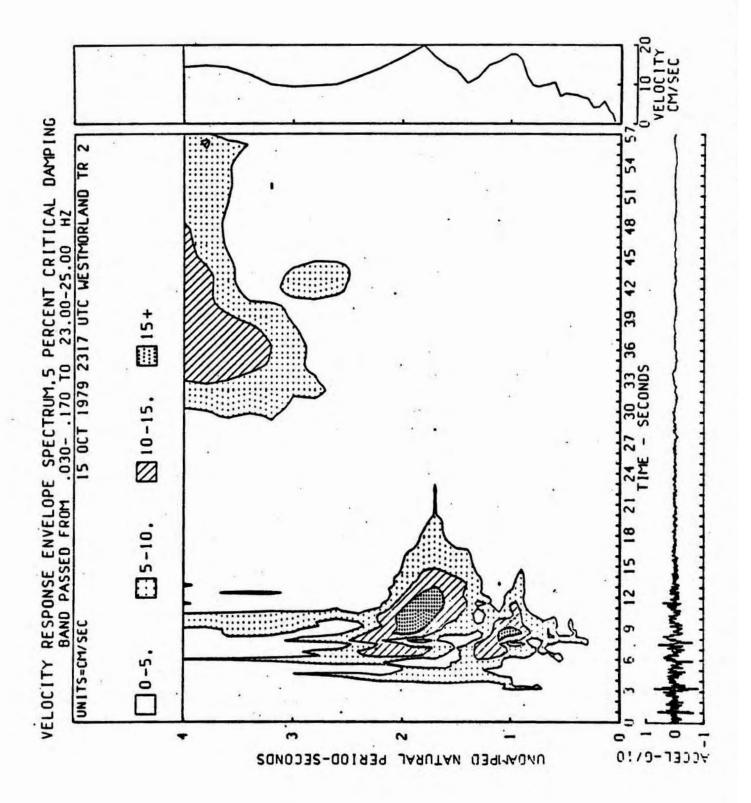
## RESPONSE SPECTRA

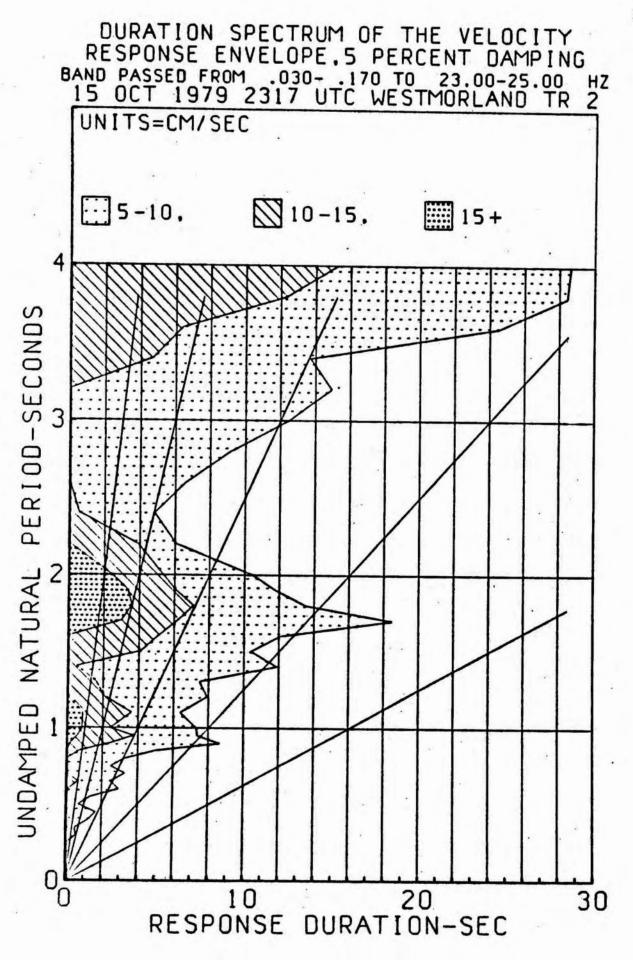
15 OCT 1979 2317 UTC WESTMORLAND TR 2 0,2,5,10,20 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



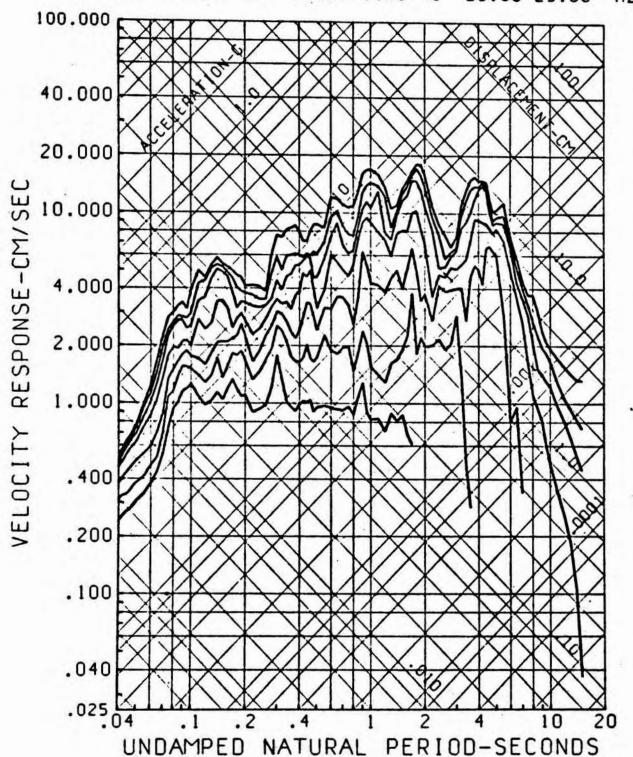


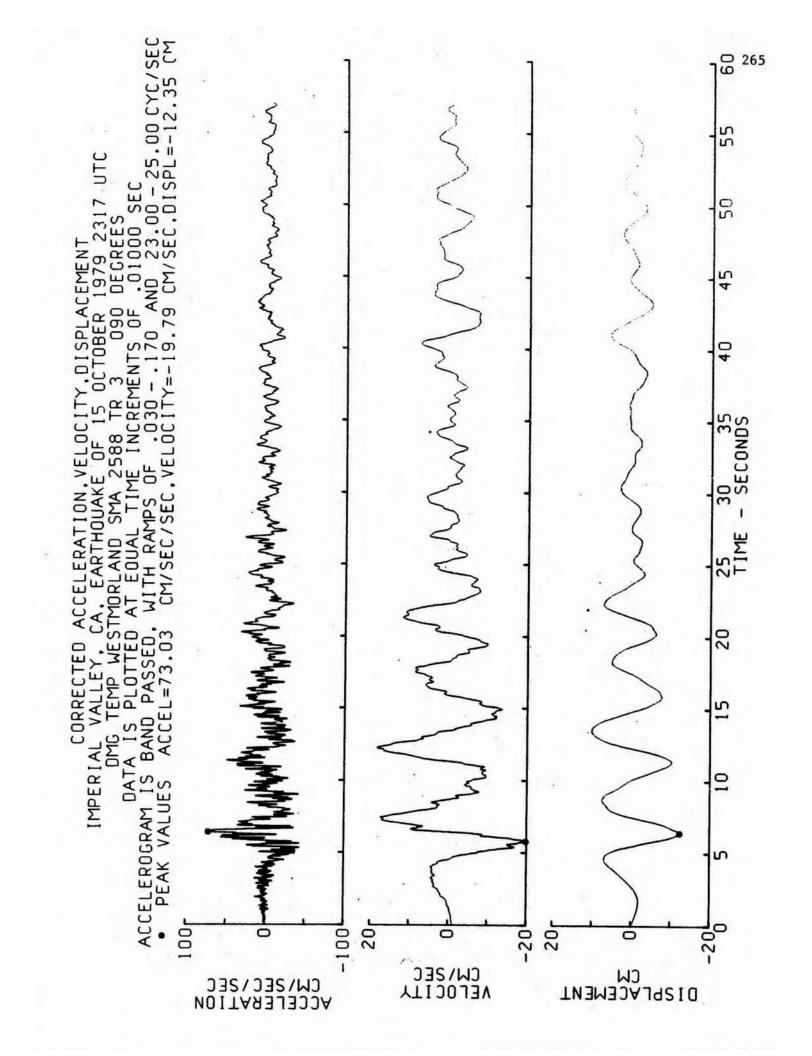






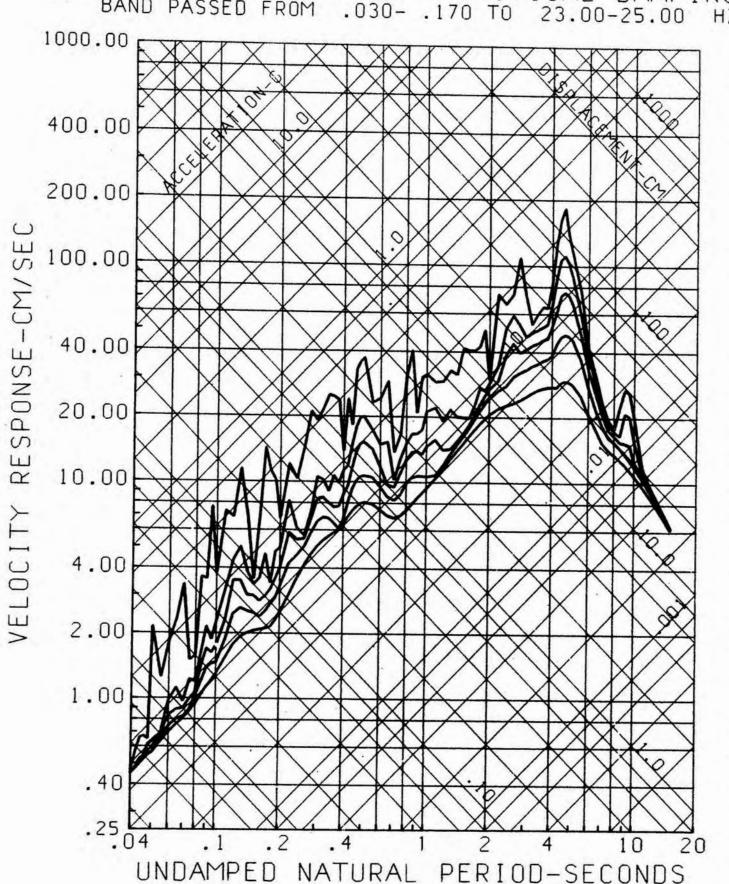
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC WESTMORLAND TR 2 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

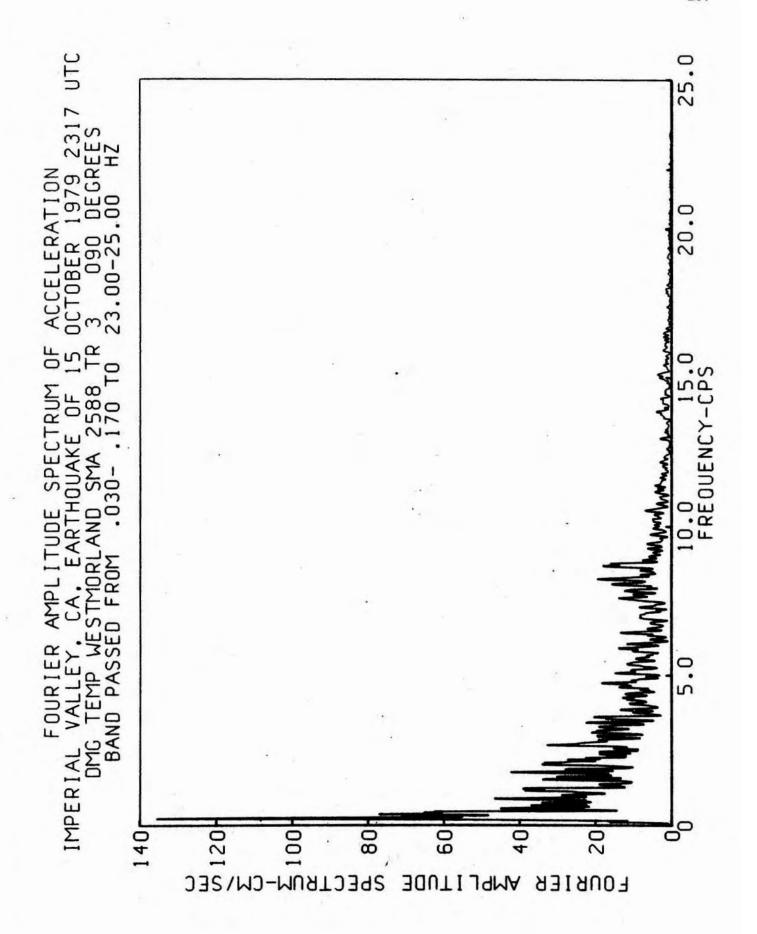


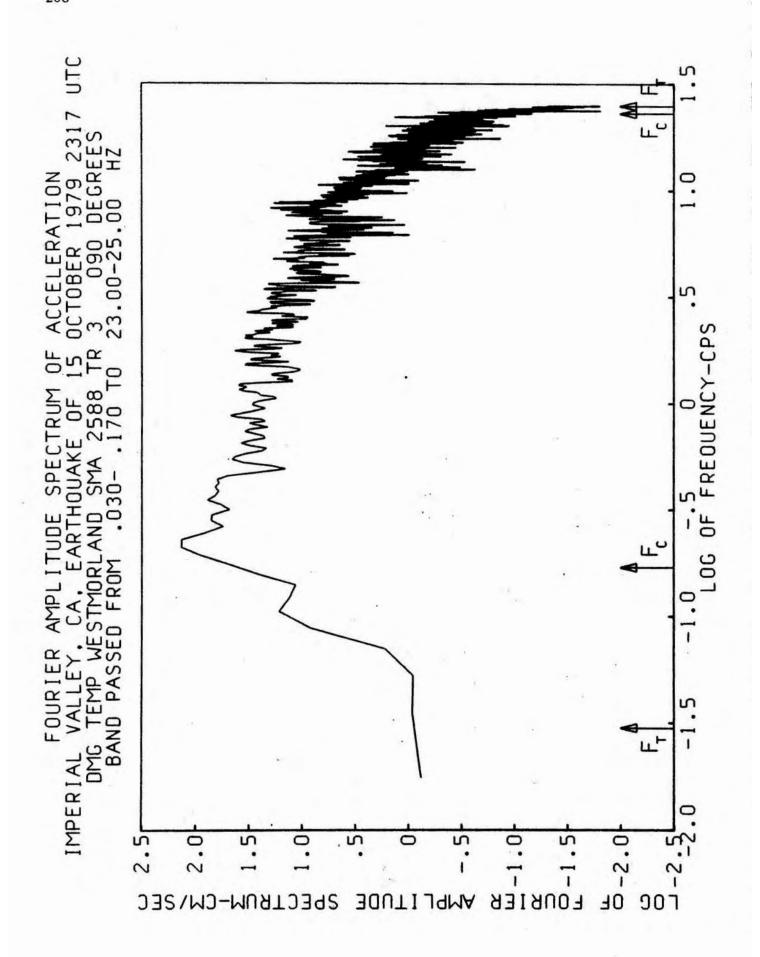


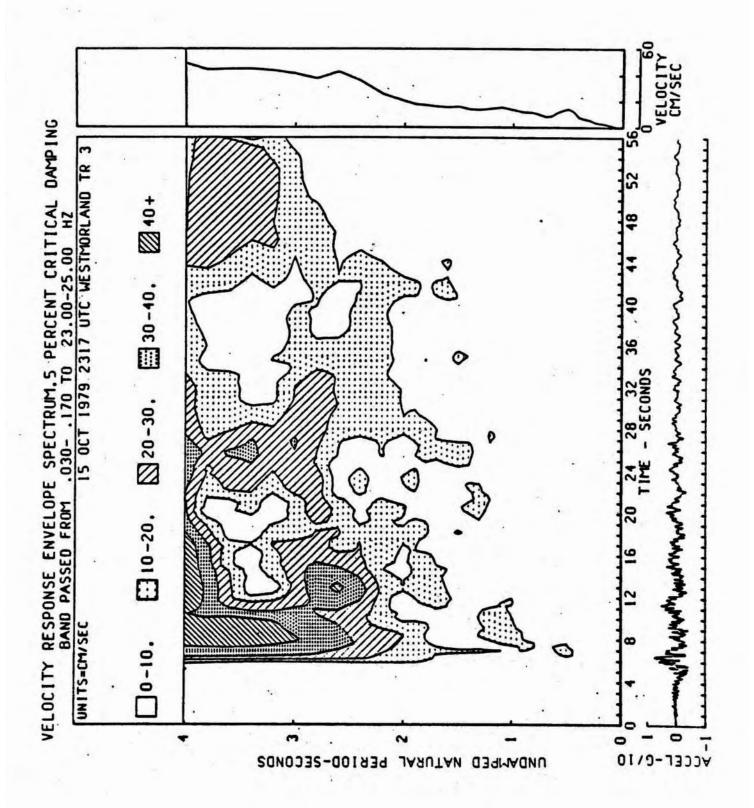
RESPONSE SPECTRA

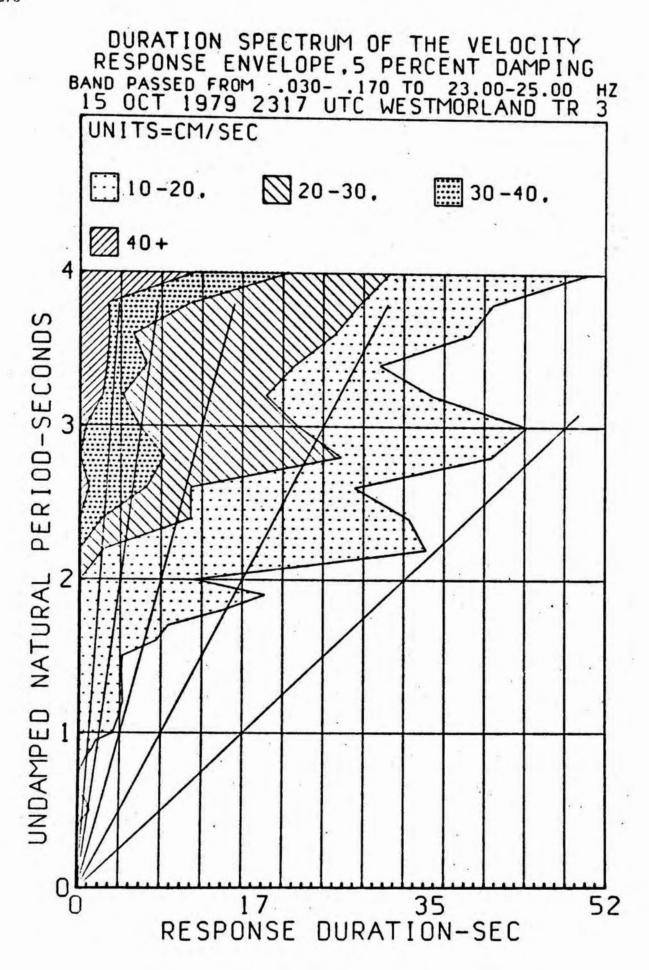
15 OCT 1979 2317 UTC WESTMORLAND TR :
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23,00-25,00 HZ



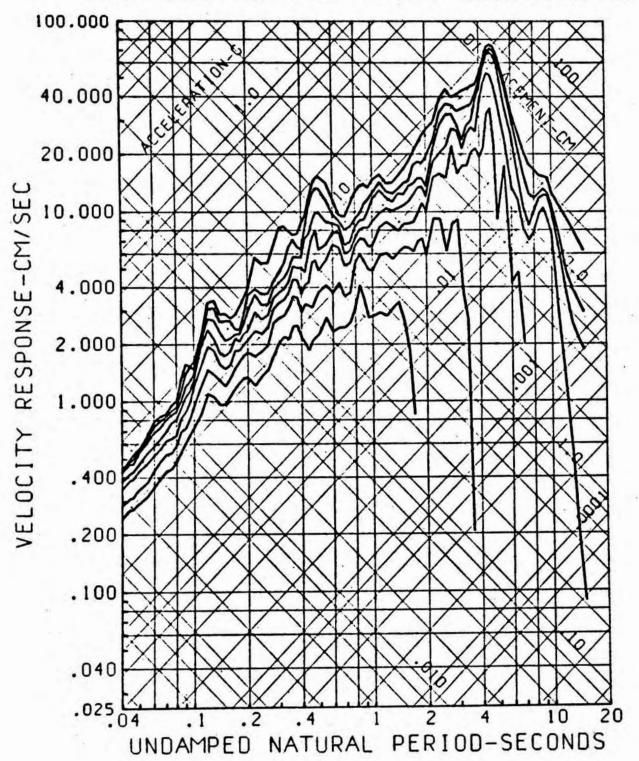


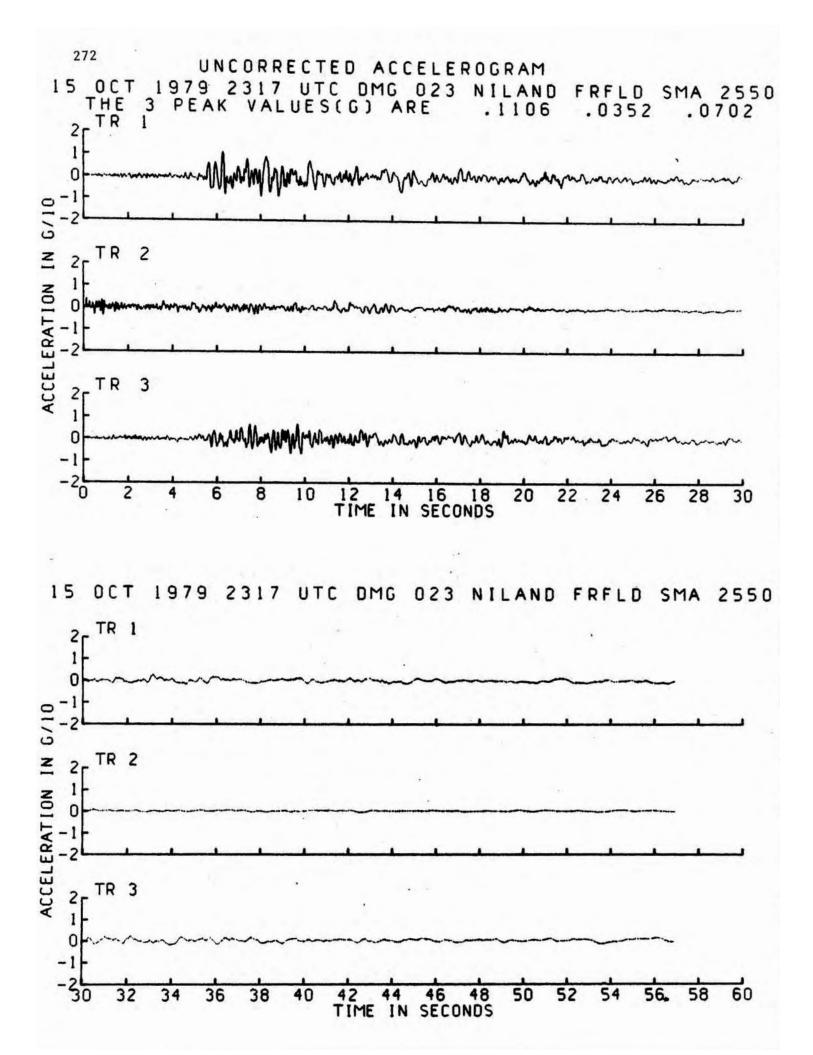


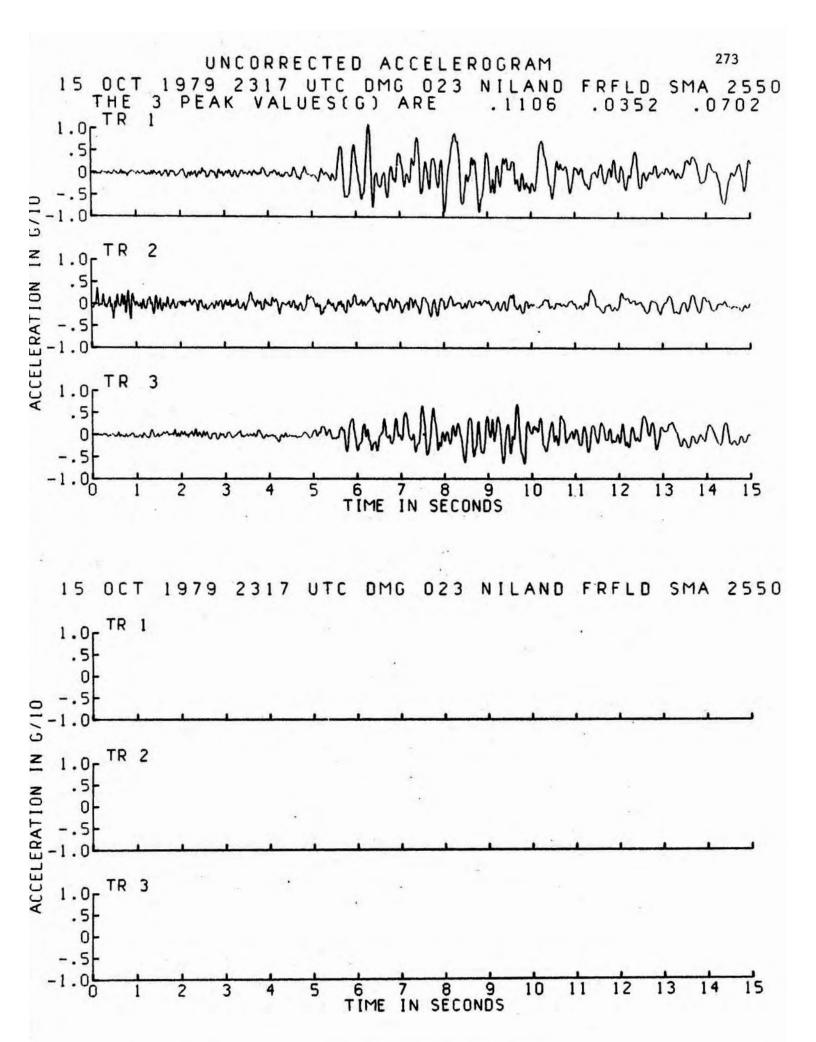




SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC WESTMORLAND TR 3 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ





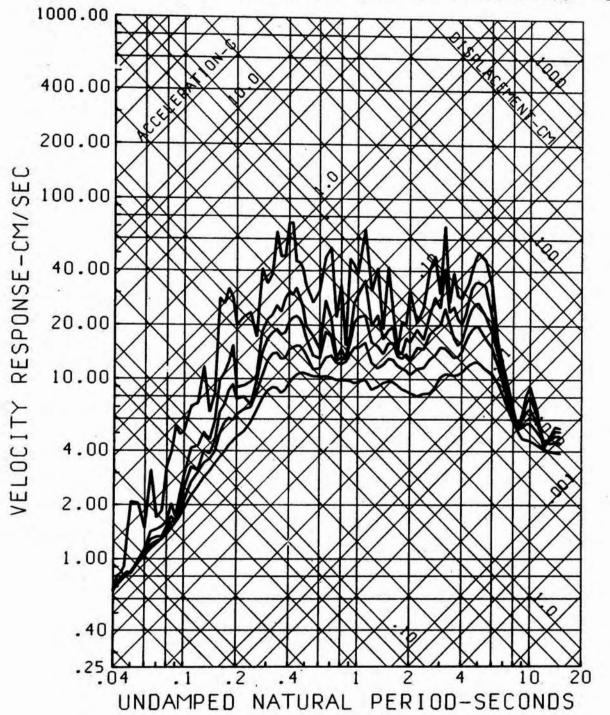


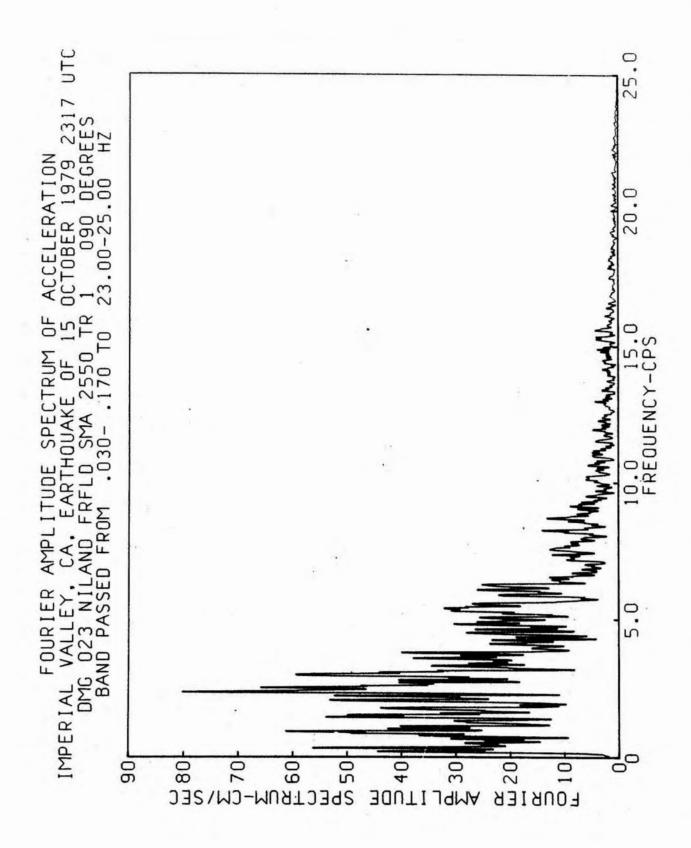
CW\SEC AEFOCITY

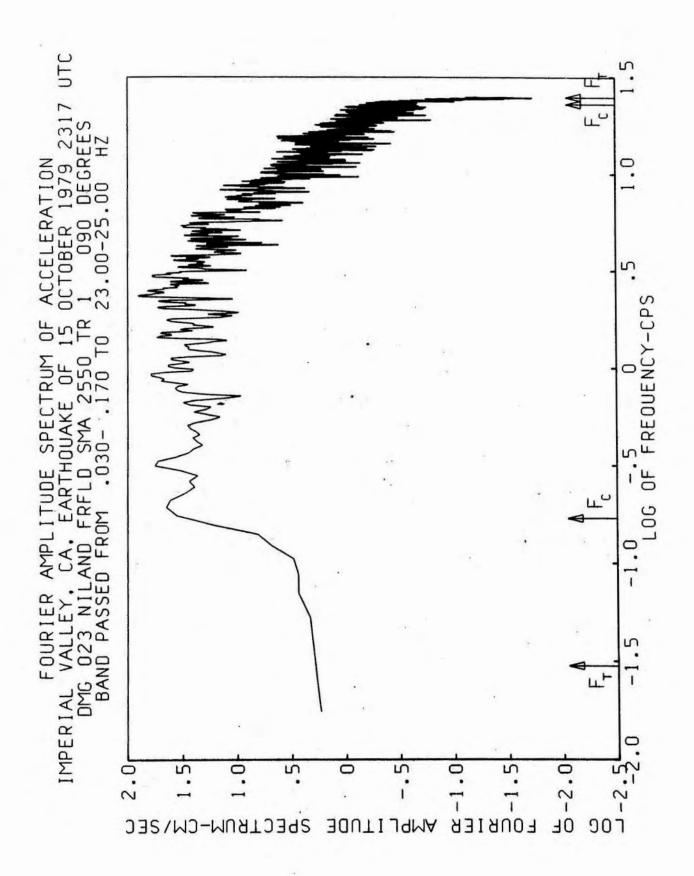
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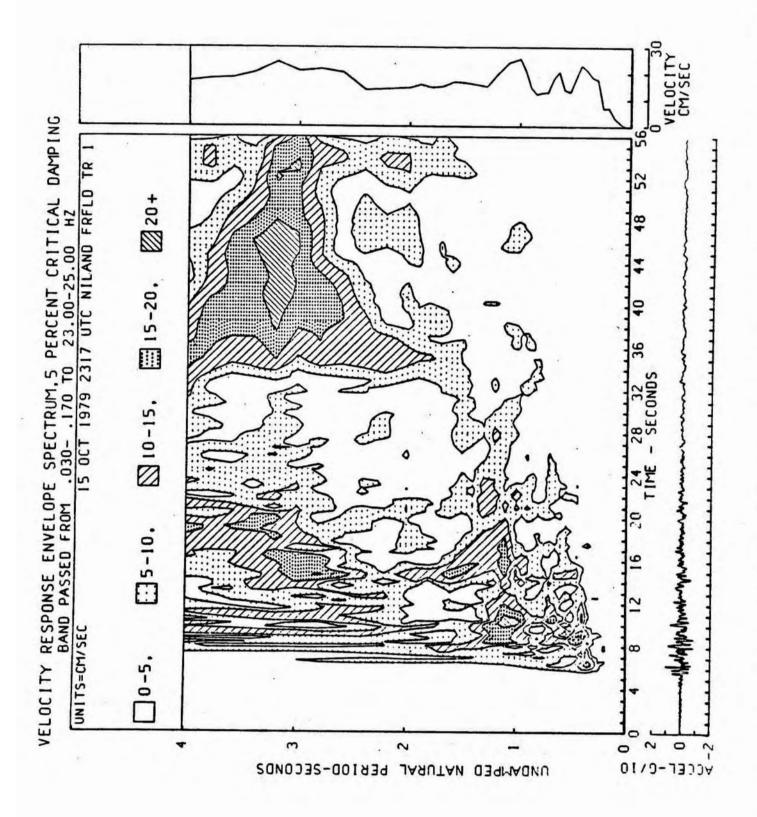
RESPONSE SPECTRA

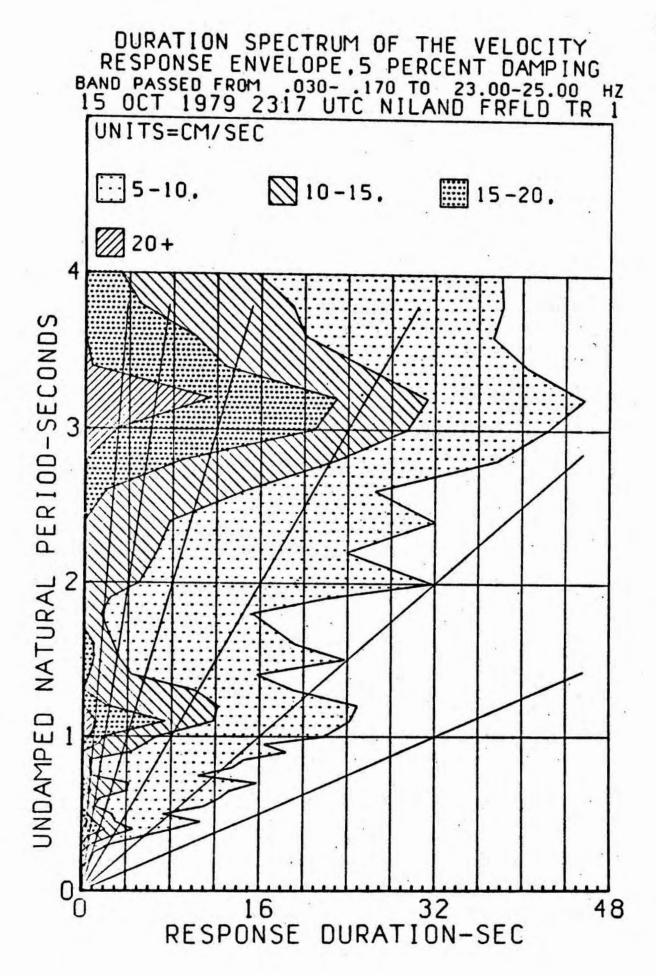
15 OCT 1979 2317 UTC NILAND FRFLD TR 1
0.2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



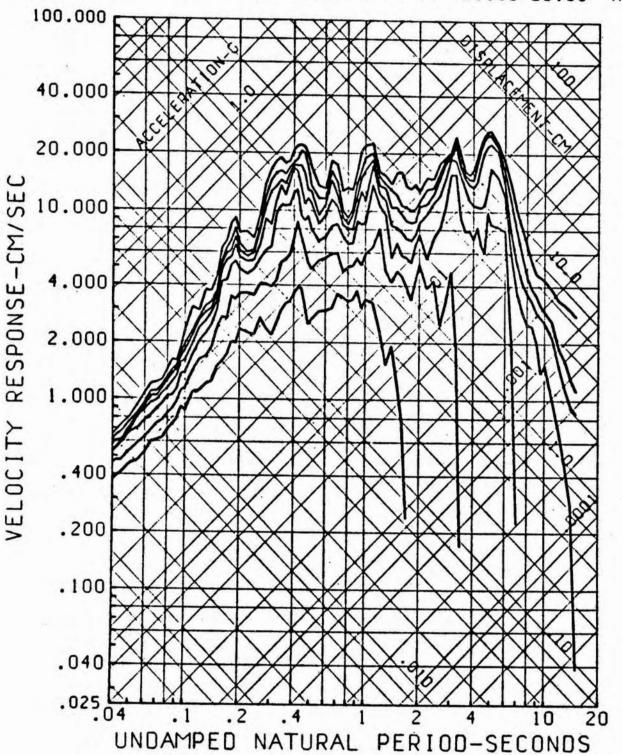


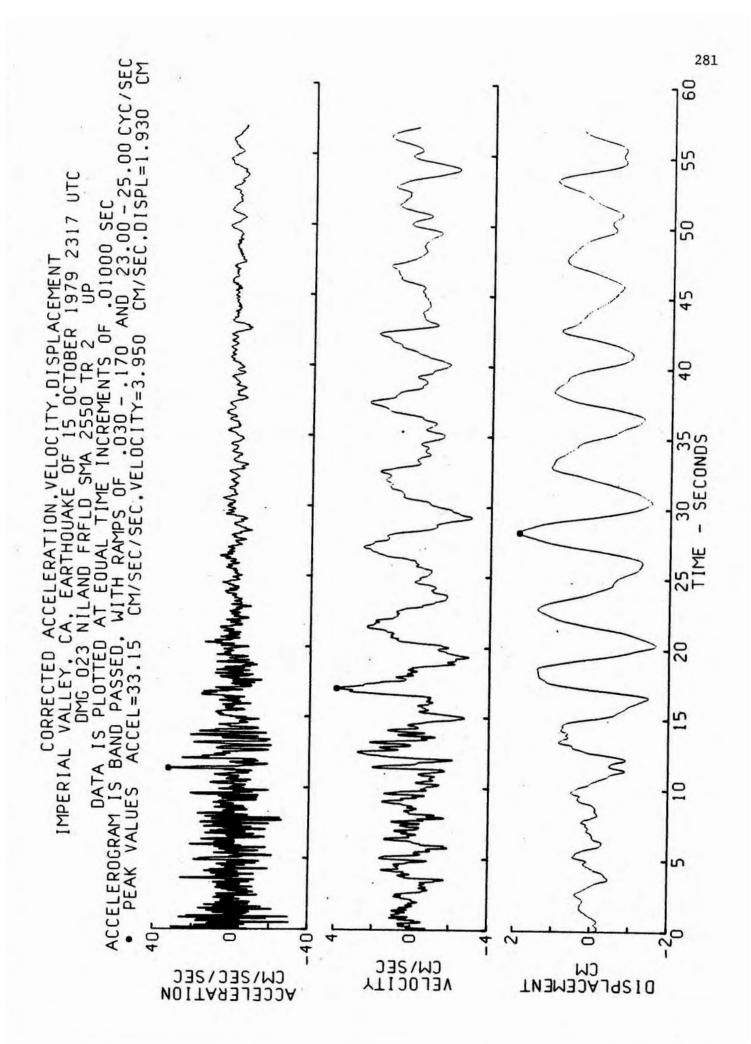






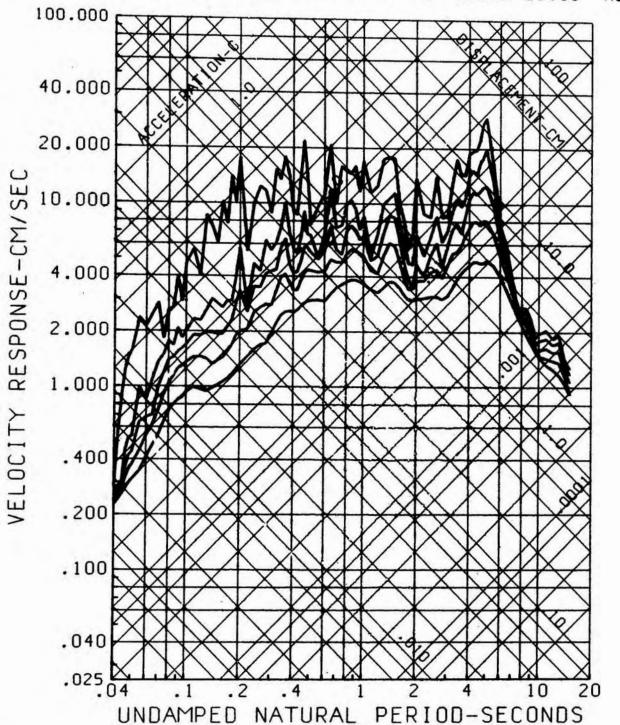
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC NILAND FRFLD TR 1 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

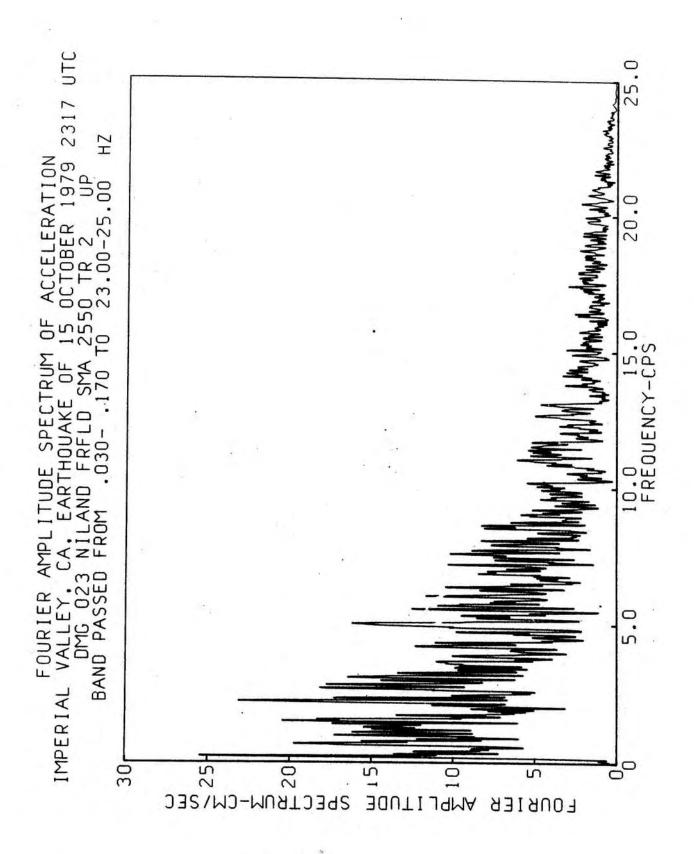


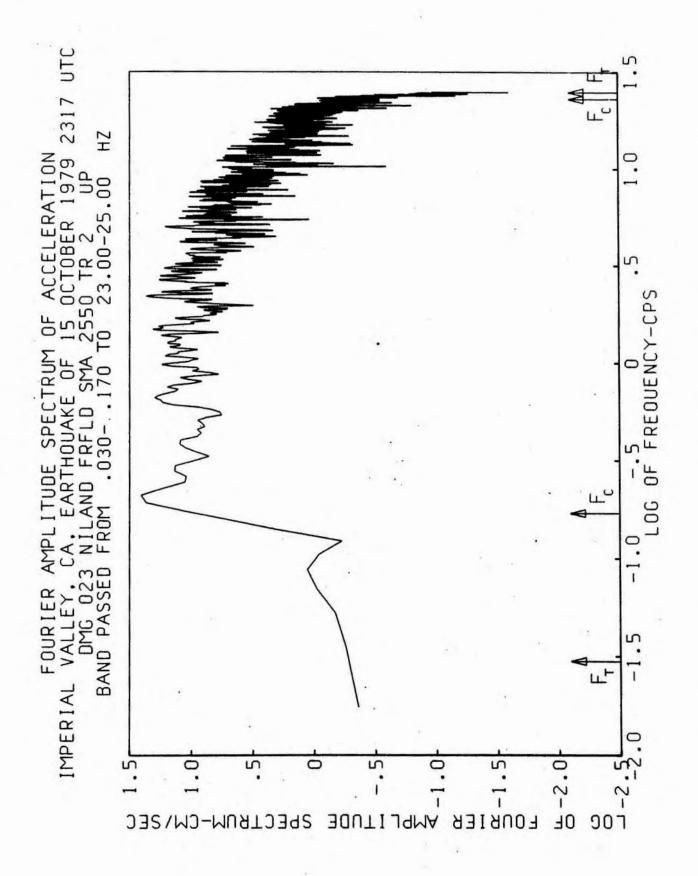


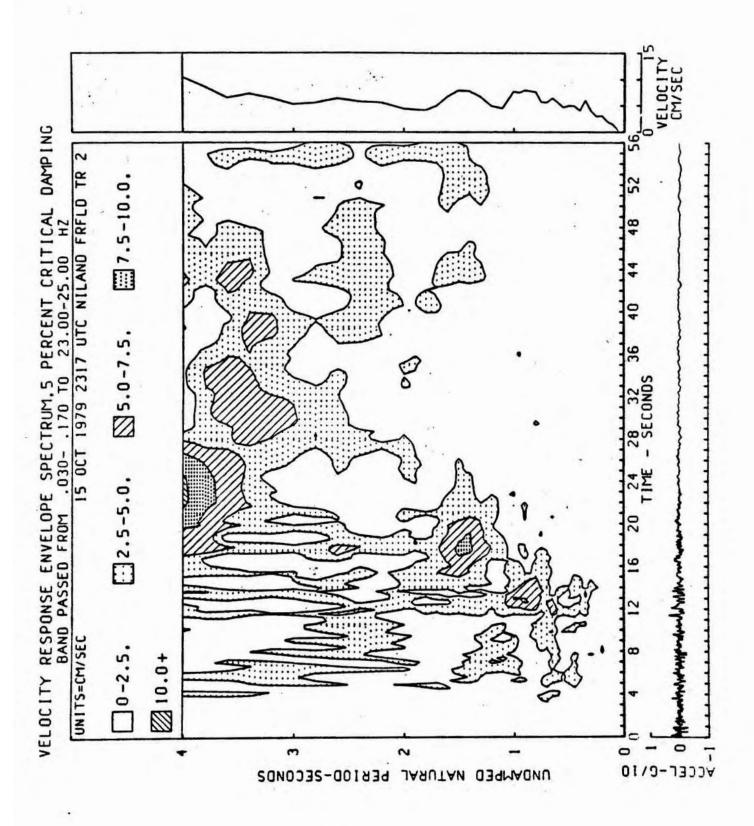
RESPONSE SPECTRA

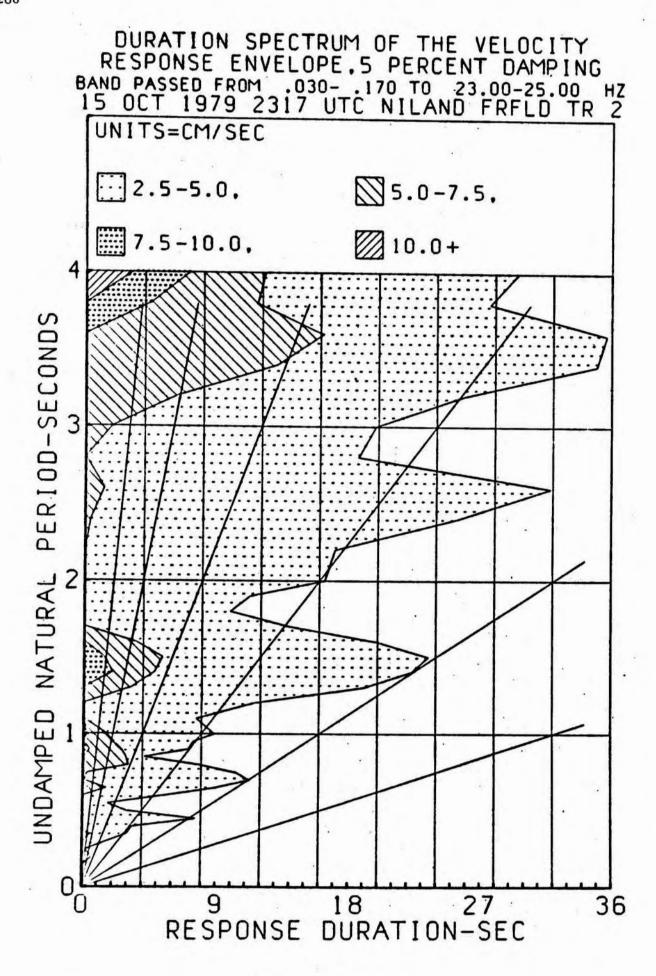
15 OCT 1979 2317 UTC NILAND FRFLD TR 2
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



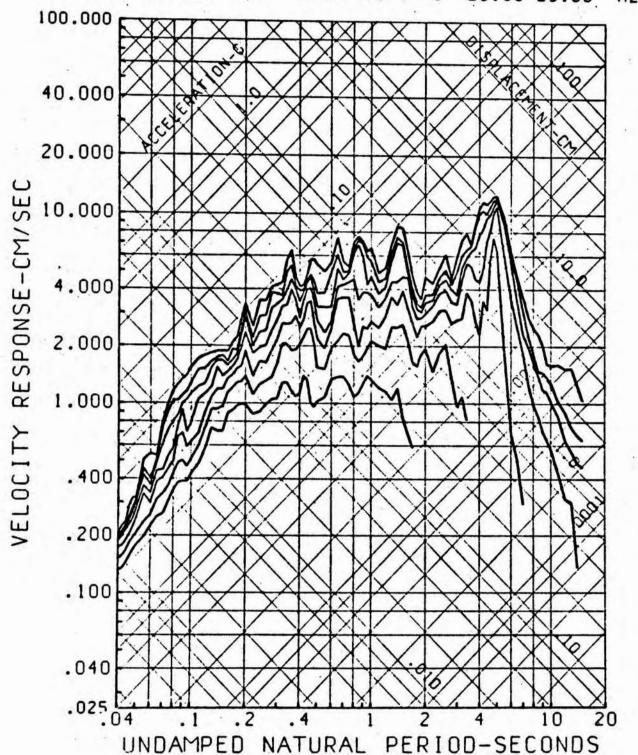


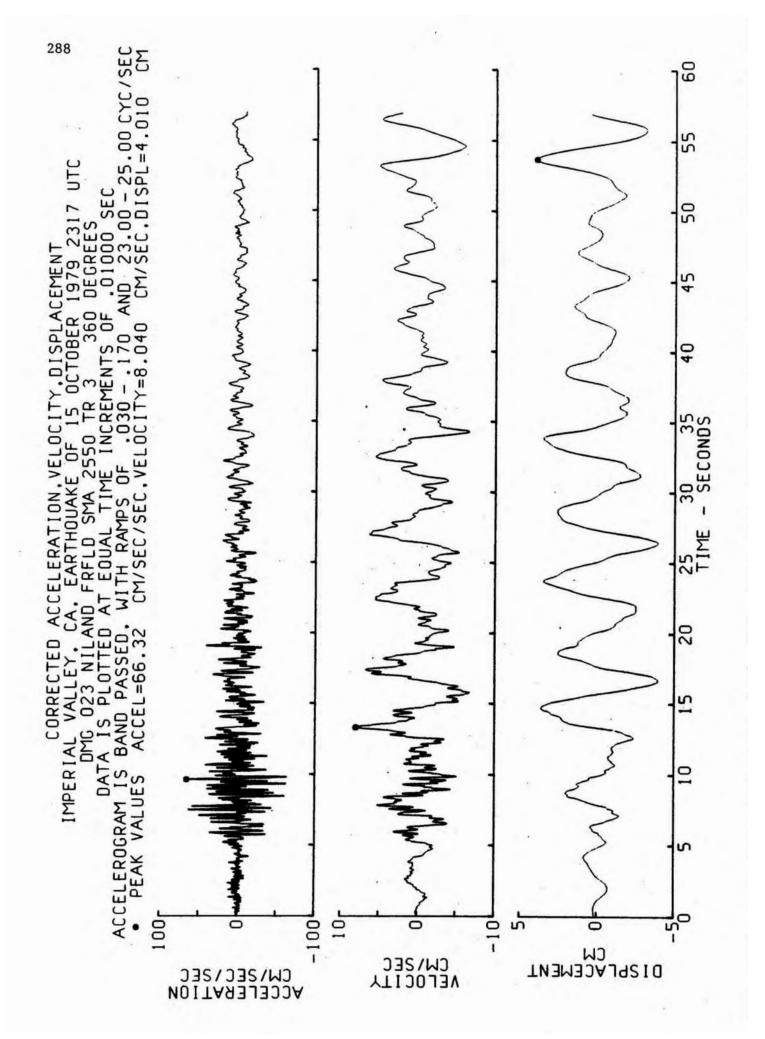






SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 2317 UTC NILAND FRFLD TR 2 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

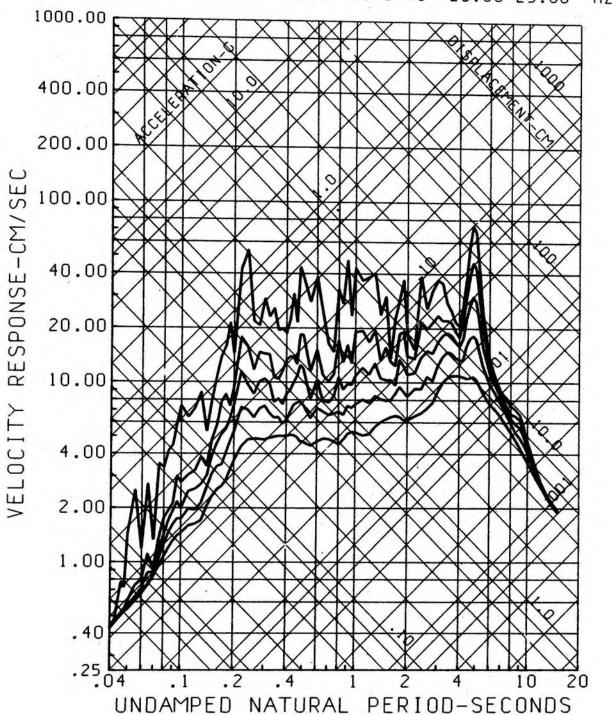


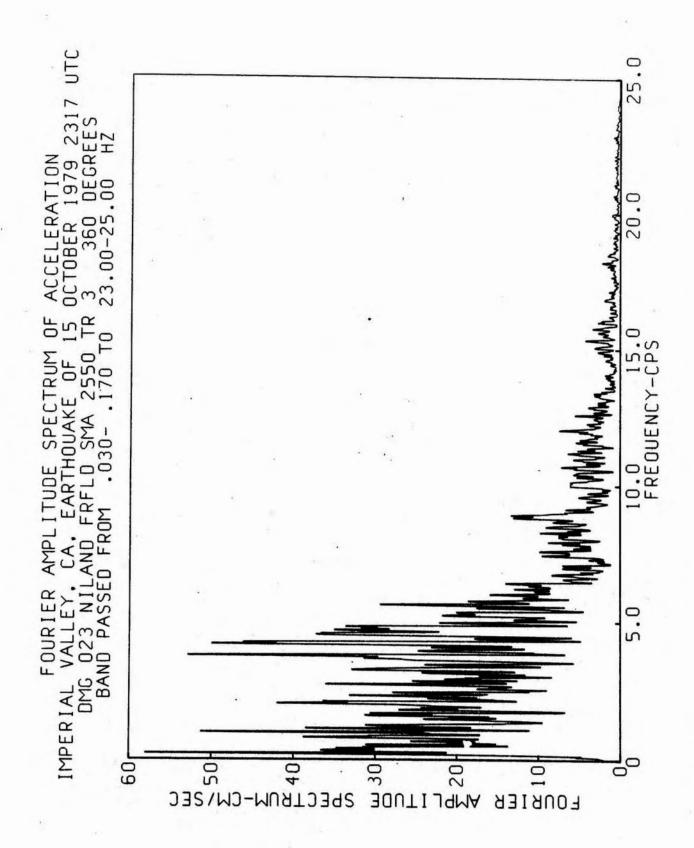


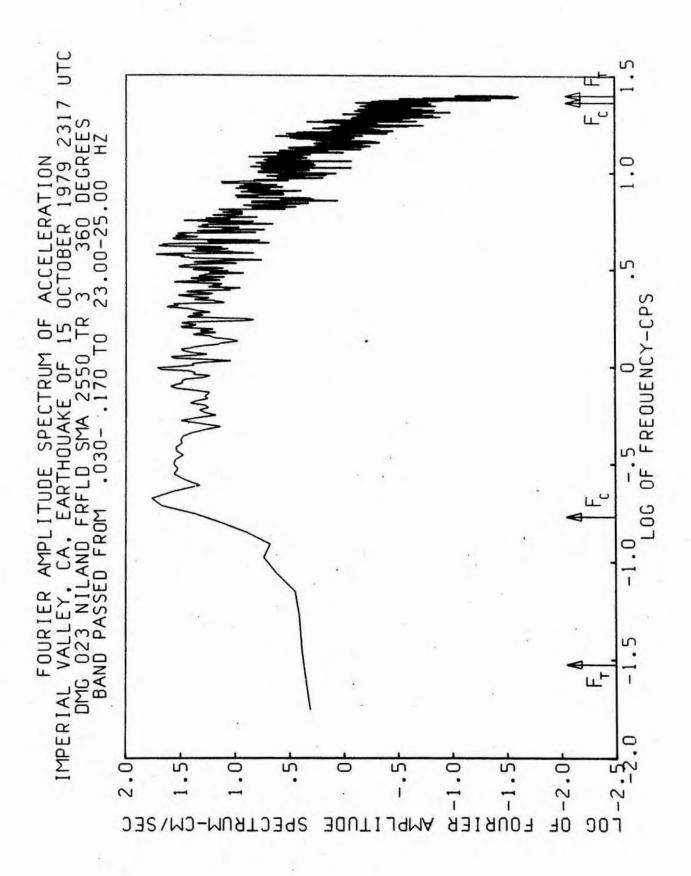
RESPONSE SPECTRA

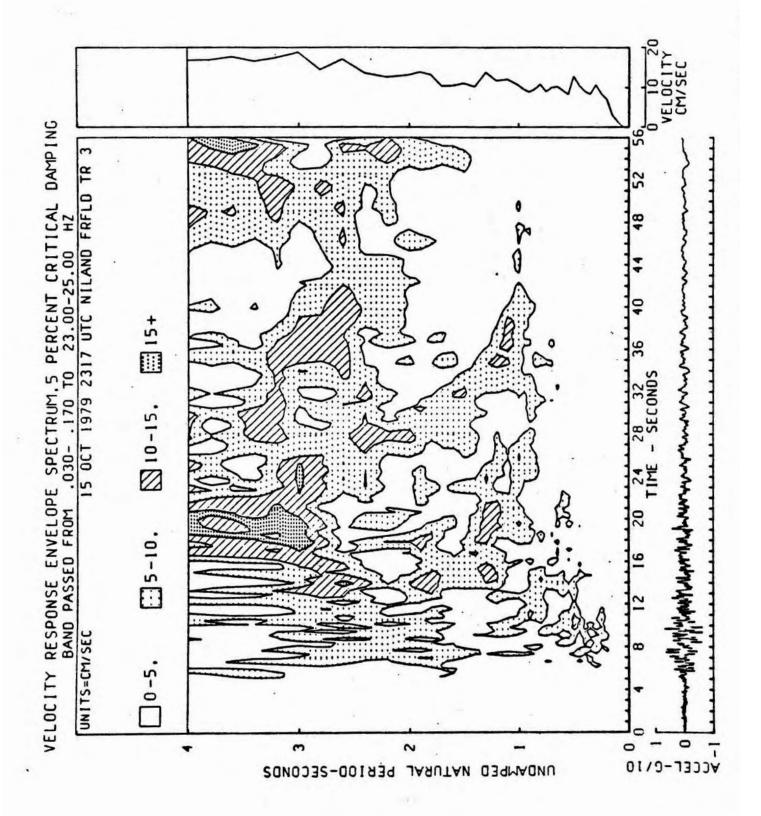
15 OCT 1979 2317 UTC NILAND FRFLD TR 3

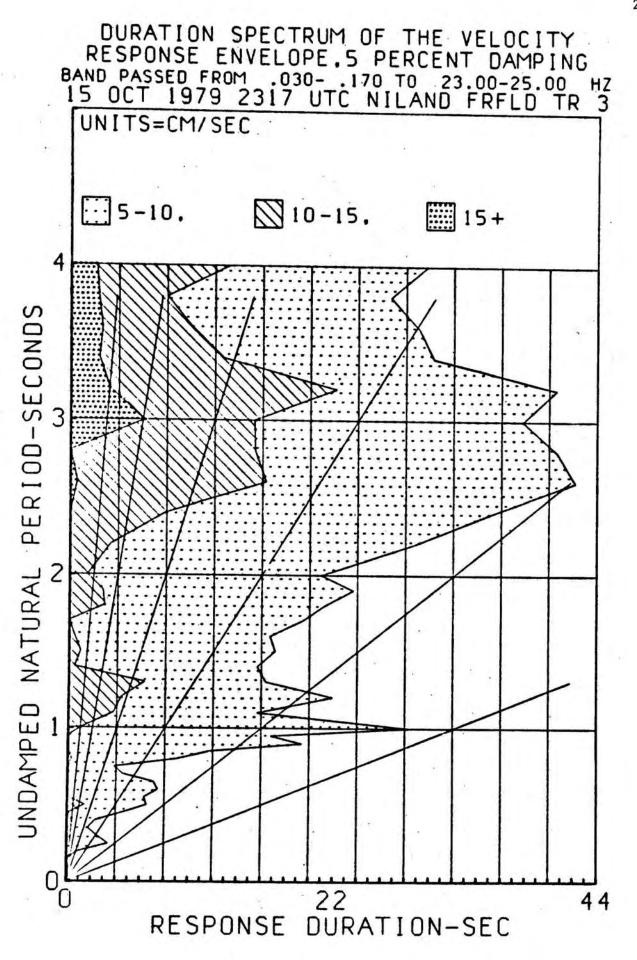
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



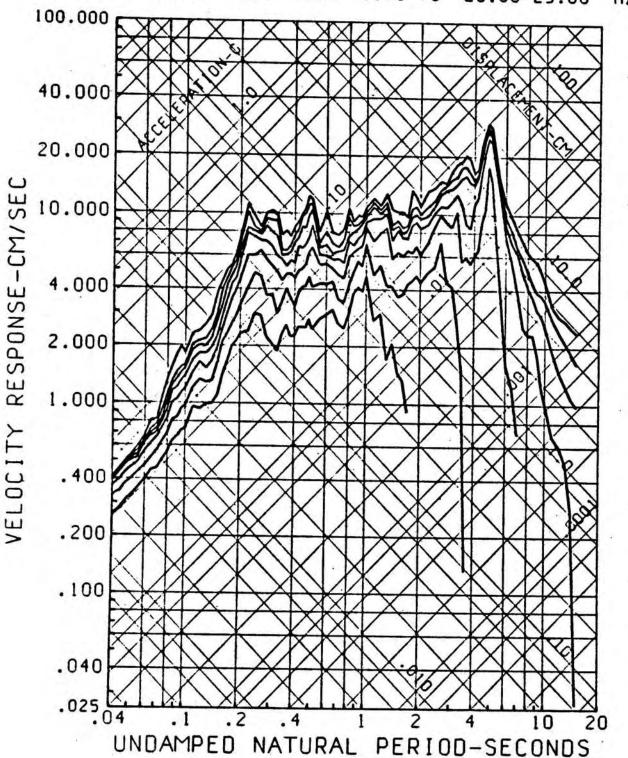


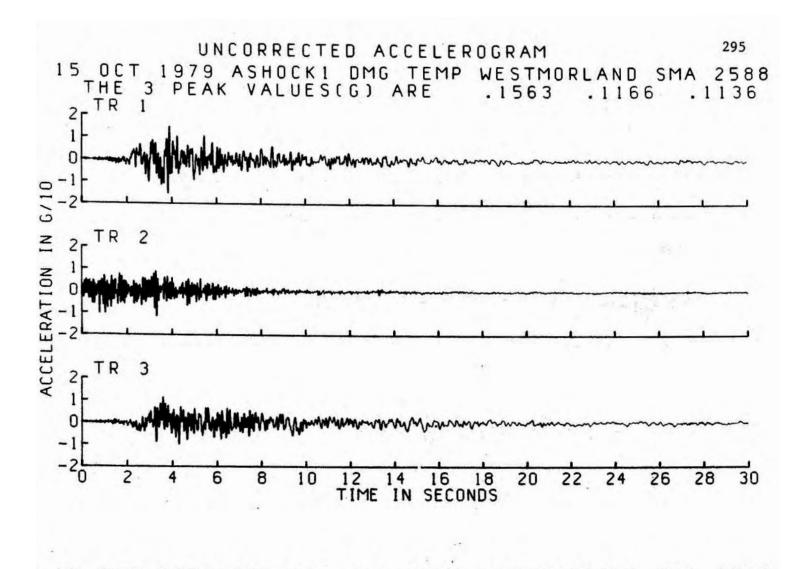


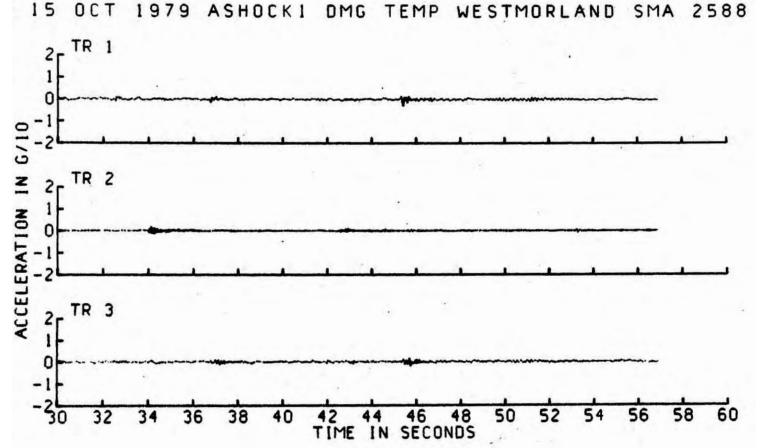


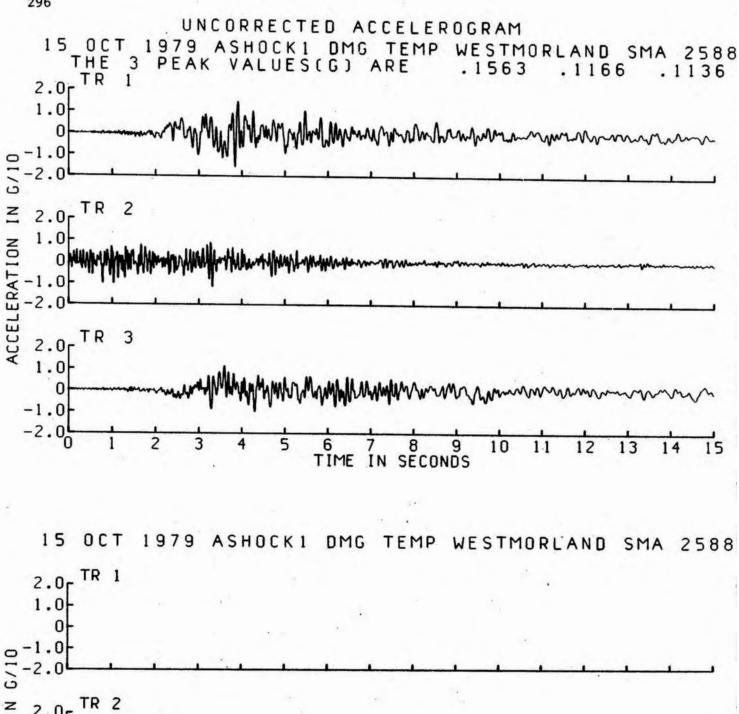


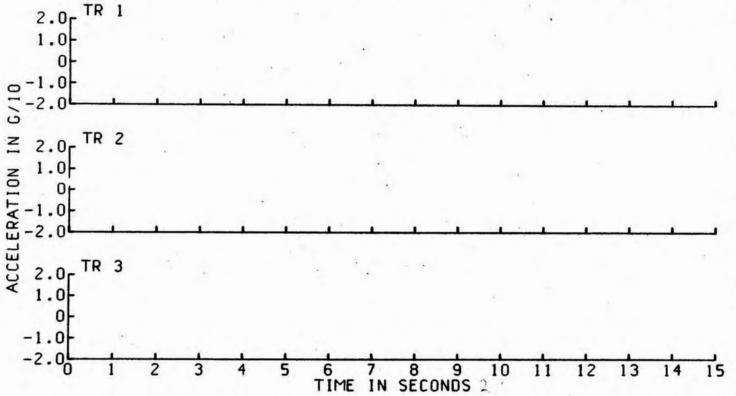
SPECTRA OF AMPLITUDES SUSTAINED
FOR ANY GIVEN NUMBER OF CYCLES
15 OCT 1979 2317 UTC NILAND FRFLD TR 3
5 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

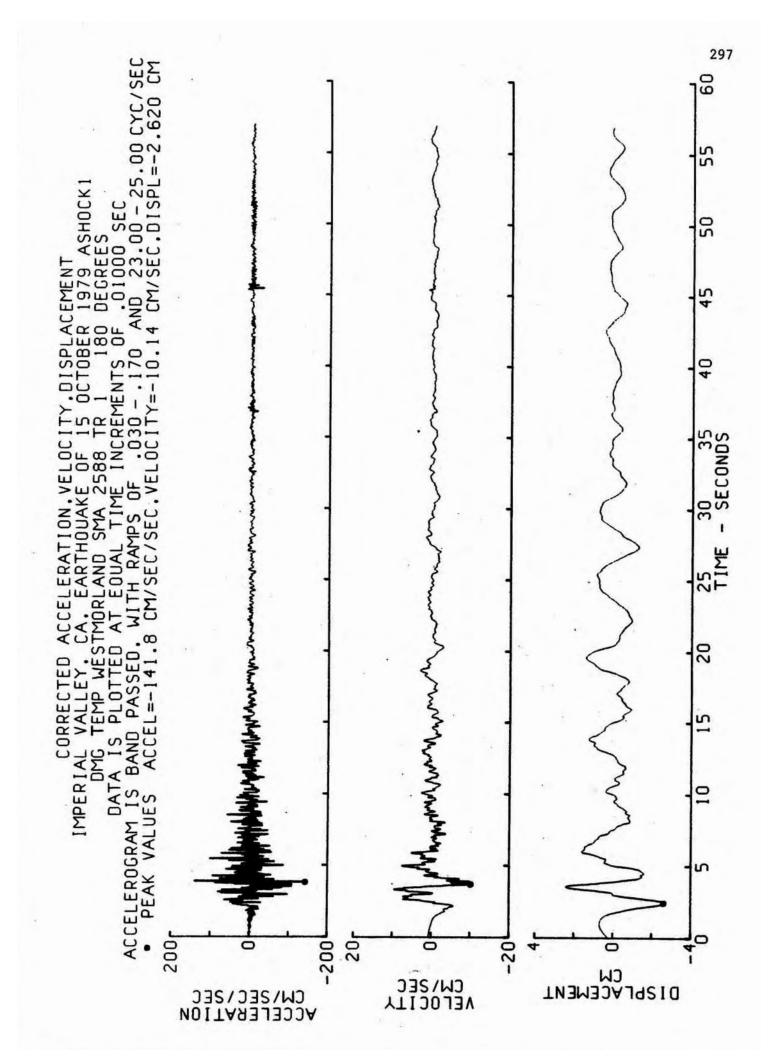




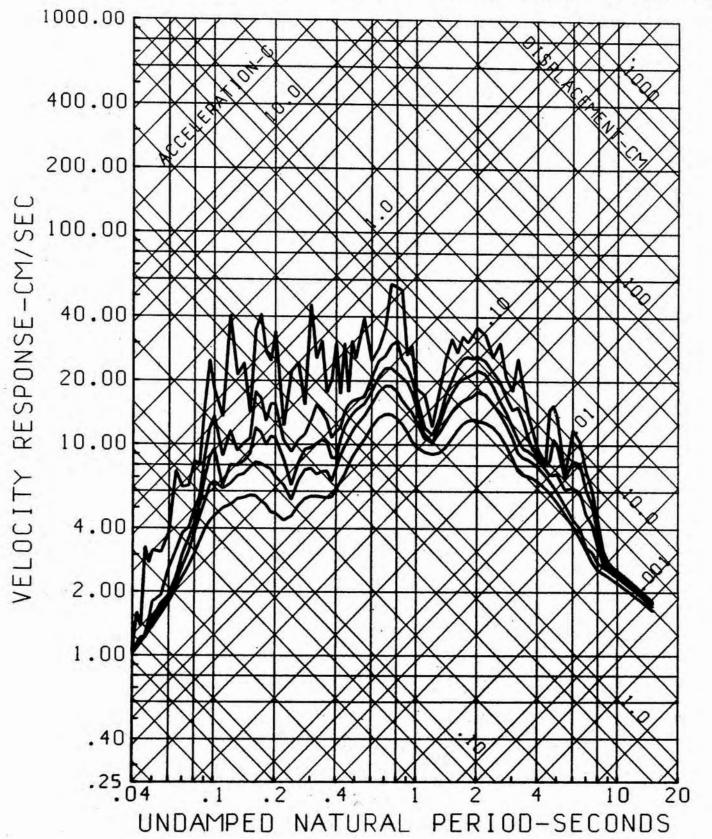


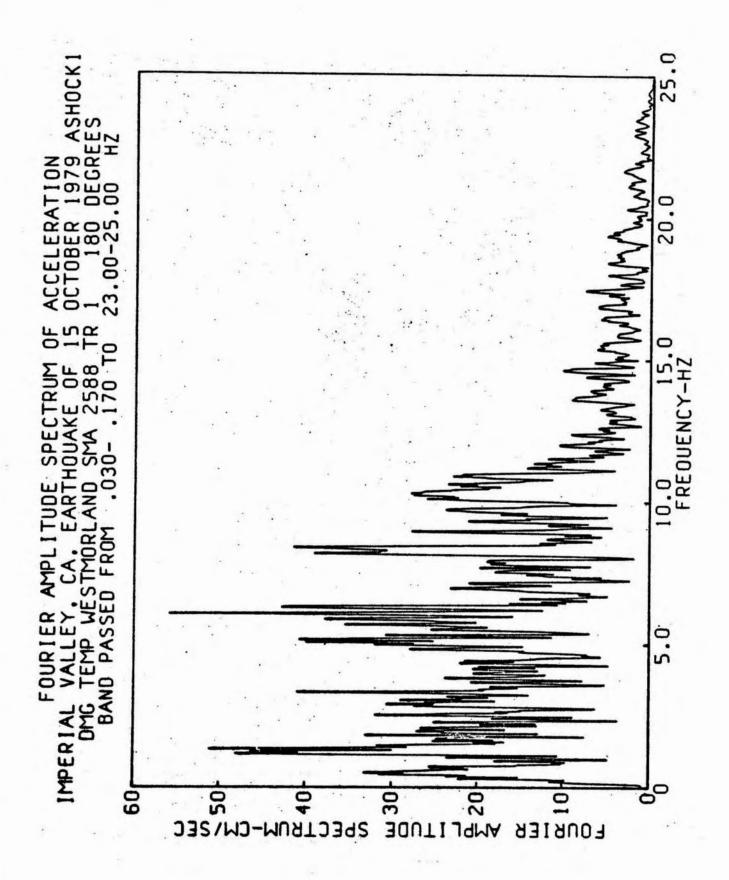


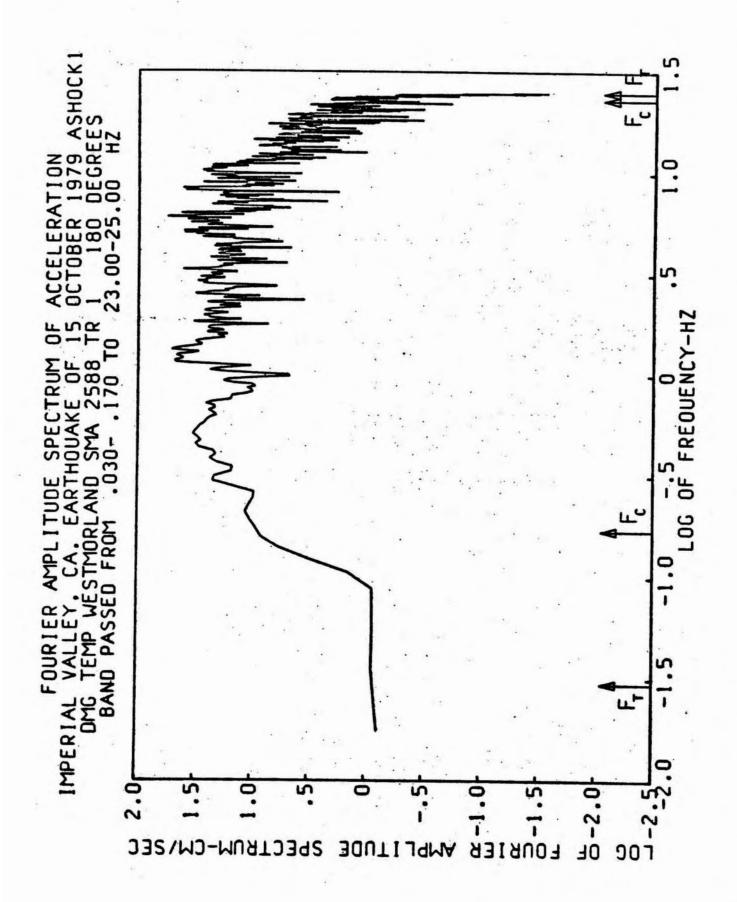


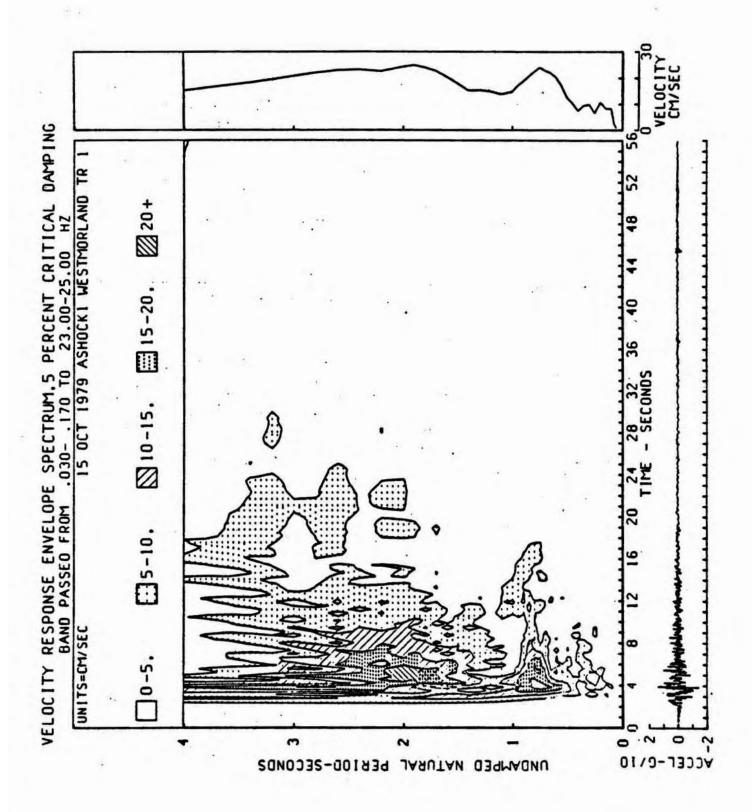


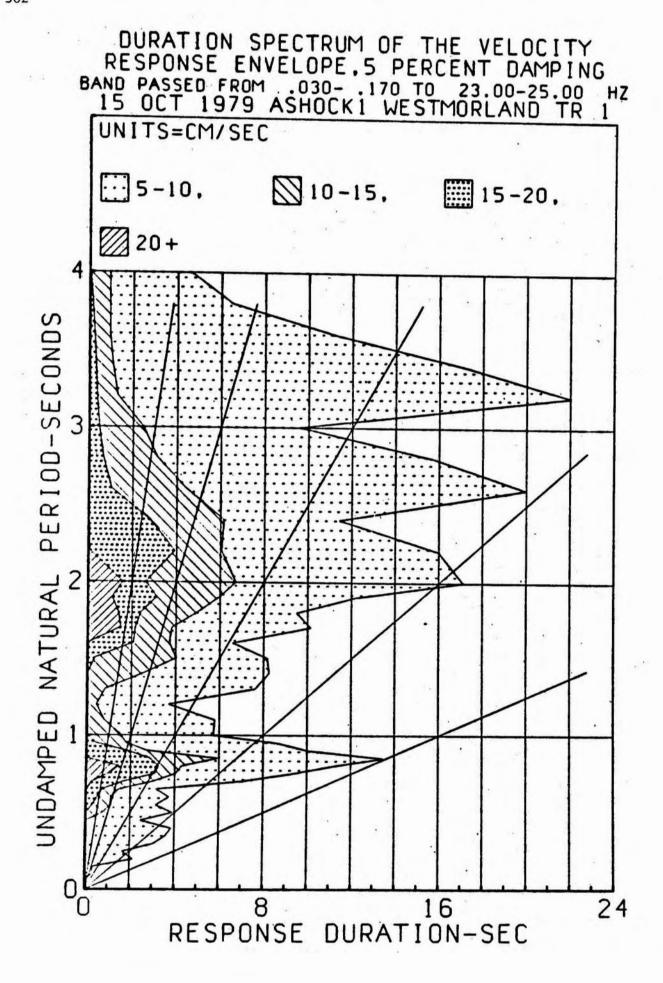
RESPONSE SPECTRA
15 OCT 1979 ASHOCK1 WESTMORLAND TR 1
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



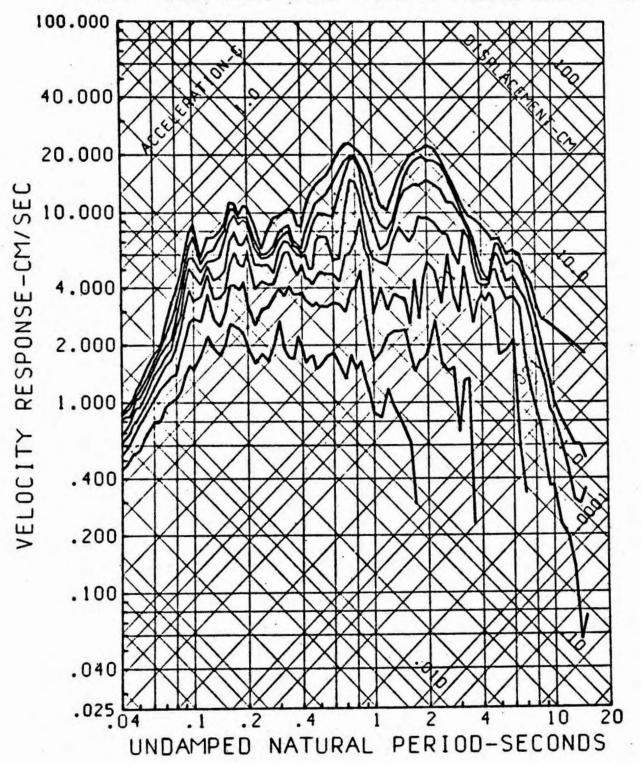


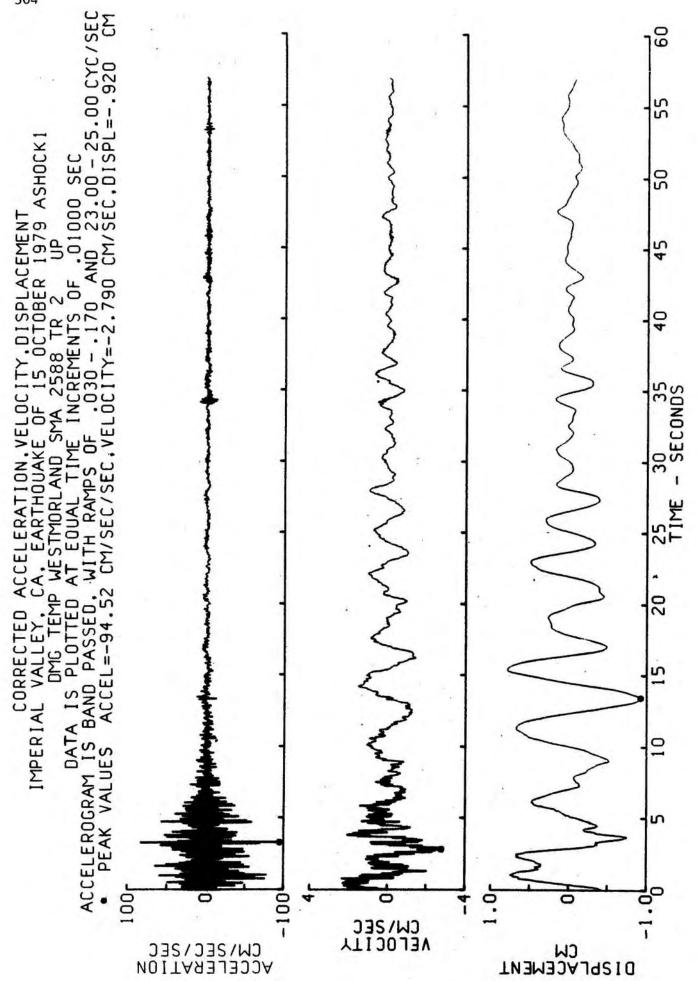






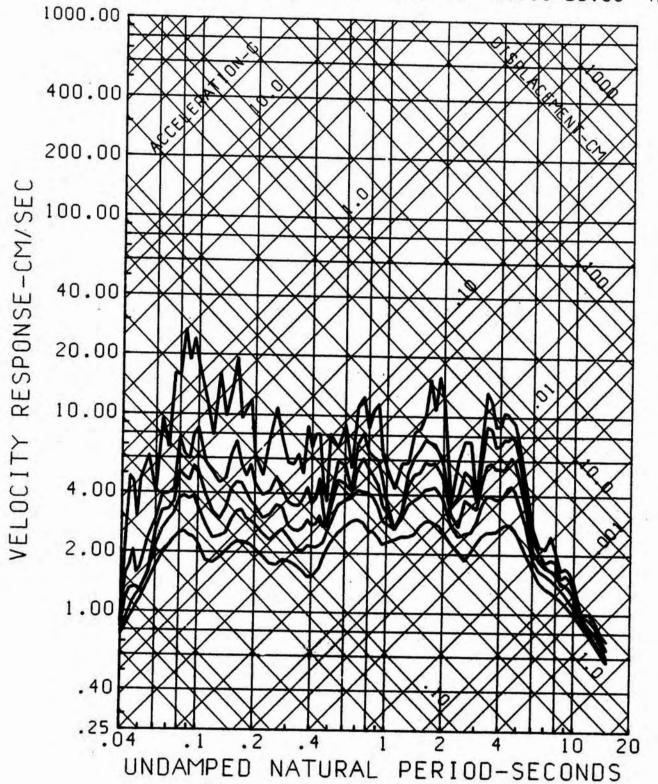
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 ASHOCK1 WESTMORLAND TR 1 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

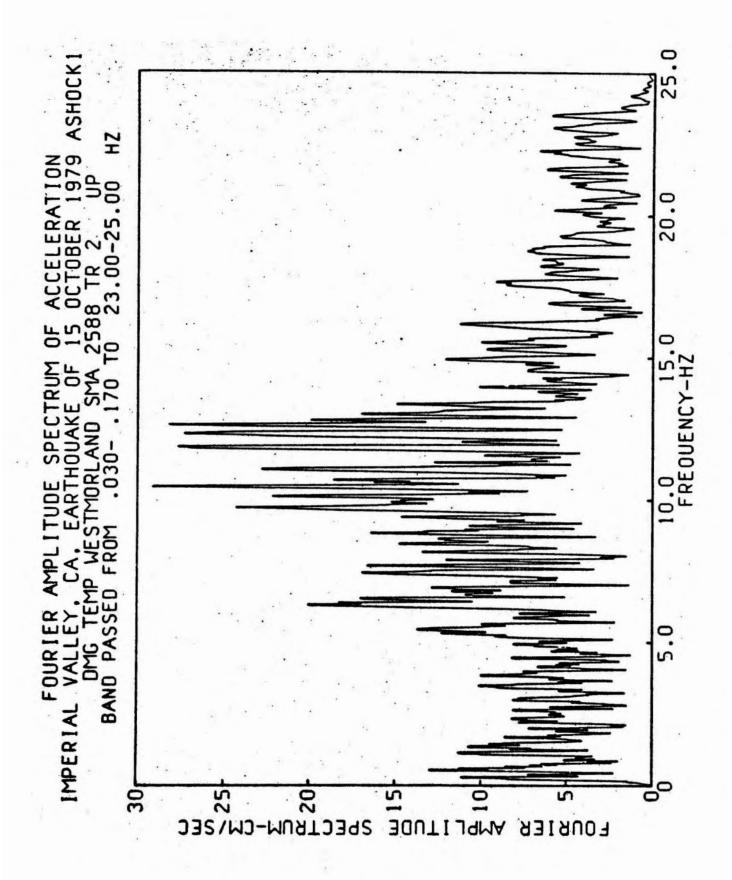


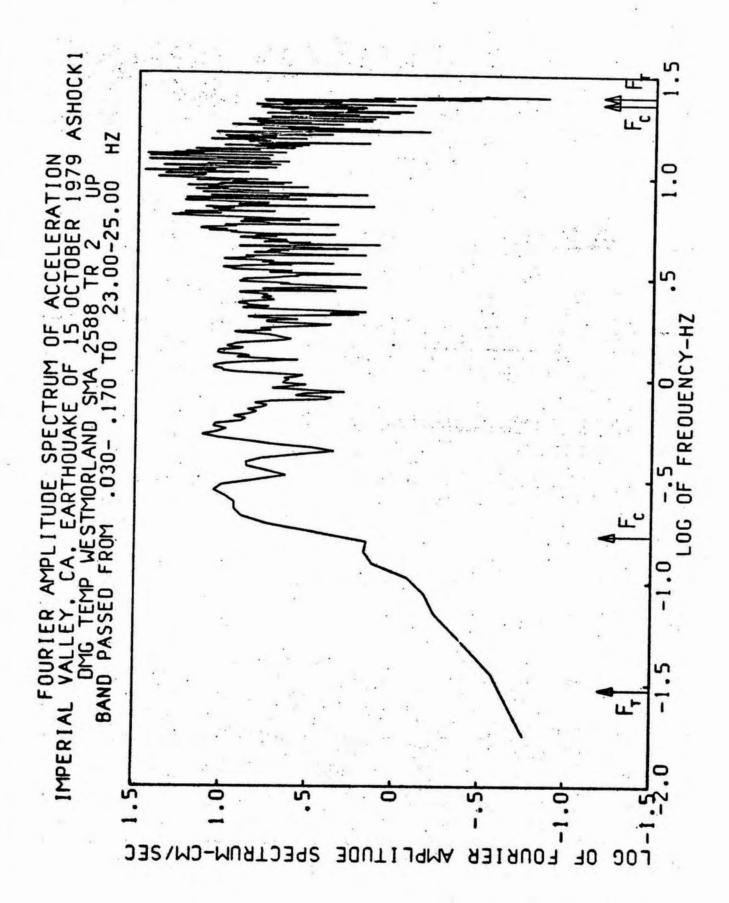


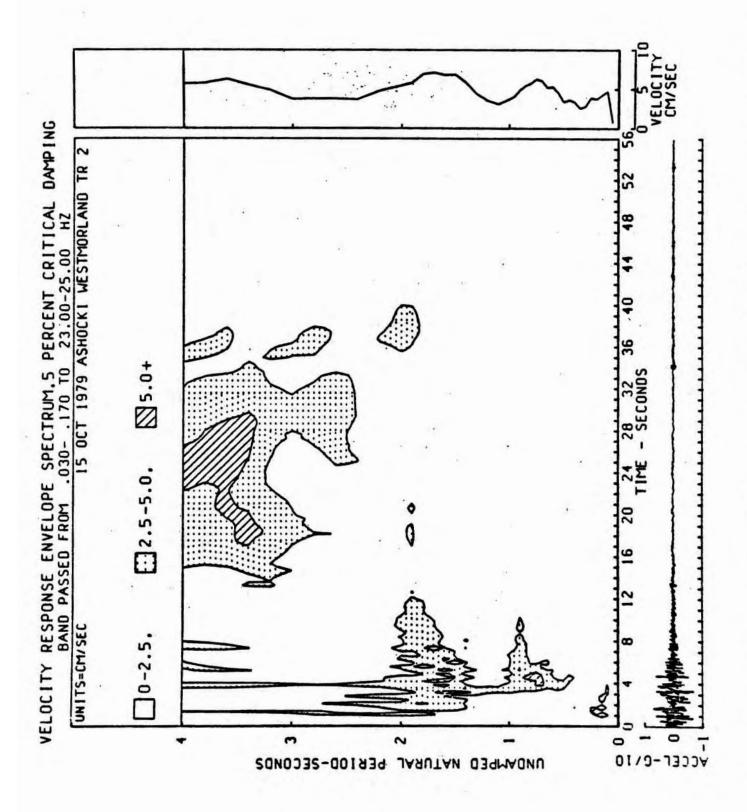
RESPONSE SPECTRA

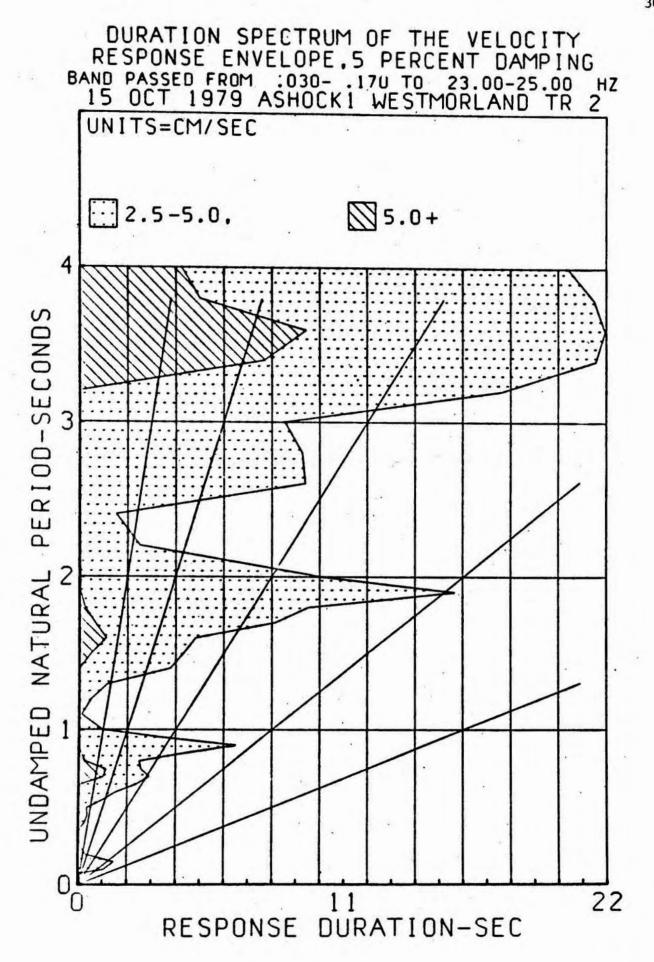
15 OCT 1979 ASHOCK1 WESTMORLAND TR 2
0,2,5,10,20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ



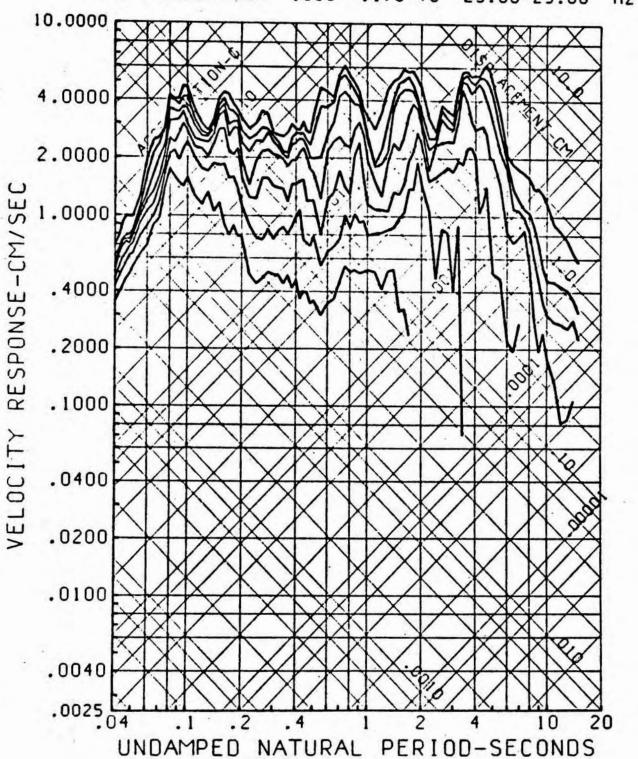






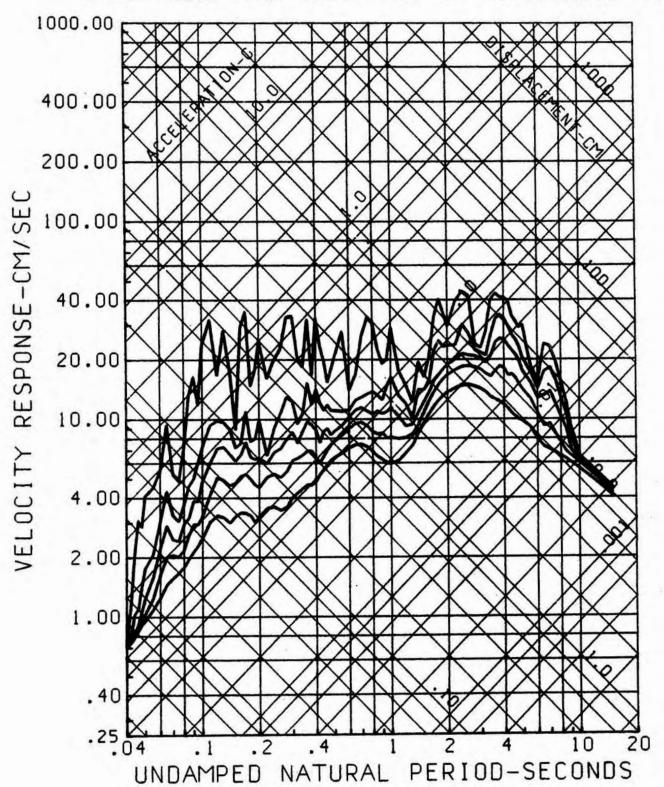


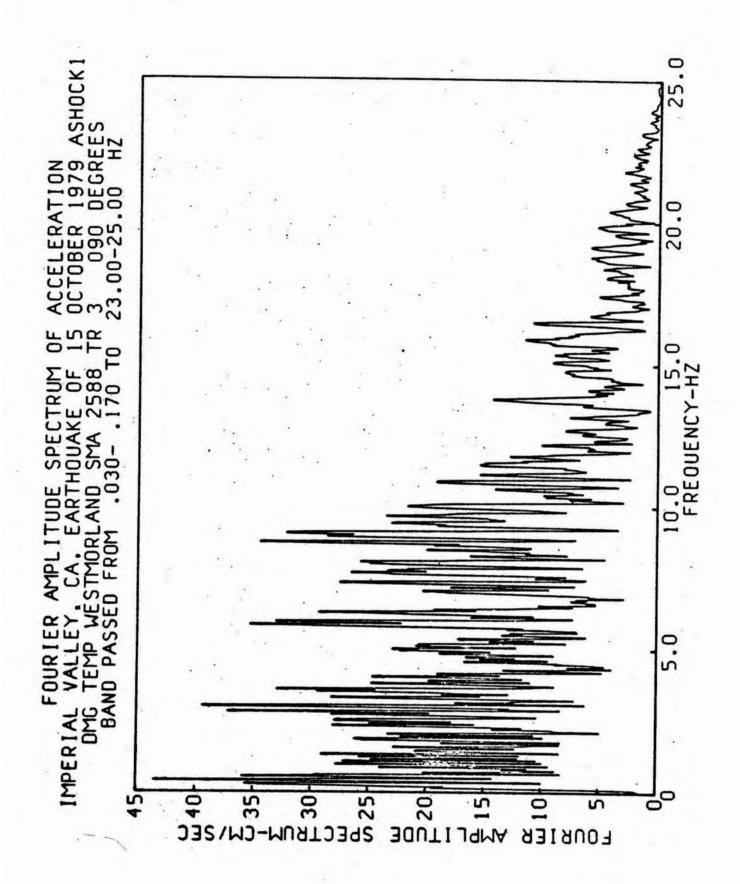
SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 ASHOCKI WESTMORLAND TR 2 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

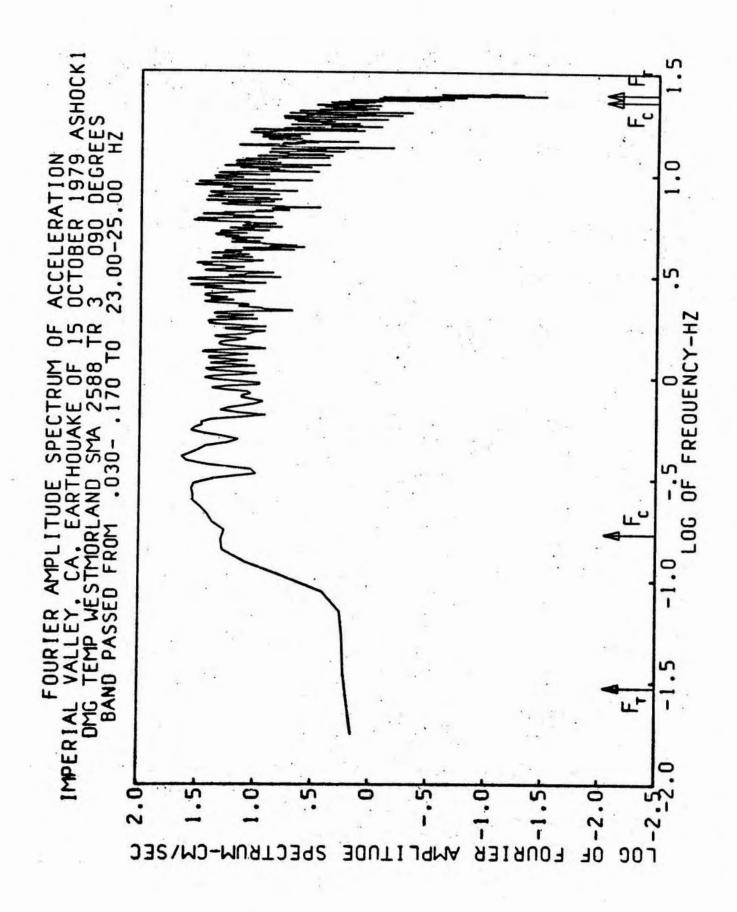


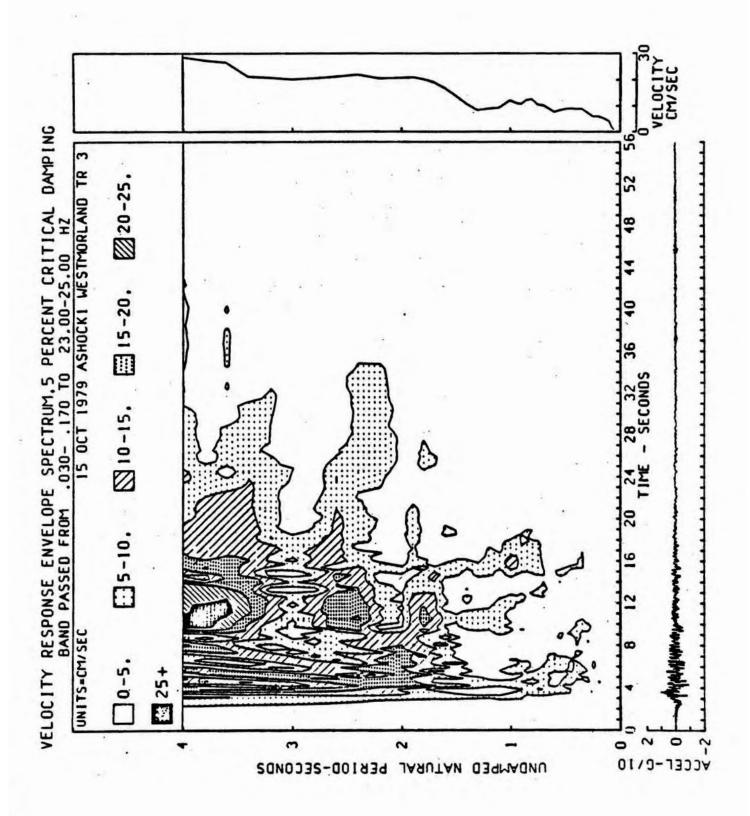
RESPONSE SPECTRA

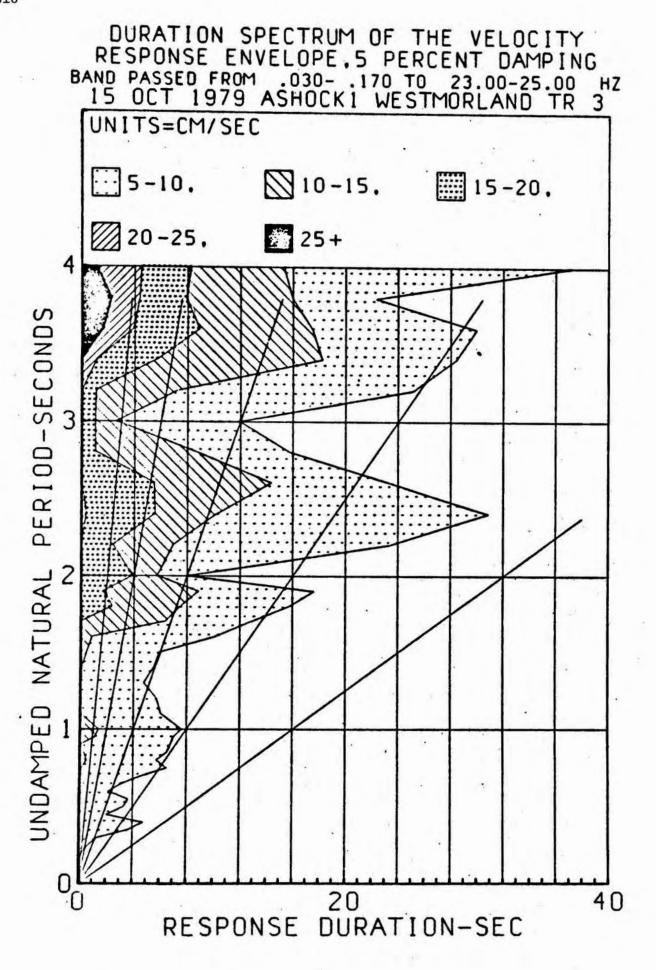
15 OCT 1979 ASHOCK1 WESTMORLAND TR 3
0.2.5.10.20 PERCENT CRITICAL DAMPING
BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ











SPECTRA OF AMPLITUDES SUSTAINED FOR ANY GIVEN NUMBER OF CYCLES 15 OCT 1979 ASHOCK1 WESTMORLAND TR 3 5 PERCENT CRITICAL DAMPING BAND PASSED FROM .030- .170 TO 23.00-25.00 HZ

